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It should be noted that most of the pages are identifiable as having been processed by me.

I put a lot of time into producing these files which is why you are met with this page when you open the file.

In order to generate this file, I need to scan the pages, split the double pages and remove any edge marks such as punch holes, clean up the pages, set the relevant pages to be all the same size and alignment. I then run Omnipage (OCR) to generate the searchable text and then generate the pdf file.

Hopefully after all that, I end up with a presentable file. If you find missing pages, pages in the wrong order, anything else wrong with the file or simply want to make a comment, please drop me a line (see above).

It is my hope that you find the file of use to you personally – I know that I would have liked to have found some of these files years ago – they would have saved me a lot of time !

Colin Hinson In the village of Blunham, Bedfordshire.

# AP116U-0516-1

# POWER SUPPLY, TRANSISTOR DEVICES TYPE SPS-1070

BY COMMAND OF THE DEFENCE COUNCIL

(T. Dunnett

Ministry of Defence

Sponsored for use in the ROYAL AIR FORCE by DWSE(RAF)

Publications authority: DATP/MOD(PE)

Service users should send their comments through the channel prescribed for the purpose in:

AP 3158 Vol.2 Leaflet No.D6 (ARMY and RAF)

1ssued Dec.73

FOR OFFICIAL USE ONLY

#### **INSTRUCTION MANUAL - MODEL SPS-1070 POWER SUPPLY**

- Status Indicating Relay: A status indicating relay is provided with double pole-double throw contacts which indicate the operating status of the power supply. The relay is actuated when the power supply is operating within predetermined voltage limits. The relay is deactuated when the power supply is operating outside of these limits or when the power supply is off.
- Margin Adjust: Provision is made for remote programming the power supply up and down (margin adjust). Programming down is accomplished by shorting terminal TB1-9 (MV3) to terminal TB1-10 (MV4). Programming up is accomplished by shorting terminal TB1-8 (MV2) to terminal TB1-7 (MV1). The output change due to programming is .2 V.

#### Front Panel Controls:

Output Voltage Meter: 0 to 10 V

Output Current Meter: 0 to 50 A

Voltage Adjustment Potentiometer, Coarse and Fine: Set to desired output voltage as measured on the front panel meter or on the front panel test points.

Overvoltage Adjust: Normally factory-set to 6 V or may be adjusted in the field.

Current (Limit) Adjust: This is normally set at 45 A at the factory. This is done by loading the power supply to 45 A and turning the current limit adjust counterclockwise until the mode indicating lamp operates. The current limit adjust may be adjusted to lesser values in accordance with the operational requirements of the system by turning the current limit adjust counterclockwise with the system operating until the mode indicating lamp illuminates. The current limit adjust should then be turned clockwise approximately 1/8 of a turn until the mode indicator lamp extinguishes.

Test Points: Makes available the regulated output voltage.

Mode Indicator Lamp DS-1: When illuminated, indicates current limiting operation.

Circuit Breaker CB-1: For on-off operation and line protection.

AC-On Lamp DS-2: Indicates power is on and circuit breaker is on.

#### **INSTRUCTION MANUAL - MODEL SPS-1070 POWER SUPPLY (LINK)**

#### 1. INTRODUCTION

The Model SPS-1070 power supply (Link P/N D697901) is

shown in Figure 1 (D13225) and has the following specifications:

Input Voltage: 105 to 132 V, 47 to C Hz

Output Voltage: Adjustable 5 to 5.4 V @ 0 to 40 A

Regulation: Line: Less than .005% or 2 MV for 105-132 V AC line change

Load: Less than .005% or 2 MV for no load to (or from) full load changes

Ripple and Noise: .5 MV RMS - 3 MV p.p. max.

- vervoltage Protection: Response time 50 usec. The overvoltage is normally set to 8 V at the factory. It may be readjusted in accordance with the application as required.
- Overload Protection: By electronic current limiting. The power supply will current limit at approximately 45A or less as adjusted by the operator. Under short circuit conditions, the load current will be reduced to a safe value and the power supply will automatically recover as soon as the overload or short circuit is removed.
- Remote Programming: By external potentiometer, 1K, connected between terminals 7 and 8 to TB2.
- Parallel Operation: Up to four units by interconnection between power supplies. See following section on rear panel connections.

Remote Sensing: Yes

**Temperature** Range: -20 to +65<sup>O</sup>C

Temperature Coefficient: .01%/°C

- Size: Front panel is 19" wide by 3½" high; depth is 16-3/4" plus 4" protrusion for terminal Blocks and power connections.
- Cooling: Cooling is by external forced air which may enter either on the left front side of the power supply or from the bottom surface of the power supply.

#### **TEPTRUCTION MANUAL - NODEL SPS-1070 POWER SUPPLY**

the on-off front panel circuit breaker CB-1. When the circuit breaker is actuated, power is applied to AC-on indicator lamp DS-2 and to the primary of transformer T1.

The main power secondary of transformer T1 (terminals 8, 9, 10) is rectified and filtered by the action of rectifiers CR3 and CR4 and filter capacitors C5 through Cl6. The voltage on these capacitors varies between 9 and 13 V in accordance with the line and load conditions.

The transistor configuration Q1, Q9, Q10 through Q19 is a Darlington-driven parallel pass transistor configuration which acts as the main regulator; i.e., the regulated output voltage appears on terminals E1 and E2. The pass transistor configuration is inserted between the unregulated output voltage appearing on the filter capacitors and the regulated output voltage appearing on the filput terminals. The difference voltage is dropped across the pass transistors. This is accomplished by adjusting the drive signal from the regulator so that the output voltage remains constant independent of line and load conditions.

A control (bias) voltage is generated by an additional secondary of transformer Tl (terminals 5, 6, 7), full wave center tap rectifiers CRl and CR2, and filter network Rl-Cl. The voltage on Cl is approximately 30 V. A control voltage is generated by the action of voltage dropping resistor R2 and zener diode CR5. The voltage on the cathode of CR5 is approximately  $1\frac{12}{7}$  V more positive than the positive sense lead.

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#### **UNTRUCTION MANUAL - MODEL SPS-1070 POWER SUPPLY**

#### **Near Panel Connections:**

Jl - Line cord connector (provided with the unit) to plug into the AC line. The two AC lines and ground connections are provided.
TB1-1: Normally open contact of status indicating relay.
TB1-2: C contact of status indicating relay.
TB1-3: Normally closed contact of status indicating relay.
TB1-4: Normally open contact of status indicating relay.
TB1-5: C contact of status indicating relay.
TB1-6: Normally closed contact of status indicating relay.
TB1-7) TB1-8) Positive margin adjust.
TB1-9) TB1-10) Negative margin adjust.
TB1-11: + output
TB1-12: + output sensing (should be jumpered to -11 or + output is remote sensing is used.)
TB1-13: - sensing (should be jumpered to minus sensing either locally or at the load.
TB1-14: - output.
TB1-15) TB1-16) Normally shorted together. If parallel opera- tion is required, the jumper from -15 to -16 should be removed on the slave units and TB1-15 should be connected to TB1-15 of the master unit.
El: + output.

E2: - output.

# 2. THEORY OF OPERATION

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### 2.1 Regulator Action

A schematic diagram of the SPS-1070 is shown in Figure 2 (Drawing #D14286). AC power is applied to Jl, which applies power to.

#### **INSTRUCTION MANUAL - MODEL SPS-1070 POWER SUPPLY**

Operation of the voltage regulator circuit is as follows: A reference voltage is generated by voltage dropping resistor R22 and zener diode CR8. The reference voltage across CR8 is reduced by the action of voltage divider network F23-R24 so that approximately 3.8 V appears on the base of transistor Q7. The output voltage is sensed by resistive divider network R27, R29, R61, and R60 (voltage adjust potentiometer). Transistors Q7 and Q8 operate as a differential error amplifier. When the output voltage is at the correct level, the voltage on the base of Q7 will approximately equal he voltage on the base of Q8. If the output voltage tends to rise, Q8 conducts more heavily, thereby reducing the conduction of Q7. The amplified error voltage appears on the collector of Q7 and is applied to the base of intermediate voltage amplifier transistor Q5. The error voltage is further amplified and inverted at the collector of Q5 and applied to the base of transistor Q2, which in turn drives the pass transistor configuration Q1, Q9, etc., through TB1-15 and -16. It will be noted that as the output voltage tends to increase, the collector of Q7 becomes more positive, thereby reducing the voltage on the collector of Q5, which in turn reduces the drive to Q2, Q, etc., and reduces the output voltage in a regulatory fashion.

#### 2.2 Overvoltage Protection

A voltage reference is generated by series dropping resistor R31 and zener diode CR10. The output voltage is measured by voltage divider network CR11-CR12, temperature compensation resistors R34, R33, R32 (overvoltage adjust). When the overvoltage condition is reached, transistor Q20 turns on, actuating the gate of SCR-1,

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#### LATRUCTION NAMUAL - MODBL SPS-1070 POWER SUPPLY

thereby shutting the power supply down. It will be noted that firing of SCR-1 removes the drive to the power supplies through resistor R59 so that once the overvoltage has fired, there is minimal current flowing in the system. The overvoltage may be reset by turning off the line power by circuit breaker CB-1 and re-applying it.

#### 2.3 Current Limiting Circuit

Resistors R40 through R49 generate a voltage drop proportional to the load current. In addition, the base to emitter drops \* transistor Q9 and the pass transistor configuration Q10, etc., are approximately proportional to the load current. Accordingly, the voltage on the base of Q9 is a direct indication of the load current flowing. This voltage is sensed by resistive divider R8-R7-R12 and applied to the base of transistor Q3 through resistor R9. Potentiometer R7 sets the maximum current capability adjust of the front panel current limit and is normally set at approximately 55 A. Front panel current limit adjust R28 is normally set at approximately 45 A, and bendback adjust R9 is normally set so that the where circuit current is between 20 and 30 A. When excessive current 1. drawn, the base of Q3 becomes positive (conducting through the emitter of Q3 to the base of Q4 to the emitter of Q4, which is tied to the positive output.) When transistor Q3 conducts, it shunts (limits) the drive signal to transistor Q2 and the power supply enters a current limiting mode of operation. As the load resistance is decreased in value (heavier load), the output voltage falls. Since R8-R7-R12 is essentially a voltage divider, less voltage on the base of Q9 is required to keep Q3 in conduction, and the current limit bendback characteristic illustrated in Figure 3 is achieved.

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#### WETRUCTION MANUAL - MODEL SPS-1070 POWER SUPPLY

Current limit operation is indicated by lamp DS-1. When Q3 conducts, Q4 conducts, which in turn illuminates lamp DS-1.

#### 2.4 Status Indicating Relay

Relay K1 is normally de-energized when the power supply is off and remains de-energized until the power supply reaches proper operating voltage. Zener diode CR13 serves as a separate reference for the over- and undervoltage indicating circuits. Differential amplifier transistors Q23 and Q24, in conjunction with resistive divider R38-R37-R36, measure the overvoltage status, and in the event of overvoltage, turns off transistor Q21. Differential amplifier transistors Q25 and Q26 and resistive divider network R57-R56-R55 (undervoltage adjust) measure the undervoltage status, and in the event of undervoltage, turn off transistor Q22. Hence, it will be noted that relay K1 can only be energized if the output voltage is between the over- and undervoltage limits previously defined. Relay K1 is shown on the schematic in its normally de-energized condition and hence, the contacts will change to the energized position when the output voltage is at the correct level.

#### 2.5 Margin Adjust

The margin adjust is for checking the performance of the utilization equipment. Margin adjust downward is accomplished by shorting terminals TB1-9 and -10 (MV3 and MV4) together, which places resistor R28 across the voltage divider sensing network and causes the regulator to shift downward in voltage. Positive margin adjust is accomplished by shorting terminals TB1-7 and -8 (MV1 and MV2) together, which places resistor R30 across resistor R29 and causes an upward change in the regulator for positive margin adjust testing.

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#### INSTRUCTION MANUAL - MODEL SPS-1070 POWER SUPPLY

#### 2.6 Miscellaneous Components

Resistor R13 is a bleeder resistor designed to prevent spillover due to leakage currents at no load. Resistor P11 is a load voltage compensating resistor which modifies the regulation in accordance with the load current for improved performance. Zener diode CR7 prevents conduction of transistor Q5 until the power supply builds up to rated voltage and hence, assures build-up. Meters M1 and M2 are the front panel ammeter and voltmeter, respectively.

#### 3. COMPONENT LOCATION

The location of major components (chassis-mounted) is indicated on the outline and installation drawing of Figure 1. The smaller components are located on the printed circuit board, a layout of which is shown in Figure 4. The electrical parts list is given on the following pages.



### INSTRUCTION MANUAL

TDI P/N SPS-1070

LINK P/N D697901

June 1970

#### TDI P/N SPS-1070

AMENDMENT NO. 1

PAGE 3 SHOULD READ:

- TB1-12 + Output Sensing (Must Be Connected To Possitive Output Either At The Power Supply Or At The Load)
- TB1-13 Output Sensing (Must Be Connected To Negative Output Either At The Power Supply Or At The Load)

#### SCHEMATIC DIAGRAM SHOULD BE:

R3	220	Ohm <b>s</b>		
R1 2	18K	Ohm <b>s</b>		
R59	10	Ohms		
R14	Refe	erence	Note	3

Note 3: To Be Selected In Range Of 680 Ohms To 1.5K Ohms

#### PARTS LIST SHOULD BE:

R3	220	Ohms	RC20GF221K
R12	18K	Ohms	RC20GF183K
R59	10	Ohms	RC20GF100K

Section No.		Page No.
1.	Introduction	1, 2, 3
2.	Theory of Operation	3
2.1 2.2 2.3 2.4 2.5 2.6	Regulator Action Overvoltage Protection Current Limit Circuit Status Indicating Relay Margin Adjust Miscellaneous Components	.3, 4, 5 5, 6 6, 7 7 7 8
3.	Component Location	8

# LIST OF ILLUSTRATIONS

Figure No.		Drawing No.
1.	Outline & Installation Drawing	D13225
2.	Schematic Diagram	D14286
3.	Current Limit Bendback	24449
4.	PC Board Layout	D14353
	Electrical Parts List	A14362



QTY REQD	ITEM NO	NOMENCLATURI DESCRIPTION	E or N	PART or IDENTIFYING NO	APPD MFR or EQUIV	
	C I	CAP. 39 MFD 60	V	CL6761,390MP3	QPL.	
	C 2	.01 '1FD 20	0 V 0	CK06CWI03K	QPL	
	СЗ	.1 MFD 200	v v	75F3R2A104	G.E.	
	C 4	39,000 MFD	IC V	86 <b>F114</b> 34	G.E.	
	C 5	10,300 MFD	20 V	86F130M	1	
	Сб			1		
	С7					
	C 8					
	C G					
	C 10			•		
	CII					
	C 12					
	C 13					
	C 14					
	C 15			1		
	CIE	10,800 MFJ	20 V	86FT-DMT	G.E.	
	C 50	.I MFD 200	V	75F5R_AL)4	G.t.	
	13 J	JAP. 3.3.MFD 35	V	CST-BE335M	QPL	
	CB I	CIRCUIT BREAK	ER	7.5 A AMI2M66	HE IN IMAN	
	CR I	SILICON RECTI	FIER	JAN 114245	0PL	
	CR 2		1	114245		
	CR 3			1.1124		
	CR 4	SILICO'I RECTI	FIER	111134		
	CR 5	JENER DIODE,	12 V	119n 3B		
	CR 5	SILICON RECTI	FIER	1No45		
	CR 7	ZENER LIODE,	5.5 V	IN752A		
	CR 8	ZENER DIOJE,	6.2 V	1.1321		
	CR 9	SILI CON RECTI	FLR	11202A		
	CR D	ZENER DIDUE,	3.9 V	11743		
	CR II	SILICON RELTI	≌1±R	JAN INF45	QPL	
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	A		Retyped ar	d corrected			1/10/69	E.D.
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	с		Added C81		ECN-1	470	3/9/70	I.Y.
	D		R3 was 820	)	ECN-1	630	3/11/70	I.Y.
	E		TP1, TP2, Added Hand	TP2, AND TP3 wrong Part No. d Handles, added Jumpers				A.A.
	F		Handle 126	64-1 was 1075-1			9/30/70	A.A.
	G		R12 18K wa	<b>IS R12</b> 27K			10/13/70	) RFB
	H		R59 was 10	00	ECN-1	768	2/3/71	AC
	I.		R80 was ad	lded			3/12/71	A.Á.
	J		R52 was 1	2 was 1 K				A.A.
	ĸ		Cl was CL6	55CK390MP3	ECN-2	178	12/12/7	2 G.A.
	L		R19 was 15	0	······································		12/12/7	G.A.
	М		Retyped ar	d updated (no p	arts c	hanged)	2/8/73	
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	с		Added C81		ECN-1	.470	3/9/70	I.Y.
	D		R3 was 820	)	ECN-]	.630	3/11/70	I.Y.
	E		TP1, TP2, AND TP3 wrong Part No. Added Handles, added Jumpers				5/12/70	A.A.
	F	, ,	Handle 126	54-1 was 1075-1			9/30/70	A.A.
	. ع		R12 18K was R12 27K				10/13/7	) RFB
	H		R59 was 10	00	ECN-1	.768	2/3/71	AC
	I.		R80 was ad	lded			3/12/71	A.Á.
	J		R52 was 1	ĸ			3/12/71	A.A.
	к		Cl was CL6	Cl was CL65CK390MP3 ECN-2178				2 G.A.
	L		R19 was 15	R19 was 150				G.A.
	м		Retyped an	d updated (no p	arts c	hanged)	2/8/73	
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QTY REQD	ITEM NO	NOMENCLATURE O DESCRIPTION	r PART or IDENTIFYING NO	APPD MFR or EQUIV
	Q 15	TRANSISTOR	JAN 2N3055	<b>QPL</b>
	Q 16			
	Q 17			
	Q 18			
	Q 19		2N3055	
	Q 20		2N2907A	
	Q 21		2N2907A	
	Q 22		2N2907/2N4037	
	Q 23		2N1613	
	Q 24		2N1613	
	Q 25		2N1613	Y
	Q 26	TRANSISTOR	JÄN 2N1613	QPL
	RI	RES. 100 I W 10%	RC32GF100K	QPL
	R 2	560 2 W 10%	RC <b>42</b> GF561K	
	R 3	220 I/2 W 109	RC20GF221K	
	R 4	IK 1/2 W 109	K RC20GF102K	
	R 5	100 1/2 W 10;	RC20GF101K	
	R 6	100 1/2 W 109	RC20GF101K	
	R 7	VAR. IO K	R <b>V5</b> LAYSB103A	
	R 8	VAR. IOK WW	RA20LASB103A	Y I
	R 9	RES. VAR. IO K	RV5LAYSB103A	QPL
	R 10	SHUNT METER	50A-50MV	EMPRO
	RII	RES. SELECT IN TEST		QPL
	R 12	18 K 1/2 W 10	0% RC20GF183K	
	R 13	· 27 2 W 10%	RC42GF270K	
	R 14	SELECT IN TEST		
	R 15	10 K 1/2 W 10	0% RC20GF103K	
	R 16	IK 1/2 W 109	RC20GF102K	
	R 17	8.2 K 1/2 W	10% RC20GF&22K	
	R 18	8.2 K 1/2 W	10% RC20GF822K	
	R 19	120 1/2 W 109	RC20GF121K	1
	R 20	RES. 270 1/2 W 109	RC20GF271K	QÞL
		*vendor item see so CODE	ource control or specification control d	rawings
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QTY REQD	IŤEM NO	NOMENCLAT DESCRIPTI	URE or ON	IDEN 1	PART or FIFYING NO		APPD MFR or EQUIV	
	R 21	RES. 5.6 K 1/.	2 W 10%	RC20GF5	62K		, QPL	
	<b>R</b> 22	I.5 K 2	N 1% WW	RW79U15	OIF		QPL	
	R 23	IK 2W	1% WW	RW79UIC	01F		Å	
	R 24	1.5 K 2	V 18 WW	RW79U15	01F			
	R 25	IK 1/2	N 10%	RC20GF1	02K			
	R 26	560 1/2	N . 10%	RC20GF5	61K			
	R 27	274 2 W	1% WW	RW79U27	40F			
	R 28	I K 1/2	V 10%	RC20GF1	02K			
	R 29	909 2 W	1% WW	RW79U90	90F			
	R 30	5.6 K 1/	2 W 10%	RC20GF5	62K			
	R 31	470 1/2	V 10%	RC20GF4	171K			
	R 32	VAR. IK	WW	RA20LAS	68102A			
	R 33	120 1/2	N 10%	RC20GF1	21K			
	R 34	560 1/2	V 10%	RC20GF5	JE I K			
	R 35	100 1/2	V 10%	RC20GF1	01K			
	R 36	VAR. 500		RA20LAS	B501A			
	R 37	I.2 K 1/	2 W 10%	RC20GF1	22K			
	R 38	IK 1/2	V 10%	RC20GF1	02K			
	R 39	330 1/2	V 10%	RC20GF3	531K		QPL	
	R 40	.1 5 W		PW5			IRC	
	R 41			1				
	R 42							
	R 43							
	R 44							
	R 45							
1	R 46							
	R 47							
	R 48	Y						
	R 49	.1 5 W		PW5			IRC	
	R 50	4.7 K 1/	2 W 10%	RC20GF4	172K		QPL	
	R 51	I.2 K I/	2W 10%	RC20GFI	22K		1	
	R 52	RES. 820, 1/2	N 10%	RC20GF8	321K		QPL	
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	R 53	RES. IK 1/2 W	10%	RC20GF102K		QPL
	R 54	330 I/2 W	1 10%	RC20GF331K		
	R 55	VAR. 500		RA20LASB501A		
	R 56	1.5 K 1/2	W 10%	RC20GF152K		
	R 57	I K 1/2 W	10%	RC20GF102K		
	R 58	4.7 K 1/2	W 10%	RC20GF472K		
	R 59	10 1/2 W	10%	RC20GF100K		
	R 60	VAR. IO K		RA20LASB103A		
	R 61	2.7 K 1/2	W 10%	RC20GF272K		
	R 62	IK VAR.		RA20LASB102A		
	R 63	· VAR. IK		RA20LASB102A		
	R 64	IK 1/2 W	10%	RC20GF102K		V
	R 80	RES. 220 1/2 W	10%	RC20GF221K		QPL .
	ŢI	TRANSFORME	R	B <b>-1</b> 3848		TDI
	·	HANDLES	(2 per Unit)	1264-1		CAMBION
		JUMPERS (2	per Unit)	604J		KULKA
	тв і	TERMINAL E	BLOCK	699-2104 <b>-16-</b> GD1-30F		KULKA
	TP I	TEST POINT (	RED)	111-102		JOHNSON
	TP 2	TEST POINT (	BLK)	111-103		JOHNSON
	TP 3	TEST POINT (	V10)	111-112		JOHNSON ;
	SCR I	SILICON CONTRO	LLED RECT.	C45 F		G.E.
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