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Colin Hinson
In the village of Blunham, Bedfordshire.

## TELEVISION MONOCHROME CAMERA

## MARCONI VIDICON TYPE V321 SERIES

## AND CONTROL EQUIPMENT

BY COMMAND OF THE DEFENCE COUNCIL

(Ministry of Defence)
FOR USE IN THE
ROYAL AIR FORCE
(Prepared by the Procurement Executive, Ministry of Defence)

## FIRST AID IN CASE OF ELECTRIC SHOCK

DO NOT TOUCH THE VICTIM WITH YOUR BARE HANDS until the circuit is broken.

SWITCH OFF. If this is not possible, PROTECT YOURSELF with dry insulating material and pull the victim clear of the conductor.

## THE EXPIRED AIR METHOD OF ARTIFICIAL RESPIRATION <br> (Approved by the Royal Life Saving Society)

1. Lay the patient on his back with his arms to his sides. If on a slope have the stomach slightly lower than the chest. Make a brief inspection of the mouth and throat to ensure that they are clear of obvious obstruction.
2. Kneel on one side of the patient level with his head, place one hand under his neck and the other on top of his head (Fig.1).
LIFT THE NECK AND TILT THE HEAD BACK AS FAR AS POSSIBLE.
3. Move the hand from under the neck and place it on the chin of the patient, the thumb between the chin and mouth, the index finger along the line of the jaw, the remaining fingers curled (Fig.2). Whilst positioning the patient, open your mouth and take deep breaths.
4. Using the thumb of your hand on the chin to keep the lips sealed, open your mouth wide and make a seal round the patient's nose and blow into it (Fig.3).
5. After blowing, turn your head to observe the rise of the chest (Fig.4). If no air enters the patient's lungs, the nose may be blocked and the mouth should be opened using the hand on the chin; open your mouth wide and making a seal round his mouth blow into it. Turn the head to observe the chest rise. This may be used as an alternative to blowing into the nose even when the nose is not blocked, but the nose must be sealed either with the cheek or by moving the hand from the top of the head and pinching the nostrils.
THE HEAD MUST BE KEPT AT FULL BACKWARDS TILT.
6. Start with ten quick deep breaths and then continue at the rate of twelve to fifteen breaths per minute. This should be continued until the patient revives or a doctor certifies death.
7. In the case of facial injuries it may be necessary to do a manual method of artificial respiration (Holger Nielsen).

8. It is ESSENTIAL to commence artificial respiration without delay and to send for medical assistance immediately.

## TREATMENT FOR BURNS

If the patient is also suffering from burns, then, without hindrance to artificial respiration, observe the following:
(a) DO NOT ATTEMPT TO REMOVE CLOTHING ADHERING TO THE BURN.
(b) If help is available or as soon as artificial respiration is no longer required the wound should be covered with a DRY dressing.
(c) Oil or grease in any form should NOT be applied.

## Further details of charts and books on artificial respiration may be obtained from:

The Royal Life Saving Society, 14 Devonshire Street, Portland Place, London, W. 1

1. This Technical Manual is intended to ensure satisfactory operation of Marconi equipment over its working life. It is intended for use by skilled technicians who have had adequate basic training in this general type of equipment, and does not aim to provide information for basic training. This type of information is only included where new or complicated techniques are used. Those sections dealing with day to day operation are, however, specially written with the needs and experience of operating staff in mind.
2. Marconi Technical Manuals are normally divided into Sections and Chapters; each chapter is sub-divided into numbered paragraphs. Illustrations and circuit diagrams are located imnediately following the final chapter. Each manual includes consolidated lists of those parts which are replaceable in the event of failure. These lists, which are cross-referred to the individual diagrams, define each part fully in terms of a Marconi part reference number, which may be used for ordering spare parts. A glossary is available from Central Division (price 5/-) giving NSN references where available.
3. This manual includes an amendment record sheet. Amendments will normally be by the issue of replacement pages and drawings. On these, changes in the text will be indicated by means of a heavy line in the margin alongside the amended material. Where the amendment relates to a modification, the equipment should be checked to see if the modification has been incorporated before the manual is amended.
4. The equipment covered by this manual is subject to modification control. The Modification State of the Equipment sheet defines the modification zones into which the equipment is divided, and shows the modification state of each zone to which the manual relates. Manual amendment will be in terms of modification state and equipment should be checked before manual amendments are made.

Modification Record Labels are fitted to the units of the equipment listed below. Embodiment of a modification is indicated by scoring through the relevant number on the appropriate label.

The amendment state of this manual is related to the modification state of the equipment. To ensure that this relationship may be determined at any time, the following table is re-issued with successive amendments to the manual.


## V321 SERIES <br> VIDICON CAMERA CHANNEL

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## Chapter 1

## INTRODUCTION

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## INTRODUCTION

7. The Vidicon Camera Channel Type V321 comprises a Camera Type V3211 and a Camera Control Unit Type V3215, V3216 or V3217 depending upon the application. In addition to these basic units a number of ancillary units may be supplied to increase the versatility of the channel in specialized applications.
8. The channel is almost completely transistorized, the CCU being constructed in modules in which the majority of components are mounted upon printed wiring boards which are readily removed for ease of servicing.
9. The channel is designed to give an extremely high performance with long-term stability of operation.
10. The camera uses a vidicon tube, the type depending upon whether a rugged or light-duty application is required (see equipment characteristics). The camera is an extremely compact unit having a cylindrical construction and is normally fitted with a mounting block designed for fixing on a standard tripod.
11. The stainless steel cover is sealed at both ends to make it dust and moisture proof and the addition of a simple waterproof lens cover to the front of the camera makes it suitable for operation in unfavourable weather conditions.
12. The lens mount is designed to take the Broadcast or C type lenses, a simple adaptor insert being provided to convert from the former to the latter.
13. A manual focus control is provided on the camera and where desired it may be replaced by an electrical focus drive (optional) operated from the Control Unit. When manual focus is used a focus lock is provided for fixed focus applications.
14. To increase the light-handling range of the camera a neutral density lens filter assembly may be fitted and a sun shutter may be used to protect the vidicon tube from intense light sources. An electrical feature of the camera is the 'High Flux Mode' of vidicon operation providing a much sharper focused beam giving an improved resolution with a consequent improvement in signal/noise ratio since less aperture correction is required for a given resolution.
15. Three types of Camera Control Unit are avaiiable. They are:-

Type V3215 This is a free-standing ruggedized unit which is either airtight or forced ventilated. The printed boards are clamped to the frame ensuring relizbility under vibration and acceleration.
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Type V3216

Type V3217

## INTRODUCTION

This is a 19 in ( 48.5 cm ) rack mounted unit.

This is a rack mounted unit designed for airborne applications and is of similar construction to $V 3215$ but complying with ARINC Specification 404.
10. The Camera Control Unit houses the video processing circuits, the timebase circuits and the synchronizing circuits. The operational and preset controls are mounted on the front panel of the control unit. Provision is made for fitting the additional controls for remote optical focus and sun shutter/filter selection. The preset controls are fitted with a protective cover to prevent accidental disturbance.
11. Connection from camera to control unit is made by means of a multicore cable which may be up to 1000 ft in length. A cablecompensation circuit in the camera control unit provides correction to the video signal for the length of camera cable employed.
12. The timebase circuits may be driven from standard external drive pulses (broadcast applications) or by internal generators having no fixed relationship between the line and field frequencies, giving a random interlace, but with the necessary facilities for crystal controlled line oscillator and mains locked field timing.
13. In applications where it is necessary to have a fixed relationship between the line and field frequencies to produce an accurately interlaced picture, synchronizing circuits may be installed in the Control Unit. This unit can then be arranged to drive other channels. A shading generator may be fitted to give an optimum quality of picture when operating the camera at high light levels with vidicon tubes not having a separate mesh connection and also to provide an auto-alignment output to ease the adjustment of the alignment controls.

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## Chapter 2

## EQUIPMENT CAARACTERISTICS

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## EQUIPMENT CRARACTERISTICS

## Iaputs

1. (a) Power

The camera will operate from the following suppliess-

| $100-125 \mathrm{~V}$ | $200-250 \mathrm{~V}$ |
| ---: | :--- |
| $100-125 \mathrm{~V}$ | $48-62 \mathrm{~d}$. |
| 24 V |  |
|  | $+6 \mathrm{~V}-200-250 \mathrm{~V}$ |

Power consumption 50-60VA.
(b) Synchronizing Pulses

Line Drive, Field Drive, Mixed Blanking, Mixed Sync
(o) Looking Signal

> Standard negative pulses -6 dB . to +l2 dB ref. 2 V peak-to-peak. High impedance, bridging output. 6.3V RMS into 3,300 ohms.

## Outpute

2. (a) Vision

IV to 1.5 V composite or equivalent non-composite into 75 ohms.
(b) Synchronizing

Pulses from internal sync pulse generator Line Drive, Field Drive, Mixed Blanking, Mixed Sync.

Standard negative pulses $2 \mathrm{~V} \pm 2$. dB into 75 ohms for use with other channels. Equalizing pulses are not incorporated in the mixed sync signal.

NoTE: No pulse outputs are available when the channel is operatod from the simple internal pulse generator giving unrelated line and field frequencies.

## Performance

3. All performance figures are quoted for operation on 525/625 line systems. Although the channel is designed to operate in an ambient temperature up to $55^{\circ} \mathrm{C}$ the performance specified is obtainable at ambients in the range $20^{\circ} \mathrm{C}-30^{\circ} \mathrm{C}$. Outside this range the degradation of circuit performance is negligible compared with the performance of the Vidicon.

## Semsitivity

4. The channel is designed to operate, with the performance specified, under the following conditions. The specified Vidicon is a 7263A, P831, or equivalent.
(a) Low Light-level condition (Vidicon sensitivity at maximum).

Scene highlight brightness: 3 ft L.
Lens aperture: T 2.8
Signal Current:
$0.1 \mu \mathrm{~A}$
Dark Current:
$0.2 \cdot \mu \mathrm{~A}$ approximately.
(b) 'Average' Light-Level condition

Scene hightlight brightness: 50 f't L.
Lens aperture:
T 2.8
Signal Current:
$0.3 \mu \mathrm{~A}$
Dark Current:
$0.02 \mu \mathrm{~A}$ approximately.
Sensitivity will be reduced when Vidicons of a less sensitive type are used, e.g. 7038, P810, etc. The average light-level conditions are those for which other aspects of the performance are specified below. A T.T.H. 3 cm Vidital lens is used.
5. Resolution

Centre Resolution:
(Average tube with 750 V on focus electrode).

Corner Resolution:

Limiting Resolution:

Loss at 400 T.V. lines per picture height less than 6 dB without aperture correction. With aperture correction full modulation may be achieved at 500 lines per picture height.

Loss at 400 lines less than 4 dB below centre resolution depending upon the type of vidicon tube employed.

Bandwidth limited ( $9 \mathrm{Mc} / \mathrm{s}$ ) on all standard systems except 405 lines which will resolve 800 lines per picture height in the centre.

## 6. Vision amplifier

(a) H.F. response

> Flat $\pm 0.5 \mathrm{~dB}$ to $8 \mathrm{Mc} / \mathrm{s}$
> -3 dB at $9 \mathrm{Mc} / \mathrm{s}$
(b) Aperture correction:
(c) Hum on vision signal:

Phaseless correction with peaking frequency adjustable according to system. Amount of correction variable up to 12 dB at 600 lines/ picture height.
R.M.S. hum output at least -55 dB ref. l. OV peak-to-peak vision output.

## Automatic sensitivity

7. Using the parameters given in para. 4 sub-item (b) above, a variation of scene highlight brightness from $10,000 \mathrm{ft}$. L. to 10 ft . L does not cause the peak vision output level to alter by more than $40 \%$ ref. 1.0 V . When subjected to this change the circuit re-establishes itself in approximately $l$ second. Operation in the condition quoted in para. 4 sub-item (a) reduces the above brightness figures by a factor of approximately $3: 1$.

## Automatic dark current compensation

8. If the Vidicon dark current changes from zero to $0.2 \mu \mathrm{~A}$ the shift in level of picture black information is not more than $15 \%$ ref.l. 0 V .

## Contrast correction

9. It is possible to apply a contrast correcting law of $\gamma$ (gamma) <l to improve observation of scenes of exceptionally high contrast.

## EQUIPMENT CHARACTERISTICS

## Lone tern stability

10. During 7 days continuous operation in the conditions quoted in para. 4 sub-item (b) there is no significant change in picture quality on a picture monitor. The picture black level and peak vision signal output does not change by more than $15 \%$ ref 81.5 V . During this period the ambient temperature may vary between $20^{\circ} \mathrm{C}$ and $50^{\circ} \mathrm{C}$, the mains input by $+\mathbb{\%} /-10 \%$ and the scene brightness between 20 ft . L. and 1000 ft . L.

## Imanity to pulse variations

11. Input pulse amplitude variation of $\pm 6 \mathrm{~dB}$ about the nominal and width variation of $\pm 1 \%$ of nominal do not cause a visible change of picture levels on a picture monitor. Superimposed hum up to $30 \%$ of pulse amplitude on line drive or field drive ( $15 \%$ for blanking and syncs) causes no visible effect when the output is observed on a picture monitor.

## 15. ScanninE circuite

(a) Standards.

The channel will operate on the following scanning standards either internally or externally driven:-
(i) 405 lines, 50 field 2:1 interlace.
(ii) 525 lines, 60 field $2: 1$ interlace.
(iii) 625 lines, 50 field $2: 1$ interlace.
(iv) 819 lines, 50 field 2:1 interlace.
(v) 875 lines, 60 field $2: 1$ interlace.
(vi) The above standards, but with no fixed relationship between line and field frequencies, and single field pulse only.
NOTE: Where no fixed relationship exists between line and field frequencies, the actual number of lines may vary between the number quoted above and half that number. Internally generated systems do not have equalizing pulses but othervise can be set to conform to C.C.I.R. widths and timings.
(b) Amplitude.

With nominal blanking periods the Vidicon scan sizes are adjustable over the range $15 \%$ of nominal.
(c) Stability.

With a mains input variation of $+7 \% /-10 \%$ of nominal and an ambient temperature variation from $20^{\circ} \mathrm{C}$ to $50^{\circ} \mathrm{C}$ the scan size or position does not change by more than $3 \%$ of nominal scan size. A limit of $2 \%$ of scan size is independently applicable to the warm up period in an ambient temperature of $20^{\circ} \mathrm{C}$.

## (d) Positional scanning errors.

The maximum displacement of any picture point from the ideal is less than $1 \%$ of picture height or width. The maximum error builds up over not less than $1 / 3$ rd picture height or width.
(d) Positional hum

Less than $0.1 \%$ of picture height or width.
13. Transistors, etc.

NOTE: All transistor types and quantities are liable to alteration.

Camera. Vidicon 1 inch types with magnetic focus and deflection.
Input stage: 7586 Nuvistor. (R.C.A. 7586)

| Commercial Type | C,V, Type | American Equivalent |
| :---: | :---: | :---: |
| 4-BSY 27 | - | 2N708 |
| 3-AFZ12 | 7335 | 2N1495 |
| 1-BFY 18 | - | 2N2484 |
| 1-0C205 | - | 2N1475 |
| 1-Al704 | - | 2N2893 |

C.C.U. (Less S.P.G. Boards)

| 1-2N | 711 | - | 2N1495 |
| :---: | :---: | :---: | :---: |
| 3-BFY | 17 | - | 9N2477 |
| 3-AFZ | 12 | 7335 | 2N1495 |
| --2S30 |  | - | 2N2551 |
| 10-BSY | 27 | - | 2N708 |
| 14-ASY | 27 | 7087 | 2N1305 |
| I-OC | 23 | 7054 | 2N1908 |
| 4-0C | 28 | 7085 | 2N2870 |
| 1-0C | 35 | 7084 | 2N2870 |
| 1-0C | 44 | 7003 | 2N1305 |
| 13-0C | 84 | 7074 | 2N527 |
| $14-0 C$ | 140 | 7112 | 2N1302 |
| 3-0C | 202 | - | 2 N 1475 |
| 9-0C | 205 | 7188 | 2N1475 |

## P.U. Rectifiers

| Commerical Type | C.V. Type | American Equivalent |
| :---: | :---: | :---: |
| 4-20AS | 7045 | IN3194 |
| 2-80AS | 7356 | IN3196 |
| 1-40AS | 7013 | IN3196 |
| 4-8G7 | 7356 | IN3196 |
| 4-BYZ38-300 |  |  |

S.P,G, Boards

| 24-ASY 26 | 7004 | 2N1303 |
| :---: | :---: | :--- |
| 14-ASY 27 | 7077 | 2N1305 |
| 2-OC 76 | 7007 | 2N527 |
| 1-AFZ 12 | 7089 | 2N1495 |

14. Mechanical

Camra: $\quad 14.5$ in.
Diameter Weight
Camra: $\quad \begin{array}{r}14.5 \mathrm{in} \\ (37 \mathrm{~cm})\end{array}$


Wilth Depth Height Woight
V/215 Control Unit: $E$ in. 16 in. $10.5 \mathrm{in} 30 lbs.$.

$$
(20.5 \mathrm{~cm})
$$

( 41 cm ) $(26.7 \mathrm{~cm})$ ( 13.6 kg )
V3216 Control Unit: 19 in. 12 in. 7 in. 33 lbs. $(48.5 \mathrm{~cm})(30.5 \mathrm{~cm})(17.8 \mathrm{~cm})(15 \mathrm{~kg})$

Camera finish: Stainless steel case with blach anodized end plates.

Control units
finish: Two tone textured P.V.C. paint (Light and Dark Grey).

## Equipment List

15. The Industrial Television Camera Channel Type V321 comprises:1 - Industrial Television Camera Type V3211
Either l - Camera Control Unit V3215
or $\quad 1$ - Camera Control Unit V3216 (for rack mounting)
Cables required (subject to extra charge)
I - 37-way camera cable fitted with connectors:-
For use with V3215 or with V3216 having VBll-3216 back panel.
Either Straight Entry Soc et and Straight Entry plug. B99-1051-01. or Side Entry Socket and Straight Entry plug. B99-1051-03
or Straight Entry Socket and Side Entry Plug. B99-1051-04 For use with V3216 having VB10-3216 back panel

Either Side Entry Socket and Crimped Connectors. B99-1051-05
or Straight Entry Socket and Crimped Connectors. B99-1051-06
1 power cable with connectors:-
Either Straight Entry Plug and Straight Entry Socket (unscreened cable).

B99-1053-01
or Straight Entry Plug and Straight Entry Socket (screened cable).

B99-1053-02
or Straight Entry Plug and free end, (unscreened cable).

B99-1053-03
or Straight Entry Plug and free end, (screened cable).

B99-1053-04

The following features may be incorporated, subject to extra charge:-
Remote Focus Unit Type $\mathrm{V}_{4} 012$ Sun Shutter Assembly Type V4033
Neutral Density Lens Filter Assembly Type V4034
Fibreglass Sun Shield Type V4202
Waterproof Lens Cover Type V4281
Zoom Lens Type V4024
Shading Generator and Auto-Alignment Type B99-0033-01
Synchronizing Pulse Generator Types B99-0028-01 \& B99-0029-01

In addition, a Remote Control Unit can be supplied to provide for remote operation of the following features:-

Remote Focus
Neutral Density Lens Filter/Sun Shutter Operation
The remote control unit can house controls for operating Picture Polarity Revercal and Line Scan Reversal relays. Full details of these facilities are to be found in the Appendices. When a remote control unit is supplied a l9-way cable will be required with connectors as detailed below:-

Either Straight Entry Socket and Straight Entry Plug.
B99-1052-01
or Straight Entry Socket and Crimped Connectors.
B99-1052-02
or No Socket and Straight Entry Plug.
B99-1052-03
or Straight Entry Socket and No Plug.
B99-1052-04

# T. 6768 Part 1 <br> Sect.2.Chap. 1 

## Chapter 1

## MECHANICAL

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## mechanical

## Aeference should be made to Figs.119 and Figs.123-126.

## Canera tube

1. The camera uses a $5 \frac{1}{8}$ inch ruggedized Vidicon, type 7263-A or P831. These tubes are pipless and have a completely uniform photo-conductive layer. It is also possible to use the standard $6 \frac{1}{4}$ inch Vidicon with or without a side pip. The Vidicon heater supply is adjustable for a current requirement from 90 mA to 600 mA with a camera cable up to 1000 f't long.

## Camera

2. The camera is housed in a cylindrical case $3 \frac{1}{2}$ inch ( 8.8 cm ) in diameter and $14 \frac{1}{2}$ inch ( 37 cm ) long excluding the lens and cable connector. Space is provided for the remote focus motor, sun shutter and filter solenoids without the necessity for fitting additional external components. It is possible, however, to reduce the length by 2 inch for special applications if remote focus is not required. For manual focus an extension shaft is fitted to the focus drive and this shaft protrudes from the rear of the camera to provide manual control. A focus lock is provided. The case is dust and moisture proof. Inlet and outlet connections may be provided for forced cooling or pressurization by conditioned gas, when required. An over-temperature indicator may also be fitted.
3. As a result of operating the Vidicon focus electrode at 750 V the line scanning current generator is housed in the camera. The maximum dissipation in the camera is approximately $13 W$ when a Vidicon with 600 mA heater is used. This reduces to approximately 10 watts when a 90 mA heater is used. The maximum ambient temperature is limited to $55^{\circ} \mathrm{C}$. A sealed multi-way outlet is fitted to give access to the camera for inter-communication and to provide power for a limited number of camera accessories.

## Camera control unit

4. The Camera Control Unit (CCU) is transistorized with the exception of the Vidicon H.T. stabilizer and includes all circuits necessary to produce a 1.5 volt composite, or equivalent non-composite, vision signal. The mobile unit Type V3215 is housed in a case approximately 8 inch ( 20.5 cm ) wide $\mathrm{x} 10 \frac{1}{2}$ inch ( 26.7 cm ) high $¥ 16$ inch ( 41 cm ) deep. The case is sealed, all cable connectors being situated on the front panel. The printed wiring boards are mounted vertically and are held rigid to the structure by bolts with spacers fitted to the boards. The power supply unit is removable from the main structure and is available in versions suitable for operation on $50 / 60 \mathrm{c} / \mathrm{s}, 400 \mathrm{c} / \mathrm{s}$ and d.c. mains. Operation direct from lightweight storage cells is also possible.
5. The V3216 version of the CCU is designed to fit a standard 19 inch rack. The printed wiring boards are plugged in from the front and occupy the left-hand side of the unit. Provision is made for an extension board (for test purposes) to be retained in a socket at the extreme left-hand end of the unit. The power unit and panel controls form a separate unit occupying the right-hand side. This unit is plugged into two multi-way connectors mounted at the rear of the case. Access to the panel controls is obtained by removing the escutcheon which is attached by four captive screws. All cables are brought into the rear of the unit and two methods of connection are possible as follows:-
(a) Plugs and sockets, as on the mobile version, using back panel VB11-3216-01.
(b) With no back panel, wired to the existing sockets.

The Power Supply Unit (PSU) is removable from the main structure and is available for operation from $50 / 60 \mathrm{c} / \mathrm{s}$ mains only.
6. The only exposed controls are the ON/OFF switch and accessory controls when fitted. All circuits are designed for excellent long and short term stability including automatic compensation for variation of ambient illumination and temperature.

On the heavy duty unit, setting-up controls, which will need adjusting when a Vidicon is changed, are located under a hinged sealed cover at the top of the front panel. Air inlet and outlet connections may be provided to allow forced cooling or pressurization, especially at high altitudes. A number of cases exist to suit various environments. These include:-
(a) Sealed sheet metal case Type V4230.
(b) Ventilated sheet metal case Type V4232.
(c) Sealed cast case with fins Type V4231.

All cases will provide space for the inclusion of a circulating fan to improve cooling and ambient capability. An over-temperature indicator can also be fitted.

## Camera channel accessories

7. The mechanical design of the camera allows the inclusion of an optional remote focus motor and/or neutral density lens filter and sun shutter with operating solenoids. Focusing may be carried out at two rates to suit the focal lengths of lens in use. The shutter is a 'fail safe' device which will protect the Vidicon when the camera is not powered and may be used in conjunction with a photocell unit to provide automatic protection against exposure of the vidicon face to the sun.

The front casting of the camera is removable to allow easy attachment to the camera body of externally fitted accessories, e.g. lens turret, zoom lens and special optical systems. The addition of a simple lens protecting cover makes the camera suitable for a wide range of environmental conditions without further protection.

## Chapter 2

## PRINCIPLES OF OPERATION

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## PRINCIPLES OF OPERATION

Reference should be made to the block diagram Figs. 101 and 102.

1. The Industrial Canera Channel Type V32l comprises the Vidicon Camera Type V3211 and its associated Camera Control Unit Type V3215 (mobile) or V3216 (rack mounted).

## Canera

2. The camera houses the vidicon pick-up tube V2, its deflection and alignment coils, the head amplifier and the line scan generator. The output from the target of the vidicon is applied to the input stage of the head amplifier which consists of a Nuvistor (V) and a transistor (VTI) in a cascode circuit. This circuit gives a good signal to noise ratio and is followed by three amplifiers (VT2-7) in cascade and an emitter follower output VT8 feeding the coaxial line in the camera cable at a level of 250 mV for a signal current of $0.3 \mu \mathrm{~A}$.
3. The scanning waveform applied to the line deflection coils is generated from the line drive pulses fed from the control unit which are used to fire a silicon controlled rectifier circuit.
4. Shading and blanking waveforms are combined by VT9 and MR9-11 and are fed to the grid and the cathode of the vidicon tube.

## CAMERA CONTBOL UNIT

## Video amplifier

5. The video amplifier in the Camera Control Unit amplifies and processes the signal from the camera to produce a standard level signal at the output, which should always be terminated in 75 ohms.
6. The video amplifier stages are mounted on two printed wiring boards Video 1 - B99-0038 and Video $2-B 99-0037$, with functions as indicated in the following paragraphs.

## Video 1 (B99-0038)

7. The Hum Stripper stage (VTI), removes hum on the signal from the camera introduced by different a.c. potertials between the camera and camera control cases.
8. The Aperture Corrector stage (VT3-VT5) provides a high frequency boost to the signal to improve the overall resolution of the channel and is followed by an inverter stage (VT6) from which either a positive or negative polarity picture may be selected.

## PRINCIPLES OF OPERATION

9. To compensate for the frequency attenuation characteristic of the coaxial Jine in the camera cable the cable length corrector stage VT8 provides a boost which is preset by the CABLE CORRECTION control RV2 to correct for the length of cable in use.
10. The corrected signal is further amplified by VT9, VTIO and an emitter follower output VTIl feeding the Video 2 board.
1l. The Video 1 board also incorporates a clamp pulse generator (VT13-VT15, VT7) and a camera blanking mixer circuit (VTI6-19). In addition to providing clamp pulses to the line clamp VTl on Video Board 2 , the clamp pulse generator also feeds an output to the video amplifier VT9, VTIO to provide a positive black level on the signal which is clear of any spurious noise.
11. The LINE SCAN RESET transistor VII2 provides an output to protect the line scan generator on the camera should the silicon controlled rectifier $X 1$ stick in the $O N$ condition when switching on or changing sync. sources. VTl2 and SCRI are only fitted on early camera channels.

## Video 2 (B99-0037)

13. The input to the Video 2 board is an emitter follower VT2 in which the blaci level of the signal is established by the line clamp VTl.
14. The emitter follower is followed by a blanking mixer and clipper VT3. Blankine pulses are provided by the blanking generator VT7-VT8 and are mixed with the video signal to provide the necessary blanking during the flyback periods.
15. The clipper circuit establishes the black level on the signal such that when the synchronizing pulses are mixed with the signal through the sync. clipper VT9, VT10 and the sync. mixer, (VT4,VT5) a composite standard level signal is provided from the output (VT6).
16. A sampling signal from the output stage is fed to the auto-target circuit (VTII, VT12, VTI7 \& VTI9) which provides an automatic sensitivity correction for changes in the light level at the photo-conductive surface of the vidicon.
17. The auto-black level circuit VTI3, VTI4 and VTI5 provides automatic compensation for changes in dark-current from the tube.
Field scan B99-0031
18. The scanning circuits of the camera may be operated from the following sources:-
(a) Intermally generated drive pulses.
(b) Externally senerated drive pulses.
(c) Under a random interlace condition where there is no fixed relationship between line and field frequencies.
When using internal or external drive pulses, line drive, field drive, blanking and sinc. should be terminated in 75 ohms. When using random interlace these pulses should not be terminated.

## PRINCIPLES OF OPERATION

19. Field drive and line drive pulses are fed into the Field Scan Generator board. The field drive pulses operate a field delay circuit VTl, VT8,VT9,VT10, VTll, which makes possible an adjustment to the delay between the start of the field scan and blanking in order to remove the characteristic white line on the raster at the bottom of the field.
20. The output from the field delay circuit operates the field sawtooth generator (VT2-VT4) and the scanning current for the deflection coils is obtained from the Field Scan Output stage consisting of VT5 and VT6 operating as a complementary pair. The scanning waveform is taken to the scanning coils via a bridge resistance network which is supplied with a d.c. potential for centring the raster on the tube.
21. Line drive pulses to trigger the line deflection circuits are taken via a buffer stage VTI2 to a phase inverter VII5 which supplies three outputs of $+5 \mathrm{~V},-5 \mathrm{~V}$ and -2 V , respectively. The -2 V output provides the drive pulses to operate the silicon controlled rectifier or the transistor on the line scan generator of the camera via VTI6.
22. The vidicon tube is protected from target damage in the event of scan failure by the scan protection circuits VT17-VT20. The field scan waveform is rectified and fed to the scan protection circuit. The d.c. voltage for charging the capacitor in the line scan generator is taken via a potential divider network, and a voltage from this potential divider is also taken to the scan protection circuit. Failure of either, or both, the field and line scan circuits will cause a change of d.c. level at the protection circuit. The protection circuit provides the d.c. return for the vidicon power supply circuit VT8-VT9 and the resulting change of d.c. level at the protection circuit switches off the generator, thus removing all the supplies to the tube with the exception of the heater supply.
23. Under the simplest conditions of operation, without synchronizing generator, the camera channel is operated on a random interlace system. In this case part of the field delay circuit is converted (by means of internal links) to a free-running multivibrator which may, if desired, be mains locked. The line frequency is generated by means of a crystal controlled blocking oscillator and there is no fixed relationship between the line and field frequencies.

## Shading generator B99-0033

24. This unit produces a shading waveform and an auto-alignment waveform. The shading waveform is a combined line and field parabola which is fed to the vidicon to compensate for beam landing errors on the target which would cause deterioration of the ricture when using tubes not having a separate mesh connection. The field component of this waveform is generated by the field frequency parabola generator (VTI, VT2) triggered from the output of the field sawtooth generator; the line component is generated through the line frequency sawtouth generator (VT3-VT5) and the line frequency parabola generator and mixer VT6.

## PRINCIPLES OF OPERATION

The mixed shading signal is amplified by VT7, VT8 and fed to the grid and cathode electrodes of the vidicon tube through the emitter follower VT9 to correct any shading on the output of the tube.
25. The automalignment waveform is to facilitate the correct alignment of the beam as it emerges from the gun of the tube.
26. A pulse from the field scan board, at field frequency, is applied to the field drive switching stage VTIO whose output is then divided to half frequency by the automalign bi-stable multivibrator VIII, VTI2. The alignment pulses are then fed to the wall and mesh electrodes of the Vidicon through VTI3 and produce a rotational movement of the picture if the beam is not correctly aligned. This movement is minimised by the correct setting of the alignment controls.

## syac pulse senerator

Reference should be made to the Block Diagram Fig. 102.
27. The Sync Pulse Generator consists of the two boards B99-0028 and B99-0029 which are fitted when an accurate interlace is required.
28. The first board contains a master oscillator running at twice the line frequency of the system. This oscillator may be locked to the $50 / 60 \mathrm{c} / \mathrm{s}$ mains frequency or, alternatively, may be crystal controlled. A divide-by-two circuit reduces the oscillator output to line frequency and a series of binary counters act as frequency dividers. These counters, together with the counters on the input of the second board, reduce the line frequency signal to field frequency. The second board also contains the shaper circuits to form the line drive, field drive, mixed sync and mixed blanking pulses.

## Power supply

29. Power for the equipment may be supplied from the $50 / 60 \mathrm{c} / \mathrm{s}$ mains. V3215 and V3217 CCUs may be supplied from a $400 \mathrm{c} / \mathrm{s}$ supply, a d.c. supply, or from a battery source. The output is a smoothed d.c. supply which is applied to a stabilizer VTl-VT4.
30. The stabilizer provides outputs of -16.5 V and +4.5 V as reference supplies to the various boards in the channel. The combined output of 21 volts is taken, via a focus current regulator (VT5-VT7) to the focus coils and to the vidicon power supply VI8-VT9 which supplies all the voltages for the operation of the vidicon with the exception of the heaters.

## Remote control unit

31. The remote control unit has facilities for reversing the line scan and the picture polarity. A line centring potentiometer for reverse scan operation is also provided.

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## Chapter 1

## CAMERA

## Para.

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Head Amplifier 2

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3
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## CAMERA

## Reference should be made to the circuit diagram Fig. 103.

## General

1. The camera incorporates the vidicon pick-up tube, the scanning, alignment and focus coils, the line scan generator circuit, a circuit for feeding blanking (and shading, if provided), to the camera tube and a head amplifier board Type B99-0447. The optional facilities, Remote Focus Motor, Neutral Density Lens Filter and/or Sun Shutter may be added, if required.

## Head amplifier

2. The first stage is a cascode amplifier using a nuvistor triode valve VI and a transistor VII. In this way advantage is taken of the high input impedance of a valve having a gain roughly equivalent to that of a pentode valve. At the same time, partition noise is avoided by using a triode valve, and noise in the transistor is minimized by the negative feedback provided by the triode acting as an emitter load for the transistor. The base of the transistor is decoupled by Cl and the cathode resistor is bypassed by a small capacitor C4 to increase the amplifier bandwidth. The second, and succeeding stages, consist of complementary pairs of transistors. The second, third and fourth stages have gains of 7,4 and 11 respectively. The emitter voltage of the output transistor in each pair is stabilized by zener diodes MZ1, MZ2 and MZ3. A frequency-conscious network is connected between the second and third stages. This is to compensate for the falling frequency characteristic of the amplifier caused by shunt capacitance across the 56 K load resistor Rl into which the vidicon output is fed. The effective coupling impedance decreases as frequency increases until R20 is short-circuited by C9 and Cl0 in parallel. The inductor Ll tunes out the effect of the input capacitance of the final amplifier. The response of the amplifier is set up by the adjusting C9 and Ll. C9 is normally adjusted for minimum streaking after horizontal low frequency edges. The capacitor Cll is to compensate for tilt in the waveform caused by loss of low frequency response resulting from the interstage coupling capacitors. The final amplifier stage makes up for the loss of gain which occurs in the frequency response correction network. The output is taken from transistor VT8, connected as an emitter-follower. The coaxial cable carrying the output to the video gain control on the Camera Control Unit is terminated by a $75 \Omega$ load and the cable forms part of the emitter load of VT8. The output impedance tends to increase as frequency increases and capacitor Cl5 compensates for this effect.

## CAMERA

## Field scan

3. The resistors R37, R38 and the thermistor R36 form a temperature dependent circuit the resistance of which varies inversely to the resistance of the copper scan coils. Thus the resistance of the loop is held constant over a wide range of temperature. Because of this, and because the field scan generator produces a linearly rising voltage, a linear sawtooth current having a constant swing is obtained in the scan coils.

## Line scan

4. An ideal line scan coil appears as a pure inductance so that the required linearly rising scanning current is obtained when a rectangular voltage waveform is applied to the coils. Typical idealized waveforms are shown in Fig.1. below.


Fis. 1. Waveforms in ideal scan coils.
Because all coils include some resistance a constant voltage applied during the scan period, as indicated in Fig.l, would result in an exponential rise of current. The current would ultimately become constant but is interrupted by the flyback. To overcome this problem it is necessary to add a linearly rising voltage as indicated in Fig. 2.


Fis. 2. Idealised maveforme allowing for coil resistance.

In the scanning circuit on the Camera the sawtooth component of the scanning waveform is generated across TRI and the pulse across TR2. The two waveforms are added in the secondary windings and applied to the line scan coils.
5. A current from the +4.5 V line is taken, via the line scan reset circuit VII2 on VIDEO 1 board to the horizontal amplitude control (on CCU) and then to the camera where it is decoupled by C32. The capacitor C33 is charged via the primary winding of TRI. The resonant period of this path is very long, compared with the line period so that an almost constant current flows into $C 33$ during the scan period. Because of this a voltage sawtooth is developed across TRI primary and will be transferred to the secondary.
6. C 33 is discharged, at line frequency, through the primary winding of TR2 by the transistor VTIO or rectifier X1. This path has a resonant period approximately four times as long as the desired flyback time of the scan current waveform. The voltage on the secondary winding of TR2 is clamped by diode MR12 to the d.c. potential acquired by C34. After a few initial scanning cycles the capacitor C34 acquires a charge sufficient to clamp TR2 secondary at the end of the first quarter-cycle of oscillation of the C33-TR2-XI loop. This coincides with the end of the flyback period so that a substantially constant voltage appears across TR2 secondary during the flyback period. The sum of the sawtooth voltage across TRl and the rectangular voltage across $T R 2$ provide a

## CAMERA

voltage of the desired form as indicated in Fig.3.


Fig. 3. Addition of voltages to provide scan voltage.
7. RV1 should be adjusted so that the current in the secondary of TR2 just decays to zero at the end of the scanning period. RV1 oan be further reduced in value beyond this optimum by a small amount and, over this range, acts as a linearity control. Note that a change in the setting of RVI changes the scan amplitude. A change in the amplitude setting will not alter the linearity.

## Lime acan reversal

8. Line scan reversal can be obtained by operating relay RLA. The contacts change over to reverse the direction of current flow through the line scanning coils. Full details will be found in Appendix 3 .

## Shading and blanking

9. The shading waveform is applied to both grid and cathode electrodes of the vidicon while the blanking is fed to the cathode only. During blanking, transistor VT9 and diode MR10 conduct, but MR9 is cut off so that blanking does not reach the beam electrode. During the unblanked period the transistor VT9 is cut off and its colleetor is at -16.5 V . The instantaneous voltage at the output of the shading generator is always less than -16.5V i.e. nearer to earth potential and as a result MR9 will conduct and MRIO will cut off. Consequently the shading waveform will be fed to both grid and cathode electrodes.

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## VIDEO 1

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## VIDEO 1

## General

Reference should be made to circuit diagram Fig. 104.

1. The Video 1 board includes a hum stripper circuit, aperture correction, phase reversal circuit, cable correction amplifier, feedback amplifier and driver stage. Ancillary circuits incorporated are clamp pulse generator, camera blanking mixer and line scan reset circuit.

## Hum etripper

2. The camera output is fed, via a $75 \Omega$ gain control, to transistor VII to remove hum and other low frequency disturbances which may occur as a result of the camera and camera control unit frames being connected mechanically to points at different earth potentials. Spurious hum voltages which appear between camera and CCU earths are developed across R3 and are not applied across base-emitter junction of VTl. C6 is the only trimming control in the CCU video amplifier and is adjusted for flattest overall response. The output from VIl collector is taken to an emitter follower stage VT3 which is used to drive the aperture correction circuit.

## Aperture correction

3. The resolution of the vidicon tube is limited by the finite diameter of the scanning beam and can be improved by introducing a rising frequency response on the signal, whilst maintaining a linear phase response. Transistors VT3, VT4 and associated circuit provide the required response adjustment. An output from VT3 is fed through a $\pi$-section low-pass filter Ll, C9 and C10. A second output is taken from the slider of RVI to transistor VII, which has R13 as collector load. The output from VT4 is fed through capacitor C7 and combined with the output from the filter. The short time-constant of Rl3, C7, VT4 collector and VT5 emitter circuits, ensure that only the highfrequency components are fed via VT4. The signal at VT4 collector will be in anti-phase to the signal fed to the filter. The signal path from the collector of $V T \psi_{+}$gives a leading phase response by virtue of capacitor C7 while the signal path through the filter gives a lagging phase response as a result of inductor $\mathrm{L}_{4}$. At the junction of these paths the signals are combined to give a rising response with increase of frequency. The circuit is normally set up during test to give minimum h.f. boost (RVI fully anti-clockwise) and Ll adjusted to peak at $9.5 \mathrm{Mc} / \mathrm{s}$.

## VIDEO 1

## Picture polarity reversal

4. A conventional emitter follower stage, VT5, drives the phase reversal circuit associated with transistor VT6. This circuit has loads in both emitter and collector, i.e. R21 and R20 in parallel with R22, respectively. The slight difference in value is necessitated by the differences in output impedance. Polarity reversal is obtained with the aid of RLB. The contacts RLBI are shown in the normal position. Operation of RLB will invert the video signal.

## Cable correction

5. The RC network in the emitter circuit of VT8 provides a rising frequency characteristic to compensate for the falling characteristic of the cable. The amount of compensation may be adjusted by RV2. The potentiometer RV3 in the collector circuit of this transistor is an auxiliary gain control which is adjusted on test so that, with the main gain control at minimum, the vidicon target current is standardized at $0.3 \mu \mathrm{~A}$.

## Amplifier and clamp driver

6. A pulse is added to the signal at the output of VT8. A relatively small pulse is added with normal video polarity to ensure that any spurious signals during the dark current period do not affect the autoblack level circuit. With reversed picture polarity the black level is now represented by the peak signal so that to establish the black level a large pulse, greater than the peak-to-peak signal, is added. Contact RLB2 modifies the collector load of VI7 (shorting R65) and thus controls the amplitude of pulse added to the video signal after the cable correction circuit.

The major part of the gain is obtained from a complementary pair. of transistors VT9 and VTIO. The bandwidth can be extended, if required, by putting C23 in parallel with R34. This will have the effect of decreasing the negative feedback on VT9, at high frequencies. The output from VTIO is taken to Video 2 through an emitter follower stage VT11.

## Line scan reset. VT12

7. The silicon controlled rectifier which provides the line scanning waveform is normally switched off by the pulse which appears at its anode. Should this pulse fail to turn the device off, as could possibly happen during a change of line drive with the unit switched on, the rectifier could 'stick' in the fully conducting condition. The transistor VTI2 and associated circuit is designed to prevent this from occurring. If the silicon controlled rectifier goes into continuous conduction the voltage across R39, R40 will become more negative; the base voltage of VT12 will be greater than the voltage acrous MZl and the transistor will conduct. This will actuate RLA, the contact RLAI
will open and the circuit to the silicon controlled rectifier on the Line Scan Generator will be broken. Once the circuit is broken VTl2 base voltage will return to normal, the transistor will cut off and the relay contacts close again. The whole operation is comp.eted within a few lines. The potential divider R39, R40, is also used to provide the voltage which operates the scan failure protection circuit. If the scan fails the voltage at the junction of R39, R4O will become less negative and operate the protection circuit to stop the h.t. generator. When VTIO in the camera is fitted, VTl2 is not used.

## Clamp pulse generator

8. Negative line drive pulses are applied to $\mathbf{C 2 4}$ and differentiated by C24, R 41 . Transistor VTl3, which is normally conducting, will be cut-off for a period determined by the differentiating circuit. A positive pulse will appear at the collector and will be d.c. restored by diode MR12. Transistor $\mathrm{VTl}_{4}$ is held cut-off by the voltage drop across P 44 and is switched on by the trailing edge of the pulse at VII3 collector. The resulting positive pulse at VTIU collector produces a pulse across L2 which switches VT15 into conduction for a period determined by L2. The output pulse at VT15 collector is timed to occur during the dark current period for all lengths of cable. It is approximately 2 microseconds wide, and is negative going. Transistor VT7 supplies the pulse which is added to the signal after the cable correction stage to ensure that clamping is not affected by spurious signals occurring during the dark current period. Where picture polarity reversal facilities are provided contact RLB2 of relay RLB short circuits R 65 to reduce the pulse amplitude for pictures of normal polarity.

## Camera blanking

9. Field pulses are fed to emitter follower VTM6, and the output is mixed with line drive pulses fed via MR14. The mixed blanking signal is amplified by VTl7 and fed to a complementary pair VTI8 and VTI9 which form the output stage. The output stage is switched from cut-off to the bottomed condition and drives a common base stage in the camera which blanks the cathode of the vidicon. The transistor VTI7 is bottomed to such an extent that the trailing edge is slightly delayed and this ensures complete blanking of the line scan waveform. The start of camera blanking is delayed with respect to the start of system blanking. The camera blanking pulse suffers additional delay when very long camera cables are used so that the end of the pulse may occur later than the end of system blanking. Under these conditions it is advantageous to restrict camera blanking to the minimum width. The pulse can be shortened by breaking the link between tag No. 52 and tag No. 53.

## Chapter 3

## VIDEO 2

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Auto Black Level Circuit
Fig.

Auto-Target Circuit

## VIDEO 2

## General

Reference should be made to circuit diagram Fig. 105 and Fig. 118.

1. The circuit functions of the Video 2 board are as follows: the dark current tips of the signal are clamped, the signal is then blanked and a black level established, controlled manually or automatically, as required; a peak white clipping circuit follows which may, alternatively, be used to provide gamma correction; sync pulses are then added and a composite signal fed out of the unit at an impedance of 75 ohms. Ancillary circuits on this board are the system blanking generator and the sync pulse clipper, circuits for automatic control of target potential and black level, and a shaper circuit for sync and blanking when operating under a random interlace condition.

## Black level clamping

2. The output of the Video 1 board (whech is negative signal for positive picture output) is clamped at the base of VT2, by VIT. The d.c. level is determined by the setting of the BLACK LEVEL control RV6 on the front panel. The level may be entirely manually controlled or be maintained automatically, at a preset level, by the AUTO BLACK LEVEL circuit. Fig.l is a simplified diagram showing the AUTO BLACK LEVEL circuit. The clamping pulse is generated on the Video 1 board and applied to the base of VII as a negative pulse during the dark current period. The clamp pulse will drive the collector of VTl (and the base of VT2) to a potential determined directly by the setting of RV6 (MANUAL) or to a potential determined by transistor VII5 (AUTO). Transistor VT2 is an emitter follower and an unblanked video output from the emitter is taken to a second emitter follower VIIl3. The output from VII3 is a.c. coupled to a gated d.c. restorer, diode MRI3. This diode is gated by transistor VTI4, which receives line and field frequency pulses. These gating pulses cut the transistor off during the dark-current period to d.c. restore the signal on the picture black or the vidicon mask. The unblanked video applied to MRl3 will therefore be d.c. restored to the potential at VTI4 emitter except during the vidicon blanking period. The signal is thus restored to the blackest part of the picture instead of to the dark current tips. This restoration level corresponds to 'true black' and any signal beyond this level represents the dark current. The signal is now peak rectified by transistor VT15 and the resulting potential used as the reference level for the clamp transistor, VT1. In this way the clamping level is automatically adjusted should the vidicon current change. Note, however, that the initial clamping level is still controlled by BLACK LEVEL CONTROL, RV6, which determines the potential at VTI4 emitter and hence the restoration level at diode MRI3. It is therefore possible to adjust the control to give any required set-up.


Fig. 1. Auto black level circuit.
3. The gating pulses for $\mathrm{VTI}_{4}$ are obtained from field drive via MR14 and from line drive via VT16 and MRI5. The +5 V line drive is d.c. restored by diode MRI6, to the +4.5 V rail and taken, via MRl7, to the base of VTI6. Transistor VT16 is thus held cut-off between pulses until the base potential falls sufficiently to allow conduction to occur. A lengthened, negative, line frequency pulse, greater in width than camera line blanking, is produced at VT16 collector and fed to VT14 via MRI5. This method of gating VT14 produces d.c. restoration to blacks which are inside system blanking but outside the gating pulse period and is achieved by linking tag No. 6 to tag No.7. In practice, the method results in a constant reference level because the scanned area includes the mask in the vidicon tube mount. The mask will not appear in the final picture because system blanking removes this part of the video information. Alternatively tag No. 6 may be linked to tag No. 8 and the gating pulses to VII4 will be system blanking. The d.c. restoration now takes place on the blackest part of the picture. This is the normal condition but the former method will be advantageous when viewing, say, an all white surface.

## Black level and peak white clipping

4. Emitter follower VT3 acts as a buffer between the clamping circuit and the clipping circuits. Positive going system blanking from VT8 cuts off MR3 during the blanking period and MR4 acts as black level clipper. The positive side of MR4 is returned to zener diode MZ2 which also supplies the reference potential for black level setting. The video information will thus be eliminated during blanking by MR3 and any signal more positive than the reference potential at the junction of MR4 and R9 will be removed by MR4. The level at which peak white clipping occurs is determined by MR5 and the setting of potentiometer RV3. However, MR5 acts as a peak white clipper only when tags 15 and 16 are short-circuited. When R10 is included, as shown on the circuit, gamma correction is provided. The level at which correction starts is determined by the setting of RV3 while the amount of correction depends on the value of RlO.

## Output atages

5. VT4 and VT5 form a conventional feedback pair having a high input and a low output impedance. The emitter of VT4 is a suitable point for the addition of sync from VTIO via the sync amplitude control RVI. VT6 is an emitter follower whose output impedance is built out to $75 \Omega$ by R21 and C8. The capacitor C5 provides a boosted l.f. response to enable a reasonable value to be used for the output capacitor C 23 on the main chassis.

## VIDEO 2

## Blanking and sync pulse clipping

6. VT7 emitter follower, feeding VT8, provides a high input impedance and prevents variations of input level affecting the blanking amplitude. Negative blanking pulses at its base make VT7 conduct, VT8 is therefore cut off and positive going pulses appear on its collector. VI8 is prevented from bottoming by MR9 which conducts when the collector of VT8 falls below the potential at the junction of R24 and R25, giving a defined blanking width. The output waveform is thus not delayed by hole storage effects. VT9 provides a high input impedance and is prevented from bottoming by diode MRIO. The transistor is normally cut-off; negative sync pulses cause conduction but its collector is not able to rise above the potential set by zener diode MZ1. The current in VT9 is limited by R28. Clipping of the pulses to VTIO in this way prevents it bottoming and a negative sync pulse of constant width appears at its collector.

## Auto-target circuit

7. The Auto-Target circuit, shown on Fig.2, maintains a constant output level over wide changes of scene brightness and may be operated either from the blanked signal at VT4 emitter or the unblanked signal at VII3 emitter. The signal is d.c. restored to approximately earth potential by MRI2 which is returned to earth through VIII. VTI7 can be cut off during system blanking so that d.c. restoration occurs only during the picture period. Where positive picture only is being used the blanked signal at VT4 emitter is preferred for operating the AutoTarget circuit. Where negative pictures are being used, or where picture polarity reversal facilities are provided, it is preferable to use the unblanked signal at VT13 emitter and to gate VIIl7 with system blanking.
8. The transistor VTMI and the capacitor C14 form a peak rectifier circuit and, effectively, measure the amplitude of the video signal. The potential to which C14 is charged, in conjunction with the setting of RV2, determines the potential at VTI2 collector. In the AUTO position of AUTO-TARGET switch SWE on the CCU the collector of VTl2 is connected, via the artificial earth line, to the vidicon cathode. As a result any changes in signal amplitude will alter the cathode potential. The vidicon target is returned to earth potential so that changes in cathode potential will produce a corresponding change in signal current. The control RV2 is adjusted during test to give a video output at the CCU of $1 \mathrm{~V}, 0.75 \mathrm{~V}$ or 0.7 V dependent on the value of Rl 5 . Dark current limiting may be incorporated by linking tag No. 36 to tag No.37. The transistor VT19 is fed with unblanked video and the level at which the transistor conducts is determined by the setting of RV4. When VII9 conducts the potential at VTI2 base will be limited so that the target potential is reduced and prevents the vidicon overrunning the maximum target current specified by the manufacturer of the vidicon tube. Limitation of vidicon output is advisable as a result of the wide range of target voltage available when operating the camera using automatic target control.


## Chapter 4

## FIELD SCAN

## Para.

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## FIELD SCAN

## General

## Reference should be made to circuit diagram Fig. 106 and 118.

1. The field scan board incorporates a circuit to delay the start of field scan and thus mask the characteristic white line which occurs at the bottom of the picture when using vidicon pick-up tubes. Alternatively, when the camera is operated under random interlace conditions, the delay circuit may be operated as a free-running multivibrator. Details of random interlace operation are given in Section 3, Chapter 6. The output from the delay circuit is used to operate the field scan generator and the resulting sawtooth is taken to the output stage. The board includes a line pulse buffer circuit and an inverter stage. The line pulse buffer may be converted to a crystal controlled oscillator when using random interlace. In addition a scan protection circuit removes the h.t. supplies to the vidicon in the event of scan failure.

## Delayed field drive

2. Transistors VT8,VT9,VTIO and VTll are used to provide a field scan pulse delayed by a predetermined time. The transistors VT8 and VT9 form a monostable multivibrator which is triggered by the negative Field Drive input pulses. The period of the multivibrator may be varied by means of RV4. The rear edge of the output from VT8 is used to trigger the monostable multivibrator formed by VIIO and VTII. The duration of the output pulse is chosen to be similar to the field drive and is fed to the base of VTI. VII is a high input impedance, non-bottoming, stage which provides a current pulse to base of VT2. VT2 bottoms and a negative pulse of approximately 17 volts appears at VTI collector. A camera blanking output is taken from the collector while MRI ensures a good rear edge for this output.

## Field scan

3. VT2,VT3 and VT4 form a bootstrap scan generator. The scan voltage is generated by charging C3,C4,C5 and C6 through the HEIGHT control, R7, RV1 and R8. VT2 acts as a switch to discharge the capacitor when the 17 volt negative pulse from VTl arrives. RVI determines how effectively C3 to C6 are discharged during the time VT2 is switched on. This slightly alters the voltage waveform at the emitter of VT2 in the ratio of 'spike to sawtooth'. Adjustment of RVI alters the sawtooth linearity at the start of the scan and is effective during the first few milliseconds only. VT3 and VT4 act together as an emitter follower. Normally, in such a circuit, there would be no emitter resistor in VT3. However, in this circuit, amplitude changes with temperatures make Rll necessary. Feedback from the emitter circuit of VT4 is taken to the HEIGHT control. As the gain of an emitter follower is almost unity the voltage across $R 7$ and the HEIGHT control remains almost constant

FIELD SCAN

throughout the sweep period. The charging current for C3 to C6 is thus almost constant so that a high degree of linearity is obtaineत. A further improvement in linearity is obtained by taking a feedi'zok path via RV2 and R10 to the junction of C5 and C6. The feedback voltage is integrated across C3 and C5 and will have opposite curvature to the waveform across $\mathrm{C}_{4}$ and C6. By adjusting RV2 the resultant output can be made linear. An output to the shading generator is taken from VT4 emitter and is preset to give the correct ratio of line to field parabola. The Field Scan output uses a complementary pair, VT5 and VT6. These are biased to Class A by the zener diode MZl and the emitter resistors $\mathrm{Rl}_{4}$ and Rl 5 . The output to the scan coils is taken between the emitter of VT6 and the -16.5 V rail via the centring circuit.

## Line pulse buffer and inverter

4. Line drive input pulses from Sync Pulse Generator No. 2 or an external source are fed to VTl2. VTl2 is a high input impedance, nonbottoming amplifier stage. The collector waveform is clamped at -7 volts by the 5 volt zener diode MZ2. VTI5 is a phase inverter which provides low impedance outputs of -5 V at the collector and +5 volts at the emitter. A -2 volt output is also available at a tap on the collector resistor. The transistor VTIG is a driver stage which provides a current pule for triggering either VT1O or XI, whichever is fitted. The collector of VTI6 is connected to VTIO or XI in the camera via 035 in the CCU. VTI3 is used only on random interlace.

## Scen protection

5. The vidicon is protected against scan failure by removing the h.t. voltages from its electrodes. These voltages are all supplied by a push-pull transistor oscillator controlled by VTl7. In the normal condition, with field and line scan operating, VTI8, VT19 and VT20 are cut off whilst VTIT is conducting. VTI9 and VT20 are held cut off by d.c. voltages derived from the field scan generator and line scan protection circuit respectively. Base current for VTI8 is obtained from the common collector load, R59, of VT19 and VT20, so that as long as these latter transistors are off VTI8 remains of'f and VTl7 is able to conduct.
6. If the field scan should fail VTI9 will conduct and VTI8 collector will assume earth potential and remove the base current from VII7. This will cut off VTl7 and the oscillator will stop. Similarly if the line scan fails VT20 will conduct, VT18 collector will assume e'irth potential, VTll will cut off and the oscillator will stop.
7. To ensure that VT17 is held in conduction under normal conditions a positive 14.5 V supply is taken from the oscillator, through MRI2, to VTl7 base.

M23 and R53 supply base current to the oscillator and ensure correct starting conditions if field and line scan are present. During scan failure MZ3 prevents current flowing through R53, the voltage across the zener network in this condition being insufficient to allow conduction.

## Scan protection rectifier circuit

8. Rectifiers $M R 4$ and MR5 with aapacitors $C 9$ and ClO form a cascade doubler to rectify the field scan waveform and generate the field scan protection voltage. During the negative-going part of the field scan waveform, VT7 is conducting and the charging path for C9 is via VT7, R16 and MR4. Cl0 will also charge via MR5 and Rl7. During the positive going period of the field scan waveform VT7 will stop conducting but a current will pass through MR3. MR4 will now be reverse biased but Cl0 will continue to charge via MR5, Rl7, C9, R16 and MR3. During conducting periods of VT7 the input impedance will be given approximately by Rl6 times the current gain of the transistor, i.e. about 500 ohms. During non-conducting periods of VT7, the impedance is approximately equal to Rl7, i.e. 560 . The circuit thus provides a constant impedance at point T 5 and does not affect the field scan waveform. The output from ClO is fed to the scan protection circuit (see Part l, Sect.3, Chap.5).

## Chapter 5 <br> CAMERA CONTROL UNIT

## Para.

$50 / 60 \mathrm{c} / \mathrm{s}$ Power Supply Unit and Stabilizer ..... 1
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Focus Current Regulator ..... 5
Auto-Target ..... 6
Wall Focus and Auto-Align ..... 8
Width, Height, Alignment and Centring ..... 9
Line Centring and Scan Reversing ..... 10
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## CAMERA CONTROL UNIT

## Reference should be made to circuit diagrams Figs. 107 and 108 and the interconnection diagrams Figs. 114 and 115.

## 50/60 c/s Power supply unit and stabilizer

1. AC mains is connected to the unit via plug PLA and fed to double pole on-off switch SWAl. Both neutral and line are fused by FSI and FS2 respectively. Mains transformer TRl primaries may be connected in series for operation on 200-250 volt supplies or in parallel for operation on 100-125 volt supplies. The secondaries of TRI supply the a.c. for the vidicon heater, a 7.5 volts supply for internal mains lock and the a.c. for the bridge rectifiers MRI to MR4. The output from the rectifier is taken to the reservoir formed by C2 and C3 in parallel and then to the series regulator transistors VT1 and VT2. These are connected in a composite circuit which provides a high gain and thus gives much greater control than could be obtained with a single transistor, while still retaining a low impedance. The base of VTl is directly connected to the collector of VT3, the control transistor. The base of VT3 is held at a fixed potential relative to the -16.5 line by zener diode MZ2 while the emitter potential is fixed with reference to the +4.5 volt line by zener diode MZ3. Any change in the potential difference between the -16.5 volt and the 4.5 volt lines will thus alter the emitter-base voltage of VM3, change the collector voltage and alter the impedance of VT1-VT2.
2. The earth line is taken from the emitter of transistor VT4. As a result any load placed between earth and the -16.5 volt line will draw current through emitter resistor R8 while a load between earth and +4.5 volt line will draw current through VI4. In either event a change in the load current will alter the emitter voltage of VI4. Because the base voltage is fixed by zener diode MZ2 changes in load will alter VT4 emitter-base voltage and consequently the transistor impedance. The collector current for VI3 is normally supplied from a tapping on inverter transformer TR2 which supplies power for the vidicon. The a.c. is rectified by MR7 and filtered by Cll, R5 and C5. This method of supplying current to VT3 ensures good regulation over the maximum range of imput voltages. However, should the field or Iine scan fail the scan protection circuit will stop the oscillator associated with TR2. Power for the inverter is obtained from the stabilizer. If the stabilizer should fail, an alternative supply to VT3 is made available, via MR5, direct from the bridge rectifier MRI to MR4. When the inverter is operating, MR5 is reverse biased so that VT3 collector supply is isolated from the bridge rectifier
3. Decoupling is provided across the -16.5 volt lines by C8. Two other negative outputs are taken from the -16.5 volt line, a -5.5 volt supply stabilized by MZ5, and a -12.5 volt supply, stabilized by MZ6 and decoupled by C7.

## Inverter

4. A number of d.c. supplies, particularly those for the Vidicon, are obtained from a push-pull common-emitter chopper comprising transistors VT8, VT9 and transformer TR2. The bases of these transistors are returned to the scan protection circuit and the oscillator will stop if either of the scanning circuits fail (see Chap.4.para.7). Power for oscillator is obtained from the regulated output of transistors VTI and VT2. The circuit diagram shows the d.c. supplies for the vidicon. Approximately 400 V positive are provided for the accelerating anode from a winding on TR2 via rectifier MR10 and reservoir capacitor $\mathrm{Cl}_{4}$. The negative side of this supply is referred to as ARTIFICIAL EARTH and the vidicon cathode resistor is returned to this line. The target is returned to the true earth and is maintained positive with respect to cathode by a manual control or by the AUTO-TARGET control transistor. A conventional cascode doubler using capacitors Cl5 and Cl6 and rectifiers MRll to MRI4 has its output added to the 400 volt accelerating anode supply. The total voltage is about 750 and is used to supply the wall focus electrode. The supply for the control grid is obtained from half-wave rectifier circuit MR9 and reservoir Cl3. Two other supplies are obtained from secondaries on TR2; a 14.5 volt supply, rectified by MR15 and filtered by Cl7 and a lOOV supply, rectified by MR8 and filtered by C12, R25 and C24.

## Focas carrent reculator

5. Variations in focus current are prevented by transistors VT5, VT6, VT7 and associated circuit.VT5 and VT6 in a 'Super-Alpha' pair connection forms a series regulator controlled by transistor VT7. The supply has previously been stabilized and may be assumed constant. The emitter voltage is maintained constant by zener diode $\mathrm{MZ}_{4}$. If the focus current tends to increase, the voltage drop across Rll will inorease and make the base of VT7 more negative. The resulting increase in current through VT7 will cause the collector voltage to fall, i.e. to go less negative. VT7 collector is directly coupled to VT5 base and if the base voltage of the composite pair is reduced their effective resistance will increase and bring the focus current back to normal. Under conditions of low input voltage and long cables the supply to the focus regulator may be taken from the unregulated supply.

## Auto-target

6. In the $O N$ position of the auto-target switch SWE, the artificial earth is linked to the true earth by the auto-target control transistor which is situated on the video 2 board. This transistor is part of a potential divider which includes R15 and R37, and is connected across the 400 volt d.c. supply. The difference of potential between artificial earth and true earth i.e. between the vidicon cathode and target, is thus dependent on the base potential of the control transistor. This, in turn, is controlled by the brightness
of the scene being viewed by the camera. (For a description of the circuit see Sect.3, Chap.3). The auto-target circuit is so arranged that an increase in scene brightness causes an increase in the current through the control transistor and, as a result, a reduction in target volts.
7. Under conditions of very low brightness it is possible that the target potential could rise undersirably high. The control RV16 limits the maximum target voltage. This is necessary with vidicon tubes which run into secondary emission before the maximum available target voltage is reached. In this condition a Vidicon tube output commences to fall with increase of target voltage thus making it necessary to restrict the maximum range with auto-target operation. The diode MR16 is arranged to clamp the target at a limiting potential which is determined by the setting of the potentiometer RV16. Under normal conditions the diode is reverse biased because the cathode is held more positive than the anode. However, should the target potential rise above the diode cathade potential the diode will conduct and the target volts will then be limited. As an alternative, manual control may be selected. The auto-target circuit is switched off by open-circuiting the control transistor collector and target volts are then set manualld by RV4.

## Wall focus and automalign

8. The focus voltage is applied across a potential divider network consisting of R13, RV3, R30 and RI6 and is stabilized by V1, SCl/800. The slider of RV3 is taken via R2l to the wall focus electrode. Under normal operating conditions R21 is short-circuited by the AUTO-ALIGN switch SWF. An electromagnetic focusing system causes the electrons in the eleotron beam to come to a focus over a helical path. Thus, in a combination of electromagnetic and electrostatic focusing, as used in the vidicon, a change in Beam focus volts will cause the picture to rotate through a small angle. The function of the alignment coils is to ensure that the beam leaving the gun is accurately aligned with the axis of the tube. Adjustment of the alignment is achieved by altering the alignment and focus controls until an alteration in focus volts does not move the centre of the picture. To simplify this operation a square-wave from the auto-align generator, at half field frequency, may be superimposed on the focus voltage by switching the autoalign switch SWF to ON. Adjustment of alignment can now be made without recourse to adjustment of the focus volts.

## Width, height, alignment and centring

9. The WIDTH and HEIGHT controls are rheostats in series with the respective scan generators. Adjustment of the controls alters the amplitude by altering the charging voltage available. flignment current is obtained by connecting potentiometers RVII (X ALIGN) and RV12 (Y ALIGN) between +4.5 V and -5.5 V . The sliders are taken to the $X$ and $Y$ alignment coils and the common returns from the coils are taken to earth. Thus a current may be passed through soils in either

## CAMERA CONTROL UNIT

direction, depending on the setting of the controls. Field centring is obtained from a bridge circuit which includes R17 to R2O and potentiometer RV7. Field blanking makes it necessary to offset the bridge slightly in order to obtain similar shifts in each direction. The scan current from the FIELD SCAN GENERATOR is fed to the scanning coils via C 20 and C 21 in series and returned via the -16.5 V line. R18 is by-passed by Cl9 to provide a low impedance path for the scan current.

## Line centring and scan reversing

10. The facilities for scan reversing and for line centring operate in conjunction. Scan reversal is obtained with the aid of a doublepole changeover switch in the remote control unit which operates a relay RLA in the camera. As can be seen from figure 103 the relay contacts simply reverse the direction of current in the line scan coils. The relay is energized in the reverse-scan position of the switch. Two separate line centring controls, RV13 for forward scan and RVI4 for reverse scan, are connected between a positive and negative supply.

## Picture polarity reversal

11. The PICTURE POLARITY REVERSAL switch SWH operates relay RLB on Video 1 . The contact RLBl changes the video connection from the collector to the emitter of VT6 thus reversing the polarity of the signal.

## Remote optical focus

12. Provision for remote focus is made by means of the motor $X 3$ on the camera. This motor is controlled by SWC and SWD, giving two speeds of operation. These speeds are obtained by putting zener diode MZ1 in series with the supply to the focus motor. This has the effect of reducing the motor speed by supplying a reduced voltage, but maintains a high starting torque as relatively large currents can flow without a significant change in voltage. Switch SWC short-circuits MZl to provide a higher speed. Switch SWD reverses the supply polarity to drive the motor in the opposite direction.

## Sun Shutter/filter

13. To protect the Vidicon when not in use a sun shutter can be provided in the camera. A neutral density lens filter may also be fitted to extend the light handling range of the camera. These are operated by solenoids which are switched at either the CCU or remote Control Unit. The unregulated d.c. supply is taken to switch SWB which is a double-pole changeover switch with an off position.

## $400 \mathrm{c} /$ and $22-30 \mathrm{~d}$ d.c. Power supplies

Reference should be made to Figs.112, 113, 131 and 132.
14. Alternative power supplies are available to make operation possible from $115 \mathrm{~V} / 200 \mathrm{~V} 400 \mathrm{c} / \mathrm{s}$. (VB02-3215) or from $22-30 \mathrm{~V}$ d.c. (VB03-3215). Both units use the same basic chassis and the main difference between them is that the $22-30 \mathrm{~V}$ d.c. version incorporates a transistorized chopper circuit. In both circuits the transformer TRI has two secondaries each connected to a bridge rectifier circuit. The outputs from the unit are filtered and taken out on corresponding terminals to those used on the $50 \mathrm{~d} / \mathrm{s}$ power supply unit. The d.c. version supplies a $400 \mathrm{c} / \mathrm{s}$ supply to TRI with the aid of VII, VT2, transformer TR2 and associated circuit. TR2 provides feedback from collector to base of each transistor and the circuit acts as a push-pull oscillator. The circuit differs from the usual push-pull d.c. converter in that the small drive transformer TR2 is allowed to saturate while TRI steps up the output to the required value. When the supply is connected one of the transistors (say VTI) will conduct, owing to unbalance in the circuit, causing its collector voltage to swing by an amount almost equal to the supply voltage. The resulting voltage aoross TRl is applied to TR2 via R4 and R5. When TR2 saturates the primary current will increase rapidly and because of $\mathrm{R}_{4}$, R5, the applied voltage will fall. This will reduce the drives to VTl, decrease the collector current and consequently reverse the polarities to all the transformer windings. VTl will now be driven rapidly to cut off and VT2 will become bottomed. The cycle of operations will now repeat at a frequency determined by TR2 and the value of $\mathrm{R}_{4}-\mathrm{R} 5$. To ensure starting the transistors are biased into conduction by diode MR10 and resistor R1. MRI protects the circuit against accidental connection of incorrect supply polarities.

## Chapter 6 <br> RANDOM INTERLACE

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## RANDOM INTERLACE

Reference ohould be made to ciroutt diagram Fig. 105 and 106 to 118.

1. In the random interlace condition there is no fixed relationship between line and field frequencies. The crystal is fitted and connected to the field scan board where it controls the line frequency generator. The field frequency may be free running or locked to the mains.

## Line drive generator (Field scan board)

2. The crystal is connected between CI9 and VTI2 collector, and VTI2 operates as an oscillator at twice line frequency. The output is fed to VTI3 base. This stage, which is not used in the driven condition, is a blocking oscillator which divides by two, the division ratio being controlled by RV6 and the pulse width by RV5. The output winding of the blocking oscillator transformer is connected to VTl5 which drives VII6 and the line scanning circuit in the normal way.

## Field pulse generator VT8 and VT9

3. The delay multivibrator is converted to a field frequency, free running oscillator. The frequency is controlled by RV4. To obtain this condition linkages are required as shown in Table 4 of Part 2 Sect. 2 Chap.1. A mains locking voltage may be obtained through the filter R28, L3, C25 in the power supply. The circuit of VT8 and VT9 is then as shown in Fig.1. An output is taken from VT8 collector and fed to VTIO as in the normal circuit.

Sync. circuit video 2 board
4. All the facilities available on direct drive are incorporated on random interlace. Sync is obtained by mixing line and field pulses at MR22 and MR23, T33 and T34 are linked. The mixed signal is delayed by L1, C25 in order to provide a front porch. The link T27-T28 is necessary to feed the mixed line and field pulses into the sync pulse clipper. It should be noted that terminations must not be fitted to the drive coaxial sockets. The link between $T 41$ and $T 43$ provides the correct operating condition for VT9.

Blanking, Video 2 board. VT7 and VT8
'. T2j and T24 are linked and the combined line and field waveform is applied to VT7. As the field pulse is not wide enough for blanking the pulse is applied to MR11, R52. The leading edge passes through diode MRII but the diode cuts of $f$ on the trailing edge. C27, therefore, has a large effect on the trailing edge which is given a slow rise time VT18 clips the waveform at a level which will give a wise output pulse. This pulse is added to the blanking waveform by linking T25 and T26. C23 lengthens the line pulse to the required line blanking width.


Fig. 1 Field frequency multivibrator circuit (Randen Interlace)

# T. 6768 Part 1 <br> Sect.3.Chap. 7 

## Chapter 7

## SHADING GENERATOR

## Para.

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## SHADING GENERATOR

Reference should be made to circuit diagram Fig. 109.

## General

1. The shading generator board provides a waveform for application to the vidicon tube to counteract the beam landing errors which give rise to horizontal and vertical shading when vidicons without a separate mesh connection are used. The correcting signal is a composite parabolic waveform at line and field frequency together with a line sawtooth of either polarity. In addition to the above, the shading generator includes the multivibrator which provides the square wave at half field frequency for auto-alignment of the beam in the vidicon tube.

## Shading generator

2. Each parabolic waveform is obtained by integration of a sawtooth. A field frequency sawtooth is fed to VTI base and integrated at the collector by $\mathrm{R} 5, \mathrm{R} 4, \mathrm{C} 3$ and C 4 . The resulting parabola is transferred to emitter follower VT2 and a high impedance is maintained by feedback via C2. A line frequency sawtooth is generated across $C 7$ which is charged from the +4.5 rail. The incoming 5 V negative line drive pulses are differentiated by C5, R9 and the positive going spike switches VT3 on. The resulting negative pulse at the collector is squared and limited by MRI and used to switch VI4 on. VT4 thus discharges C7 at line frequency and the resulting sawtooth waveform is applied to VT5 base. The collector output is integrated by R10, R16 and C9 to form a line frequency parabola. The collector supply to VT5 is taken from the emitter of VT2 so that both line and field parabolas appear at the base of VT6. VT7 amplifies the composite parabola and following this, line sawtooth is added before final amplification in the output stages VT8 and VT9. There is a choice of polarity of line sawtooth at VTM4 and the relative amplitude of this and the parabolic waveform may be set up by the preset controls RV2 and RV3. The output transistor VT9 is an emitter follower feeding a load of 2.8 K in. the camera. The maximum peak-to-peak amplitude of composite signal across this load is 12 volts. The shading output is controlled by switch SWM on the chassis, this switch must be set to OFF when the shading board is not fitted.

## Auto-align generator

3. A half field frequency pulse is generated by the bistable multivibrator VTll and VTI2. This circuit requires a positive pulse so that VTlO is necessary to invert the incoming negative field pulse. The square wave generated by the multivibrator is passed to the output stage VTI3. This is a high voltage transistor operating from a l00V supply in order to provide a large amplitude square wave capable of producing the desired rotational effect on the picture.

## Chapter 8 <br> SYNC PULSE GENERATOR

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## SYNC PULSE GENERATOR

Reference should be made to circuit diagrams Figs. 110 and 111 and also the position of the various links on Fig. 118.

## S.P.G.1. Wanter oscillator and buffers

1. The Master Oscillator is a blocking oscillator built around transistor VT4. Feedback is applied from collector to base via transformer TRI which has a turns ratio of $4: 1$. The frequency of operation of the oscillator is governed by the time-constant of RV3, R20, Cl0 and Cll in the emitter circuit, and by the potential applied to the base of VT4 through R17 and the transformer winding 3-1. This potential is provided by the control transistor VT3 on mains lock only and is adjusted by means of RVI to correct the master oscillator frequency. A d.c. control voltage, derived from the discriminator transistor VT2, is applied to the emitter of VT3 to adjust the osoillator when locking to mains frequency. Internal mains lock is obtained by linking T26 to T 27 and T 4 to T 2 .
2. The width of the pulse at the collector is governed by the inductance in the circuit. The peak value of the current attained, however, is limited by RV3, R20. The interval between the pulses is controlled by the discharge time-constant RV3, R2O, C10 and Cll in the emitter circuit, while VI4 is cut-off. This is arranged so that the output at the collector has a mark-space ratio suitable for forming broad pulses in the mixed sync waveform. The diode MR4 limits the negative excursion following the positive pulse on the collector. R23, in parallel with the collector inductance, provides sufficient resistance to maintain a low value of $L / R$ and so enables the current to decay within the broad pulse period.
3. The positive output pulse from VT4 is coupled via R22 and R21 to buffers VT6 and VT5 respectively. These transistors are normally conducting and will both be driven towards cut-off by the input pulses. A positive-going output will be obtained at the emitters. These buffers are intended to isolate the master oscillator from the divider circuits thus preventing lower frequency components from modulating the oscillator.

## G.P.G.1. Crystal oscillator

4. Where an accurate reference with a high degree of stability is essential the master oscillator may be synchronized by a quart crystal oscillator providing a reference output of twice line frequency. The oscillator comprises VTI and associated circuit. The crystal is connected in the series mode between base and collector and gives an output of twice the line frequency of the system on which the unit is operating. Crystal control is obtained by linking $T 6$ to $T 7, T 8$ to $T 9$ und $T<5$ to T26.

## SYNC PULSE GENERATOR

5. The base of the transistor is biased by $\mathrm{R} 2, \mathrm{R} 3$ and the emitter by $\mathrm{R}_{4}$, decoupled by C3. The voltage swing on the base is sufficient to drive the transistor into saturation on the negative peaks and to cut-of $f$ on the positive peaks giving a resultant clipped sine wave of 8 volts peak-to-peak. This output is coupled via $C_{4}$ to the base of the master oscillator transistor VT4 which is thus synchronized to twiceline frequency. RV5 (Crystal lock) is adjusted to the centre of the range which locks the master oscillator to the crystal frequency.

## Count to field frequency (Counters 1 to 5)

6. The count from twice-line frequency to field frequency, which establishes the number of lines per field, is made by a series of ten binary counters arranged in two sections of five. Counters l-5 are on Sync Pulse Generator No.l (VT8-VT17). The remainder are on S.P.G. No.2. In each section feedback is applied to reduce the natural count to that required to produce the desired field frequency.
7. In a normal cascade arrangement of $n$ counters without feedback, the natural count of each binary unit is 2 giving an overall count of $2^{2 n}$. By injecting a pulse from the output binary to the input, or to an intermediate stage within the section, the count is reduced by a factor depending upon the position in the counter chain to which the feedback pulse is applied. If the pulse is applied from output to input the count is reduced by 1 , applied to the second counter it is reduced by 2 and to the third by 4 etc. In general, where the feedback is applied to the $\mathrm{m}^{\text {th }}$ counter, with a suitable delay in the feedback path, the overall count ' $C$ ', becomes :-

$$
c=2^{n}-2^{m-1}
$$

and if, in addition, feedback is applied to the $p^{\text {th }}$ counter the overall count becomes :-

$$
c=2^{m}-2^{m-1} 2^{p-1}
$$

The feedback connections are made by means of links on the printed wirine boards, the connections to which are shown at the bottom of the circuit diagram (see Figs. 110 and 111). The arrangement of the feedback connections changes according to the system on which the unit is being employed.
8. In the first section the feedback pulse is taken from the collector of VTl6 in counter 5 and is applied to the earlier stages through the delay network L2,R67, C34. The purpose of the delay network is to ensure that the feedback occurs shortly after the normal transition in the counter stage to which it is being applied and so causes the counter to revert to the state preceding the normal trigger. The output of the counter chain is taken from the collector of VTl7 and is fed to the second section in S.P.G.2. via pin 2 on the boards connector.

## S.P.G. 1 Frequency control and mains lock circuit

9. The Frequency Control and Mains Lock circuit consists of a Discriminator VT2 and Control Transistor VT3 which supplies a d.c. potential to control the frequency of the Master Oscillator. VT2 operates as a bi-directional switch with a mains frequency sine-wave applied to the collector, either from an internal, 7.5 V source, supplied by mains transformer TRI, or an external 6.3 V source. The voltage is supplied via Tl or T 2 to T 4 and then via R12 and R8. A third terminal T3 earths the collector of VT2 to give a free running condition.
10. During the intervals between field pulses, VT2 is conducting heavily since the base is returned to -6 V through R 7 . In this condition the transistor presents a low impedance to the sine-wave applied to the collector since the potential between emitter and collector is only a few millivolts. When a positive output pulse at field frequency is applied to the base of VT2 the incoming sine-wave is sampled for the duration of the pulse since the transistor is cut-off for this period. A current builds up in the coil 11 which is a function of the voltage at the junction R8 and R10. This coil has a very large inductance and integrates the current pulses appearing at the emitter of VT2 to build up a d.c. which is applied to the emitter of VT3. This d.c. modifies the normal current flowing into the emitter of VT3, which is defined by the manual frequency control RVl, being either added to, or subtracted from it.
11. The current flowing from the emitter to the collector of VT3 provides a voltage at the collector which is transferred through the diodes MR2, MR3, the resistor R17 and the winding of TRI to the base of the Master Oscillator transistor VT4. This voltage is normally adjusted by RVI to provide a base voltage of +0.5 V . As the field frequency pulses from the output of the counter chain vary their phase with respect to the incoming sine-wave so a varying voltage is applied to the base of the oscillator.
12. This change of voltage causes the oscillator frequency to change until the field frequency output of the counter chain pulls into the same frequency as the incoming mains signal and the two signals become locked. When the free-running field frequency is close to the mains frequency the pulse is phased approximately at the centre of the sinewave and no current is delivered to the control circuit. The freerunning frequency of the Master Oscillator is governed mainly by the setting of the FREQUENCY control RVI and it is essential that this control be set to approximately the correct position. To maintain the field component locked to the mains frequency the control circuit provides a range of oscillator frequency $\pm \%$ about the frequency determined by the FREQUENCY control. A convenient point for monitoring the locking signal is provided by the test point $T 5$ situated near to Ll .

## S.P.G. 1 Divide-by-two stage

1;. The Divide-by-two stage includes the blocking oscillator VT7 and the counter circuit MR5, MR6, C14 and C15. Twice-line frequency pulses from buffer VT6 are fed through capacitor $\mathrm{Cl}_{4}$ to d.c. restoration diode MR6 whose positive end is supplied from RV5 between +4.5 V and earth. The d.c. restored pulses are fed to the reservoir capacitor Cl5 through the second diode MR5. The capacitance divider $\mathrm{Cl}_{4}$, Cl 5 is appropriate to divide-by-two, i.e. the blocking oscillator is triggered on alternate input pulses. The blocking oscillator provides +ve output pulses whose width is approximately equal to that of line blanking for the system upon which the unit is operating. This width is determined mainly by the primary inductance of transformer TRI and the collector resistors RV4 and R26. RV4 is adjustable to accommodate the several line standards available.

## S.P.G. 2 Count to field frequency, (Counters 6 to 10)

14. Irput pulses from the Synchronizing Pulse Generator No.l are fed via Cl. The binary units are similar to those in the first section. Delay for the feedback is provided by Ll, R103 and C20. Tables l, 2, 3,4 and 5 summarise the count in each section, the feedback paths being used, and the overall count achieved in each section as a result of the feedback.

Table 1. 405 Line standard

| Section | 1st | 2nd |
| :---: | :---: | :---: |
| Counters in Section | 2nd to 5th (4) lst Counter Not Used. | 6 th to 10 th (5) |
| Applied Feedback | 5 th to 2nd (4th Counter to lst of section) | 10th to 6th and 8 th ( 5 th Counter of section to lst and 3 rd counters of section. |
| Feedback Connection | T24-T23 | T5 - T4 and T2 |
| Tags | $\begin{aligned} & \mathrm{T} 20-\mathrm{T} 18 \\ & \mathrm{~T} 15-\mathrm{T} 12 \end{aligned}$ | T8-T9 |
| Count without Feedback | $2^{4}=16$ | $2^{5}=32$ |
| Count with Feedback | $16-1=15$ | $32-4-1=27$ |

Table 2.
525 line standard

| Section | 1st | 2nd |
| :---: | :---: | :---: |
| Counters in Section | 1st to 5th (5) | 6 th to 10 th (5) |
| Applied Feedback | 5th to 4 th (2nd and lst of section) | 10th to 6th, 7 th and 8th (5th to $3 r d, 2 n d$ and lst of section). |
| Feedback Connection | T 24 to T 23 | T 5 to $\mathrm{T} 4, \mathrm{~T} 3$ and T 2 |
| Tags | T 21 to $\mathrm{T} 20, \mathrm{~T} 18$ and T 17 T 15 to $\mathrm{TH}_{4}$, <br> T13 to T12 | $\begin{aligned} & \mathrm{T} 6-\mathrm{T} 7 \\ & \mathrm{~T} 8-\mathrm{T} 9 \end{aligned}$ |
| Count without Feedback | $2^{5}=32$ | $2^{5}=32$ |
| Count with Feedback | $32-8-2-1=21$ | $32-4-2-1=25$ |

Table 3. 625 line standard

| Section | 1st | 2nd |
| :---: | :---: | :---: |
| Counters in Section | 1st to 5th (5) | 6 th to 10th (5) |
| Applied f'eedback | 5th to 3rd (2nd and lst of section) | 10th to 8th, 7th and 6 th ( 5 th to 3 rd , 2nd and lst of section). |
| Feedback connection Tags | T24-T23 <br> T20 to T19, <br> T18 and T17 <br> T15 to TII <br> T 13 to T 12 | $\begin{gathered} \mathrm{T} 5 \text { to } \mathrm{T} 4, \mathrm{~T} 3 \text { and } \mathrm{T} 2 \\ \mathrm{~T} 6-\mathrm{T} 7 \\ \mathrm{~T} 8-\mathrm{T} 9 \end{gathered}$ |
| Count without Feedback | $2^{5}=32$ | $2^{5}=32$ |
| Count with Feedback | $32-4-2-1=25$ | $32-4-2-1=25$ |

Table 4. 819 line standard

| Section | 1st | 2nd |
| :---: | :---: | :---: |
| Counters in Section | Ist to 5th (5) | 6 th to loth (5) |
| Applied Feedback | 3rd to lst | 10th to 7 th and to 5 th and 4 th in lst section. Effectively 7 th to 4 th, $2 n d$ and lst of section. |
| Feedback Connection Tags | T23 to T22, T21 to T16. T20 to T17, T14 to T15 T31 to T12 | $T 1$ to $T 3$ and $T 5$ |
| Count without Feedback | $2^{3}=8$ | $2^{7}=128$ |
| Count with Feedback | $\begin{aligned} & 2^{3}-1=7 \\ & 8-1=7 \end{aligned}$ | $\begin{aligned} 2^{7}-2^{3}-2-1 & =117 \\ 128-8-2-1 & =117 \end{aligned}$ |

Table 5. 875 line standard

| Section | 1st | 2nd |
| :---: | :---: | :---: |
| Counters in Section | lst to 5th (5) | 6 th to 10th (5) |
| Applied Feedback | 3rd to 1st | 10th to 5th and 4th in lst section. Effectively 7th to 2nd and lst of section. |
| Feedback connection Tags | T23 to T22, T 2 to T16 T20 to T17 T14 to T15 T13 to T12 | Tl to T5 |
| Count without Feedback | $2^{3}=8$ | $2^{7}=128$ |
| Count with Feedback | $\begin{aligned} & 2^{3}-1=7 \\ & 8-1=7 \end{aligned}$ | $\begin{aligned} 2^{7}-2-1 & =125 \\ 128-2-1 & =125 \end{aligned}$ |

15. The remainder of S.P.G.No. 2 may be considered as a separate sheper unit which rovides four sets of output pulses as follows:-

Line drive<br>Field drive<br>Mixed Blanking<br>Mixed Sync

## S.P.G. 2 Field pulse M.V.

16. The output of the counter chain is taken from the collector of VT9 and is a square wave at field frequency. This output is fed, via C26 to the base of VT12. VTIl and VTl2 are connected as a monostable multivibrator which, in the stable condition, has VTll cut-off and VTl2 bottomed. The duration of the output pulse is normally determined by the timing capacitors C28 and C29, in conjunction with RVI. However, this tends to produce an indeterminate number of broad pulses. To overcome this problem a terminating pulse is obtained from an appropriate point in the counter chain and applied to the base of VT12. A link is required between terminals $T 6$ and $T 7$, if it is desired to operate with a fixed pulse width. If the link is removed the pulse width can then be varied by adjustment of RVI. The pulse at the collector of VTl2 is transferred to transistor VTl 3 which inverts the pulse before it is applied to VT25.

## S.P.G. 2 Field drive output

17. Field drive pulses are derived directly from the field pulse output transistor VT13. An output is fed, via C46, to transistor VT25 which inverts the pulse and provides fast edges. The resultant output at the collector is a negative pulse at field frequency which is used to drive the field scan generator and provide a $75 \Omega$ output for external use.

## Line drive output

18. Similar arrangements are made for obtaining line drive. Pulses at line frequency derived from the Divide-by-two stage in S.P.C.No.l are brought into S.P.G.No. 2 to the base of transistor VTI5, the line drive output stage. The inverted pulses developed at the collector are fed out to the field scan generator board and provide a 753 output for external use.

## mixed blanking

19. The mixed blanking signal comprises two sets of pulses, line blanking and field blanking. The line blanking pulses are produced by the divide-by-two circuit, the width of the output pulse from this circuit being suitable for direct use as a line blanking signal.
20. The field blanking is obtained from a monostable multivibrator built around transistors VT22 and VT23. The multivibrator is triggered by field frequency pulses from VTl3. This multivibrator is very similar to the field pulse m.v., the period is mainly controlled by capacitors $\mathbb{C}_{4} 3$ and C44 but may be adjusted by RV3. The output is taken from VT22 collector, diode MR18 and resistor R90 ensure a sharp negative transition.
21. The line and field blanking pulses are combined at the base of Blanking Output Stage VT24. The line blanking signal is fed through C45 to the base of VT24 and, being positive pulses, cut off VT 24 during the pulse. Between pulses VT2 2 is bottomed due to the low value of base resistor R87. During the field blanking period the positive pulses from the collector of VT22 cause MR16 to conduct. This feeds sufficient current into the base resistor R87 to lift the base of VT 24 positive with respect to its emitter and so cut the transistor off. Between the field blanking pulses from the collector VT22, diode MR16 remains off as a result of the negative potential transferred through C4O from VT22 collector. VT24 is therefore cut-off during the line blanking pulses and for the duration of the field blanking period. The output from the collector is therefore a normal mixed blanking signal which is fed into an impedance of $75 \Omega$ through the series resistor R91.

## S.P.G. 2 Mixed sync

22. Line synchronizing pulses are obtained from the line frequency input by differentiation across the networks C33, R64 and RV2, and using the differentiated pulse to drive VT14. The positive pulses drive VT14 into cut-off but during the interval between pulses VTI4 is bottomed, the value of R64, RV2, being low enough to allow this. VT14 is cut-off for a duration equal to the width of a sync pulse. The resulting pulses appearing via the collector of VT14 are applied to the emitter of VIT16 where they are combined with the broad pulses fed from the timer unit as a twice line-frequency pulse to form the mixed sync signal. These broad pulses are gated into the signal at field-frequency by a gating pulse derived from the field-blanking multivibrator.
23. The field drive multivibrator provides a pulse which is applied to the circuit C39, R81, the latter having a sufficiently low value to ensure bottoming of VT20 between input pulses. The gating circuit consists of the two diodes MR14 and MRI5, which are driven by twice lineofrequency pulses from the timer and fieldafrequency pulses from VT20 respectively. The potential at the junction of R76 and R77 is such that $\mathrm{MRI}_{4}$ is conducting and sufficient current flows into R79 to cut-off VII9 between the broad pulses. However, during the period of each broad pulse from the timer, the poteritial at the junction of R76 and R77 is driven sufficiently negative to cut-off MR14. Similarly, MR15 is driven to cut-off during the period of the field sync pulse.
24. When either MRI4 or MRI5 is conducting sufficient current is applied through these diodes to drive the base potential of VT9 above that of the emitter and so cut the transistor off. The transistor cannot conduct, therefore, except during the period when pulses are applied to the two diodes during the field gating period and, within this period, for the duration of each broad pulse period. The output at the collector of VT19 consists of a series of positive-going broad pulses. Between these pulses VTI9 collector takes the base of VT16 sufficiently negative to cause VTl6 to conduct and combine the broad pulses with the line sync pulses.
25. VT16 is normally conducting but is cut-off either when VT14 is cut-off or, when its base is driven positive by the collector of VT19 during each broad pulse. During the active field period VTH is cutoff for the duration of each line sync pulse thus, in turn, cutting off VTl6 and causing the collector potential to fall to -6 V . During the field sync period the positive pulses applied to the base cut-off VT16, again causing the collector potential to drop to -6 V . The collector output consists, therefore, of two signals combined to form a mixed sync waveform with the pulses having an amplitude of approximately 6 V . This output is applied to the delay network C35,L2,C36 which delays the pulses, relative to the blanking output, to produce a front porch of approximately $1.5 \mu S$. The characteristic impedance of the delay network is approximately $3.3 \mathrm{k} \Omega$ so that resistors $R 68$ and $R 73$ are used to terminate the line at each end.
26. The delayed sync waveform is coupled to the base of VTl7 through C37. This transistor is normally cut off since the base is returned to earth, through R72, and is driven into conduction by the negative input pulses. These are of sufficient amplitude to make the transistor bottom. The collector of VTl7 then rises to approximately earth potential and gives an inverted signal across R74. This signal is coupled through C38, to the base of the sync output transistor VT18. C38 is large enough to prevent any tilt being introduced on the signal. The base resistor, R7l, is small enough to allow VTl8 to bottom between pulses. The output has been inverted again at the collector and is matched to a $75 \Omega$ co-axial cable by series resistor R69.


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HEAVY DUTY CAMERA Š́l SERIES
(VB00-3211-01)
(Refer to Master Components List T6768 List 1)
Uross Reference List
for VB00-32112 Sh. 1

| Ref. | Mo. | Rer. | мо. | Ref. | Mo. | Ref. | Mo. | Ref. | No. | Ref. | No. | Rep. | No. | Ref. | mo. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Cl | 13 | C19 | 5 |  |  | MR12 | 56 | R10 | 74 | R28 | 73 | R46 | 63 | V2 | -118 |
| C2 | 14 | C20 | $\square 8$ |  |  |  |  | R11 | 75 | R29 | 80 | R47 | 60 |  |  |
| C3 | 14 |  |  |  |  |  |  | R12 | 76 | R30 | 78 | R48 | 67 | VT1 | 105 |
| C4 | 22 | C22 | 9 | Ll | 42 | MZ] | 112 | R13 | 73 | R31 | 84 | R49 | 58 | VT2 | 106 |
| C5 | 15 | C23 | 1.1 .9 |  |  | MZ2 | 112 | R14 | 77 | R32 | 85 | R50 | 57 | VT3 | 107 |
| C6 | 16 | C24 | 5 |  |  | M23 | 112 | R15 | 73 | R33 | 86 | R51 | 88 | VT4 | 106 |
| C7 | 17 | C25 |  |  |  |  |  | R16 | 78 | R34 | 65 | R52 | 114 | VT5 | 107 |
| C8 | 15 | C26 |  | MR1 |  | PLA | 48 | R17 | 79 | R35 | 87 | R53 | 115 | VT6 | 106 |
| C9 | 26 | C27 |  | MR2 | 55 |  |  | R18 | 80 | R36 | 89 | R54 | 116 | VT7 | 107 |
| Clo | 18 | C28 |  | MR3 | 55 | R1 | 63 | R19 | 73 | R37 | 65 |  |  | VT8 | 106 |
| Cll | 19 | C29 |  | MR4 | 55 | R2 |  | R20 | 81 | R38 | 66 | RV1 | 117 | VT9 | 108 |
| C12 | 16 | C30 | 11 | MR5 | 55 | R3 | 83 | R21 |  | R39 | 68 |  |  | VT10 | 121 |
| C13 | 15 | C31 | 11 | MR6 | 55 | R4 | 71 | R22 | 82 | R40 | 62 | SKA | 90 |  |  |
| $\mathrm{Cl}_{4}$ | 20 | C32 | 10 | MR7 | 55 | R5 | 69 | R23 | 83 | R41 | 64 |  |  | X1 | 121 |
| C15 | 24 | C33 | 8 | MR8 | 55 | R6 | 70 | R24 | 74 | R42 | 62 | TRI | 104 |  |  |
| C16 | 21 | C34 | 12 | MR9 | 53 | R7 | 71 | R25 | 78 | R43 | 62 | TR2 | 104 |  |  |
| C17 | 15 | C35 |  | MR10 | 53 | R8 | 72 | R26 | 74 | R44 | 61 |  |  |  |  |
| C18 | 23 | c36 | 25 | MR11 | 54 | R9 | 73 | R27 | 75 | R45 | 59 | V1 | 109 |  |  |

- Or as specified by customer

MISCELLANEOUS ITEMS

| Bearing Block | No. 1 |
| :--- | :--- |
| Bearing Bush | No. 2 |
| Board Assembly (Head Amplifier) including: | No. 3 |
| $\quad$ Terminals | No. 101 |
| Bush | No. 4 |
| Circlip | No. 27 |
| Clamp Ring Assembly including: | No. 29 |
| $\quad$ Clamp Ring | No. 28 |

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        HEAVY DUTY CAMERA 321 SERIES
        (VB00-3211-01)
(Refer to Master Components List T6768 List 1)
    Cross Ref'erence List
        for VBOO-3211Z Sh.l
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MISCELLLANEOUS ITEMS (Contd.)

| Coil Assembly (Focus/Alignment) including: | No. 32 |
| :---: | :---: |
| Alignment Coil | No. 31 |
| Former | No. 40 |
| Split Ring | No. 93 |
| Coil Assembly (Field) including: | No. 33 |
| Coil Assembly (Vertical) | No. 36 |
| Heat Sink | No. 41 |
| Coil Assembly (Line) including: | No. 35 |
| Coil Assembly (Horizontal) | No. 34 |
| Collector Ring | No. 37 |
| Drive Screw | No. 38 |
| Focus Shaft (Manual) | No. 39 |
| Insulator (Stand-Off) | No. 43 |
| Knob (Fluted) | No. 44 |
| Lens Mount | No. 45 |
| Mounting Ring Assembly (Front) | No. 46 |
| Mounting Ring Assembly (Rear) | No. 47 |
| Plug Button for Lens Mount | No. 49 |
| Pot Core Assembly | No. 50 |
| Pot Core Assembly | No. 51 |
| Socket Assembly including: | No. 91 |
| Socket | No. 92 |
| Spring | No. 94 |
| Tag Board Assembly including: | No. 97 |
| Tag Board Assembly | No. 99 |
| Tag Board Assembly including: | No. 98 |
| Tag Board | No. 96 |
| Tag Board Assembly | No. 100 |
| Terminal | No. 101 |
| Terminal Board Assembly including: | No. 103 |
| Terminal | No. 102 |
| Vidicon Mount Assembly | No. 710 |
| Yoke Assembly | No. 111 |

HEAVY DUTY CAMEFL 321 SERIES
(VBOO-3211-01)
(Refer to Master Components List T6768 List 1) Cross Reference List for VBOO-3211Z Sh.]


HEAVY DUTY CAMERA 321 SERIES
(VB00-321]-01)
(Refer to Master Components List T6768 List 1) Cross Reference List
for VBOO-32112 Sh. 1

(Refer to Master Components List T6768 List 1) Cross Reference List
for VBOO-32112 Sh. 1



> VIDEO BOARD 1
> (B99-0038-01)
(Refer to Master Components List T6768 List 2)
Cross Reference List
for B99-00382

| F-9. | No. | Rep. | No. | Ref. | no. | Ref. | Mo. | Ref. | No. | Ref. | Mo. | Ref. | No. | Rep. | Mo. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CL | 21 | C21 | 21 |  |  | R6 | 106 | R26 | 114 | R46 | 106 | R'66 | 121 | VT4 | 210 |
| C2 | 22 | C22 | 23 | MR7 | 84 | R7 | 109 | R27 | 123 | $\mathrm{R}_{4} 7$ | 103 |  |  | VT5 | 210 |
| C3 |  |  |  | MR8 | 84 | R8 | 110 | R28 | 124 | R48 | 102 | R68 | 105 | VT6 | 210 |
|  |  | C24 | 37 | MR9 | 84 | R9 | 111 | R29 | 102 | R49 | 103 | R69 |  | VT7 | 211 |
| C5 | 29 | C25 | 38 | MR10 | 84 |  |  | R30 | 125 | R50 | 106 |  |  | VT8 | 210 |
| C6 | 49 | C26 | 24 | MR11 |  | R11 | 112 | R31 | 126 | R51 | 106 |  |  | VT9 | 210 |
| C7 | 21 |  |  | MR12 | 85 | R12 | 113 | R32 | 127 | R52 | 113 |  |  | VT10 | 209 |
| C9 | 22 | C28 | 37 | MR13 | 85 | R13 | 114 | R33 | 118 | R53 | 104 |  |  | VTl1 | 210 |
| C9 | 23 |  |  | MR14 | 85 | R14 | 111 | R34 | 120 | R54 | 129 |  |  | VT12 |  |
| C10 | 31 |  |  | MR15 | 85 | R15 | 115 | R35 | 99 | R55 | 104 |  |  | VT13 | 207 |
| C11 | 14 |  |  |  |  | R16 | 107 | R36 | 109 | R56 | 102 |  |  | VT14 | 211 |
|  |  | L1 | 69 |  |  | R17 | 116 | R37 | 107 | R57 | 104 | RV1 | 173 | VT15 | 212 |
|  |  | L2 | 70 |  |  | R18 | 117 | R38 | 118 | R58 | 98 | RV2 | 174 | VT16 | 211 |
| $\begin{aligned} & \mathrm{Cl} 4 \\ & \mathrm{Cl} 5 \end{aligned}$ | $14$ |  |  | MZ1 |  | R19 | 118 | R39 | 162 | R59 | 130 | RV3 | 175 | VT17 | 211 |
|  | $14$ |  |  |  |  | R20 | 119 | R40 | 161 |  |  |  |  | VT18 | 212 |
|  |  | MRI | 84 | R1 | 131 | R21 | 120 | $\mathrm{R}_{4} 1$ | 128 | R61 | 103 | RLA |  | VT19 | 211 |
| C17 | 14 |  |  | R2 | 132 | R22 | 104 | R42 | 104 | R62 | 113 |  |  |  |  |
| C18 | 34 | MR3 | 84 | R3 | 99 |  |  | R43 | 106 | R63 | 105 | VTI | 209 |  |  |
| C19 | 35 | MR4 | 84 | $\mathrm{R}_{4}$ | 99 | R24 | 121 | $\mathrm{R}_{4} 4$ | 114 | R64 | 120 |  |  |  |  |
| C20. | 36 | MR5 | 84 | R5 | 109 | R25 | 122 | R45 | 240 | R65 | 118 | VT3 | 210 |  |  |

MISCELLANEOUS ITEMS

Board
Clip (Transistor)
Terminal

No. 1
No. 51
No. 200
(B99-00 38-01)
(Refer to Master Components List T6768 List 3)
Cross Reference List
for B99-00 382

| Rep. | мо. | Ref. | no. | Ref. | No. | Ref. | но. | Rep. | No. | Rep. | no. | Ref. | No. | Ref. | no. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Cl | 130 | C22 | 129 | MR 7 | 155 | R9 | 179 | R 30 | 160 | R51 | 37 |  |  | VT8 | 226 |
| C2 | 128 | C23 |  | MR8 | 155 | R10 |  | R31 | 202 | R 52 | 164 |  |  | VT9 | 226 |
| C3 |  | C24 | 131 | MR9 | 155 | R11 | 177 | R32 | 185 | R53 | 45 |  |  | VT10 | 227 |
| C4 |  | C25 | 147 | MR10 | 155 | R12 | 164 | R33 | 208 | R 54 | 186 |  |  | VTII | 226 |
| C5 | 3 | C26 | 9 | MR11 |  | R13 | 192 | R34 | 47 | R55 | 45 |  |  | VT12 |  |
| c6 | 148 | C27 |  | MR12 | 157 | R14 | 179 | R 35 | 53 | R56 | 190 |  |  | VT13 | 79 |
| C7 | 130 | C28 | 131 | MR13 | 157 | R15 | 209 | R36 | 180 | R 57 | 45 | RVI | 212 | VT14 | 223 |
| C8 | -128 |  |  | MR14 | 157 | R16 | 55 | R 37 | 55 | R 58 | 38 | RV2 | 211 | VT15 | 221 |
| C9 | 129 |  |  | MR15 | 157 | R17 | 161 | R 38 | 208 | R 59 | 201 | RV 3 | 213 | VT16 | 223 |
| C10 | 143 |  |  |  |  | R18 | 200 | R 39 | 189 | R60 |  |  |  | VT17 | 223 |
| Cll | 126 |  |  |  |  | R19 | 208 | R40 | 188 | R61 | 42 |  |  | VT18 | 221 |
| C12 |  | L1 | 152 |  |  | R20 | 197 | R41 | 174 | R62 | 164 |  |  | VT19 | 223 |
| C13 |  | L2 | 150 |  |  | R21 | 47 | R42 | 45 | R63 | 50 |  |  |  |  |
| C14 | 126 |  |  | R1 | 184 | R22 | 45 | R43 | 37 | R64 | 47 |  |  |  |  |
| C15 | 126 |  |  | R2 | 181 | R23 | 234 | R44 | 192 | R 65 | 208 | VTI | 227 |  |  |
| C16 |  | MR1 | 155 | R3 | 53 | R24 | 168 | R45 | 187 | R66 | 168 | VT2 |  |  |  |
| C17 | 126 | MR2 |  | R4 | 53 | R25 | 166 | R46 | 37 | R67 |  | VT3 | 226 |  |  |
| C18 | 144 | MR3 | 155 | R5 | 180 | R26 | 192 | R47 | 42 | R68 | 50 | VT4 | 226 |  |  |
| C19 | 145 | MR 4 | 155 | R6 | 37 | R27 | 159 | R48 | 180 |  |  | VT5 | 226 |  |  |
| C20 | 146 | MR 5 | 155 | R7 | 180 | R28 | 56 | R49 | 42 |  |  | VT6 | 226 |  |  |
| C 21 | 130 | MR6 |  | R8 | 195 | R29 | 190 | R 50 | 37 |  |  | VT7 | 223 |  |  |

MISCELLANEOUS ITEMS

Board
Clip (transistor)
Terminals
No. 87
No. 149
No. 219


VIDEO BOARD 2
(B99-0031-01)
(Refer to Master Componerts List T6768 List 2)
Cross Reference list
for 1999-00372

| $f \in \mathrm{~F}$. | no. | Re? | No. | Ref. | no. | Ref. | No. | Ref. | No. | Rep. | No. | Ref. | Mo. | Ref. | Mo. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C1 | 39 | C21 | : 15 | MR6 | 84 |  |  | R16 | 136 | R36 | 128 | R56 | 144 | VT2 | 214 |
| C2 | 25 | C22 | 43 | MR7 | 84 |  |  | R17 | 110 | R37 | 139 | R57 | 143 | VT3 | 210 |
| C3 | 25 | C23 | 28 | MR8 | 84 | MZ1 | 229 | R18 | 105 | R38 | 140 | R58 | 99 | VT4 | 209 |
| $\mathrm{C}_{4}$ | 22 | C24 | 21 | MR9 | 85 | MZ2 | 230 | R19 | 160 | R39 | 101 | R59 | 102 | VT5 | 210 |
| C5 | 22 | C25 | 33 | MR10 | 85 |  |  | R20 | 119 | R40 | 125 | R60 | 145 | VT6 | 215 |
| C6 | 253 | C26 | 21 | MR11 | 85 | R1 | 133 | R21 | 137 | R41 | 139 | R61 | 110 | VT7 | 211 |
| C7 | 29 | C27 | 29 | MR12 | 85 | R2 | 125 | R22 | 138 | R42 | 147 | R62 | 146 | VT8 | 212 |
| C8 | 7 | C28 | 8 | MR13 | 85 | R3 | 120 | R23 | 106 | R43 | 141 | R63 | 125 | VT9 | 211 |
| C9 | 21 | C29 | 40 | MR14 | 85 | R4 | 104 | R24 | 116 | R44 | 127 |  |  | VTIO | 212 |
| C10 | 21 |  |  | MR15 | 85 | R5 | 114 | R25 | 125 | R45 | 116 |  |  | VT11 | 216 |
| Cl1 | 8 |  |  | MR16 | 85 | R6 | 104 | R26 | 130 | R46 | 142 |  |  | VT12 | 217 |
| Cl2 | 41 |  |  | MR17 | 85 | R7 | 112 | R27 | 106 | R47 | 102 |  |  | VT13 | 210 |
| C13 | 15 | Ll | 70 | MR18 | 84 | R8 | 104 | R28 | 135 | R48 | 117 |  |  | VT14 | 212 |
| C14 | 21 | L2 | 71 | MR19 | 87 | R9 | 102 | R29 | 123 | R49 | 125 |  |  | VT15 | 212 |
| Cl5 | 23 |  |  | MR20 | 87 | R10 | 114 | R30 | 121 | R50 | 116 | RV1 | 176 | VT16 | 211 |
| C16 | 15 | MR1 | 84 | MR21 | 85 | R11 | 101 | R31 | 107 | R51 | 126 | RV2 | 175 | VT17 | 212 |
| C17 | 42 | MR2 | 86 | MR22 | 85 | R12 | 114 | R32 | 135 | R52 | 143 | RV3 | 174 | VT18 | 211 |
| C18 | 29 | MR3 | 88 | MR23 | 85 | R13 | 134 | R33 | 125 | R53 | 123 | RV4 | 175 | VT19 | 216 |
| C19 | 21 | MR4 | 86 | MR24 | 85 | R14 | 112 | R34 | 126 | R54 | 99 |  |  |  |  |
| C20 | 8 | MR5 | 86 |  |  | R15 | 135 | R35 | 125 | R55 | 119 | VT1 | 213 |  |  |

MISCELLANEOUS ITEMS

| Board | No. 2 |
| :--- | :--- |
| Clip (Transistor) | No. 51 |
| Screen | No. 180 |
| Terminal | No. 200 |

Page 1 of 1
Issue 2

T6768
List 2 CP

VIDEO BOARD 2
(899-0037-01)
(Refer to Master Components List T6768 List 3)
Cross Reference List
for B99-0037Z

| Ref. | No. | Ref. | no. | Ref. | mo. | Ref. | *. | Ref. | мо. | Rep. | No. | Ref. | no. | Ref. | No. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Cl | 138 | C21 | 10 | MR5 | 156 |  |  | R14 | 177 | R34 | 202 | R54 | 53 | VIT | 224 |
| C2 | 136 | C22 | 142 | MR6 | 155 |  |  | R15 | 183 | R35 | 160 | R55 | 197 | VT2 | : 225 |
| C3 | 136 | C23 | 2 | MR7 | 155 |  |  | R16 | 194 | R36 | 174 | R56 | 205 | VT3 | . 226 |
| $C_{4}$ | 128 | C24 | 130 | MR8 | 155 | MZ1 | 230 | R17 | 195 | R37 | 169 | R57 | 172 | VTM | . 227 |
| C5 | 128 | C25 | 14 | MR9 | 153 | MZ2 | 231 | R18 | 50 | R38 | 203 | R58 | 53 | VT5 | : 226 |
| C6 | 139 | C26 | 130 | MRLO | 153 |  |  | R19 | 196 | R39 | 39 | R59 | 41 | VT6 | 222 |
| 67 | 3 | C27 | 3 | MRII | 153 |  |  | R20 | 197 | R40 | 160 | R60 | 206 | VT7 | 223 |
| C8 | 17 | 028 | 4 | MR12 | 153 | Rl | 171 | R21 | 198 | R41 | 159 | R61 | 195 | VT8 | 221 |
| C9 | 130 | C29 | 139 | MR13 | 153 | R2 | 160 | R22 | 199 | R42 | 204 | R62 | 207 | VT9 | 223 |
| C10 | 130 |  |  | MR14 | 153 | R3 | 191 | R23 | 37 | R43 | 173 | R63 | 163 | VTIO | 221 |
| Cll | 4 |  |  | MR15 | 153 | $\mathrm{R}_{4}$ | 45 | R24 | 161 | $\mathrm{R}_{4} 4$ | 185 |  |  | VIII | 228 |
| C12 | 132 |  |  | MR16 | 153 | R5 | 192 | R25 | 160 | $R 45$ | 161 |  |  | VII2 | 229 |
| C13 | 10 | Ll | 150 | MR17 | 153 | R6 | 45 | R26 | 201 | R46 | 170 |  |  | VII3 | 226 |
| C14 | 130 | L2 | 151 | MR18 | 155 | R7 | 177 | R27 | 37 | R47 | 42 |  |  | VII 4 | 221 |
| C15 | 129 |  |  | MRR19 | 158 | R8 | 45 | R28 | 183 | R48 | 200 |  |  | VT15 | 221 |
| 016 | 10 |  |  | MR20 | 158 | R9 | 43 | R29 | 159 | R49 | 160 | RVI | 215 | VT16 | 223 |
| Cl7 | 140 | MRI | 155 | MR21 | 153 | R10 | 192 | R30 | 168 | R50 | 161 | RV2 | 213 | VT17 | 221 |
| c18 | 3 | MR2 | 156 | MR22 | 153 | Rll | 39 | R31 | 55 | R51 | 202 | RV3 | 211 | VII 8 | 223 |
| C19 | 130 | MR3 | 157 | MR23 | 153 | R12 | 192 | R32 | 183 | R52 | 172 | RV4 | 213 | VII19 | 228 |
| C20 | 4 | MR4 | 156 | MR24 | 153 | RI. 3 | 193 | R33 | 160 | R53 | 159 |  |  |  |  |

MISCELLANEOUS ITEMS

Board
Clip (Transistor)
Terminals
Screen

No. 88
No. 149
No. 219
No. 218

Page 1 of 1
Issue 1

T6768
List 3 JS


FIELD SCAN BOARD
(B99-0031-01)
(Refer to Master Comnonents List T6768 List 2)
Cross Ret'erence List
for B99-00312

| Ref. | Mo. | Rep. | no. | Ref. | мо. | Ref. | No. | Ref. | No. | Ref. | No. | Ref. | Mo. | Rep. | No. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C1 | 44 | Cl9 | 47 | MR11 | 89 | R9 | 131 | R27 | 141 | R49 | 120 |  |  | VT5 | 207 |
| C2 | 14 | C20 | 29 | MR12 | 89 | R10 | 127 | R28 | 142 | R50 | 107 |  |  | VT6 | 215 |
| C3 | 45 | C21 | 14 |  |  | R11 | 112. | R29 | 143 | R51 | 153 |  |  | VT7 | 207 |
| C4 | 45 | C22 | 48 | MR14 | 79 | R12 | 109 | R30 | 139 | R52 | 120 |  |  | VT8 | 243 |
| C5 | 45 |  |  |  |  | R13 | 106 | R31 | 151 | R53 | 121 |  |  | Vr9 9 | 242 |
| C6 | 45 | C24 | 25 |  |  | R14 | 111 | R32 | 113 | R54 | 152 | RV1 | 175 | VT10 | 208 |
| C7 | 22 |  |  | MZ1 | 229 | R15 | 111 | R33 | 148 | R55 | 1.6 | RV2 | 177 | VT11 | 208 |
| C8 | 23 |  |  | MZ2 | 229 | R16 | 132 | R34 | 139 | R56 | 125 | RV3 | 176 | VT12 | 211 |
| C9 | 21 | MR1 | 85 | MZ3 | 229 | R17 | 100 | R35 | 141 | R57 | 123 | $\mathrm{RV}_{4}$ | 178 | VT13 | 211 |
| C10 | 21 | MR2 | 89 |  |  | R18 | 127 | R36 | 127 | R58 | 141 | RV5 | 175 |  |  |
| C11 | 37 | MR3 | 89 | R1 | 106 | R19 | 149 | R37 | 122 | R59 | 121 | RV6 | 179 | VT15 | 212 |
| Cl2 |  | - 1 | 89 | R2 | 163 | R20 | 127 | R38 | 149 | R60 | 111 |  |  | VT16 | -207 |
| C13 | 233 | MR5 | 85 | R3 | 103 | R21 | 244 | R39 | 135 | R61 | 141 | TR1 | 203 | VT17 | -212 |
| C14 | 45 | MR6 | 85 | R4 | 106 | R22 | 128 | R40 | 123 |  |  |  |  | VT18 | -212 |
| C15 | 44 | MR7 | 79 | R5 | 104 | R23 | 244 | R41 | 121 |  |  | VTI | 212 | VT19 | -207 |
| C16 | 37 | MR8 | 85 | R6 | 103 | R24 | 143 | R42 | 98 |  |  | VT2 | 207 | VT20 | -207 |
| C17 | 28 | MR9 | 85 | R7 | 148 | R25 | 141 | R43 | 116 |  |  | VT3 | 208 |  |  |
| C18 | 15 | MR10 | 89 | R8 | 252 | R26 | 127 | R48 | 111 |  |  | VT4 | 207 |  |  |

## MISCELLANEOUS ITEMS

Board<br>Clip (Transistor)<br>Terminal

No. 2
No. 51
No. 200

FIELD SCAF BOARD
(B99-0031-01)
(Refer to Master Components List T'67te iist 3)
Cross Reference List
for B92-00312

| Ref. | No. | Ref. | No. | Ref. | No. | Ref. | Mo. | Ref. | No. | Rep. | No. | Ref. | No. | Res. | No. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Cl | 125 | C20 | 3 | MR12 | 154 | R9 | 184 | R28 | 170 | R47 | - |  |  | VT5 | 79 |
| C2 | 126 | C21 | 126 | MR13 | 154 | R10 | 185 | R29 | 172 | R 48 | 179 |  | : | VT6 | : 222 |
| C3 | 127 | C22 | 137 | MRI4 | 62 | Rll | 177 | R30 | 169 | R49 | 47 |  |  | VT7 | 72 |
| $\mathrm{Cu}_{4}$ | 127 | C23 | - |  |  | R12 | 180 | R31 | 162 | R50 | 55 |  |  | VT8 | -223 |
| C5 | 127 | C24 | 1136 |  |  | R13 | 37 | R32 | 164 | R51 | 167 | RVI | 213 | VT9 | 79 |
| C6 | 127 |  |  |  |  | R14 | 1.79 | R33 | 165 | R52 | 47 | RV2 | 214 | V710 | :121 |
| C7 | 128 |  |  | MZ1 | [230 | R15 | 179 | R34 | 169 | R53 | 168 | RV3 | 215 | VT.L1 | 121 |
| C8 | 129 |  |  | MZ2 | 230 | R16 | 181 | R35 | 173 | R54 | 163 | RV4 | 216 | VT12 | 223 |
| 69 | 130 | MRI | 153 | MZ3 | 230 | R17 | 40 | R36 | 185 | R55 | 161 | RV5 | :213 | VII 3 | 223 |
| Clo | 130 | MR2 | 154 |  |  | R18 | 185 | R37 | 166 | R56 | 160 | RV6 | 217 | VT14 |  |
| Cll | 131 | MR3 | 154 |  |  | R19 | 176 | R38 | 176 | R57 | 159 |  |  | VT15 | 221 |
| Cl2 | 132 | MR4 | 154 | Rl | 37 | R20 | 185 | R39 | 183 | R58 | 173 |  | - | VT16 | 79 |
| C13 | 134 | MR5 | 153 | R2 | 178 | R21 | 175 | R40 | 159 | R59 | 168 | TR1 | 220 | VII7 | 221 |
| C14 | 127 | MR6 | 153 | R3 | 42 | R22 | 174 | $\mathrm{R}_{4} \mathrm{l}$ | 168 | R60 | 179 |  |  | VT12 | 221 |
| Cl5 | 125 | MR7 | 153 | $\mathrm{R}_{4}$ | 37 | R23 | 171 | R42 | 38 | R61 | 173 |  |  | JT19 | 79 |
| Cl6 | 131 | MR8 | 153 | R5 | 45 | R24 | 172 | R43 | 161 |  |  | VTI | 221 | V120 | 79 |
| Cl7 | 2 | MR9 | 153 | R6 | 42 | R25 | 173 | R44 | - |  |  | VT2 | 79 |  |  |
| C18 | 133 | MR10 | 154 | R7 | 182 | R26 | 185 | R45 | - |  |  | VT3 | 121 |  |  |
| C19 | 135 | MRII | 154 | R8 | 183 | R27 | 173 | R4 6 | - |  |  | VT4 | 79 |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
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MISCELLANEOUS ITEMS

Board
Clip (Transistor)
Terminal

No. 24
No. 219
No. 218

Page 1 of 1
Issue 1
T. 70 8
${ }_{\text {List }} 3$

(VBO1-3215-01)
(Refer to Master Components Lists T6768 List 2A
Cross Reference List
for VB20-32152


## MISCELLANEOUS ITEMS

Clamp Assembly
Clip
Cover
Grommet
Nut (Spindle Gripping)
Terminal

No. 6
No. 9
No. 13
No. 19
No. 24
No. 31

Page 1 of 1
(Refer $t$ Master Components List T. 6768 List 2)
Cross Reference List for VB2O-3215Z (Fig.107)

| Rep. | No. | Rep. | no. | Ref. | No. | Rep. | no. | Rep. | мо. | Rep. ${ }^{\text {a }}$ | Ret. | мо. | Ref. | no. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \mathrm{C}_{4} \\ & \mathrm{C} 5 \end{aligned}$ | 8 | C22 | : 7 |  |  |  |  | R21 | 94 | R43 236 | SKB | 185 | SWF | 192 |
|  |  | C23 | 19 | MR5 | 80 | PIA : | 75 |  |  | R44:235 | SKC | 186 | SWG | 191 |
|  |  | C24 | 16 | MR6 | 80 |  |  | R23 | 106 | RVI of | SKD | 186 | SWM | 193 |
|  |  |  |  | MR7 | 80 | R3 | 101 | R24 | 158 | RV2 164 | SKE | 186 | $\begin{aligned} & \text { TP1 } \\ & \text { TP2 } \end{aligned}$ |  |
|  |  | C26 | 14 | MR8 | 81 | R4 | 101 | R25 | 104 | RV3 165 | SKF | 186 |  |  |
|  |  | 627 |  | MR9 | 87 | R5 | 100 | R26 | : 97 | RV4 165 | SKG | 186 |  |  |
| C7 | 11 | C28 | 20 | MRIO | 2.2 | R6 | : 102 | R27: | 95 | RV5 166 | SKR | 186 |  |  |
| C8 | 12 | C29 | :28 | MRII | 83 | R7 | (1,13 |  |  | RV6 167 | SKJ | 186 |  |  |
| C9 | 13 |  |  | MRI2 | 83 | R8 | - ¢ر」 | 129: | 238 | RV7 :168 | SKK | 186 |  |  |
| Cl0 | 15 | C35 | 251 | MR13 | 83 | R9 | 103 | R30 | 159 |  | SKL | 186 | VTI | 204 |
| Cll | 15 |  |  | MR14 | 83 | R10 | 107 | R31 | 107 | RV9 172 | SKM | 189 | VT2 | 204 |
| Cl2 | 16 | FSI | $x$ | MR15 | 80 | Rll | 231 | R32 | 154 | RVI0169 | SKR | 57 | VT3 | 207 |
| Cl3 | 26 | FS2 | 3 | MR16 | 79 | R12 | 108 | R33 | 96 | RVILI 170 | SKS | 57 | VT4 | 206 |
| Cl4 | 247 |  |  |  |  | R13: | 156 | R34 | 100 | RV12170 | SKT | 57 | VT5 | 208 |
| Cl5 | 27 | LI | 68 |  |  | R 14 | 250 |  |  | RVI3171 | SKU | 57 | VT6 | 205 |
| Cl6 | 27 |  |  |  |  | R15 | 94 |  |  |  | SKV | 57 | VT7 | 207 |
| Cl7 | 15 |  |  | MZ2 | 224 | R16 | 157 | R37 | 94 |  | SKW | 57 | VT8 | 204 |
| Cl8 | 18 | $\mathrm{L}_{4}$ | 68 | M23 | 225 | R17 | 105 | R38 | 107 | RV16164 |  |  | VT9 | 204 |
| C19 | 12 | L5 | 68 | $\mathrm{NKZ}_{4}$ | 227 | R18: | 105 | R39 |  |  |  |  |  |  |
| C20 | 12 |  |  | MZ5 | 223 | R19 | 105 | R41 | 237 |  | SWA | 190 |  |  |
| C21 | 12 | LPI | . 73 | MZ6 | 226 | R20 | 104 | R42 |  | SKA 184 | SWE | 192 |  |  |
|  |  |  | - |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
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|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

## MISCELLANEOUS ITEMS

Component Board Assembly including:
Ref. 36 Tag Board Assembly
Ref. 25 Tag Strip Assembly
Ref. 9 Dust Cap
Fuseboard Assembly including:
Ref. 24 Fuseholder
Tag Board Assembly
Clip
Ref. 5 Gasket
Ref. 12 Gasket
Ref. 10 Gasket

No. 56
No. 195
No. 199
No. 59
No. 62
No. 63
No. 196
No. 50
No. 64
No. 65
No. 66

* For 240 V use No. 61

For l20V use No. 239
Page 1 of 3
6 For power supply unit $220 / 110 \mathrm{~V} 50 / 60 \mathrm{c} / \mathrm{s}$ use No. 245 For power supply unit $400 \mathrm{c} / \mathrm{s}$ use No. 249

Cr:MERA CONTROL UNIT V321-5
(VB2O-3215-01)
(Refer to Master Components List T6768 List 2)
Cross Reference List for VB2O-32152(Fig.107)

MISCETLANEOUS ITEMS (Contd.)

|  | Insulators | No. 72 |
| :---: | :---: | :---: |
| Ref. 1 | Nut (Spindle Gripping) | No. 74 |
|  | Rectifier Board Assembly including: | No. 92 |
| Ref. 27 | Gasket | No. 67 |
| Ref. 30 | Rectifier Block | No. 90 |
| Ref. 31 | Rectifier Block | No. 91 |
| Ref. 28 | Tag Board Assembly | No. 197 |
|  | Screw Captive | No. 181 |
|  | Screw Captive | No. 182 |
| Ref. 7 | Tag Strip Assembly | No. 198 |
|  | Terminal Block | No. 201 |
|  | Transformer Assembly (TR2) including: | No. 202 |
|  | Coil Assembly | No. 52 |
|  | Coil Assembly | No. 53 |
|  | Coil Assembly | No. 54 |
|  | Coil Assembly | No. 55 |
| Ref. 17 | Valveholder | No. 218 |
| Ref. 19 | Valve Mount | No. 219 |
| Ref. 20 | Valve Retainer | No. 220 |
| Ref. 15 | Valve Retainer | No. 221 |
| Ref. 16 | Valve Top Can | No. 222 |
|  | Power Supply Unit (50c/s) | No. $76 \varnothing$ |
|  | Power Supply Unit ( $400 \mathrm{c} / \mathrm{s}$ ) | No.776 |
|  | Power Supply Unit (22-30V d.c) | No. 786 |
|  | Board Assembly (Video 1) | No. $5 t$ |
|  | Board Assembly (Video 2) | No. 64 |
|  | Board Assembly (Field Scan) | No. $4 t$ |
|  | Frame \& Control Panel Assembly | No. $60+$ |

[^1]CAMEHA CONTROL UNIT V321-5
(VB20-3215-01)
(Refer to Master Components List T6768 List 2)
Cross Reference List
for VB20-3215Z (Fig.107)


Page 3 or 3
Issue 1

T6768
List 2
CA

for VB20-32162 Sh. 1

| Rep. | мо. | Ref. | no. | Ref. | No. | Ref. | No. | Ref. | но. | Rep. | no. | Ref. | no. | Ref. | мо. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Cl | 13 | C23 | 1 | MR4 | 236 | PLN | 36 | R20 | 45 |  |  | SKP | 66 |  |  |
| C2 | 19 | C24 | 11 | MR5 | 58 | PLP | 36 | R21 | 48 |  |  | SKQ | 65 | V1 | 82 |
| C3 | 19 |  |  | MR6 | 58 |  |  |  |  | RV1 | 104 | SKR | 65 |  |  |
| C4 | 4 | C26 | 4 | MR7 | 58 | R1 | 56 | R23 | 37 | RV2 | 105 | SKS | 65 | VT1 | 78 |
| C5 |  | C27 | 8 | MR8 | 59 | R2 | 57 | R24 | 51 | RV3 | 106 | SKT | 65 | VT2 | 78 |
| C6 | 6 | C28 | 18 | MR9 | 60 | R3 | 39 | R25 | 45 | RV4 | 106 | SKU | 65 | VT3 | 79 |
| C7 | 7 | C29 | 2 | MR10 | 59 | R4 | 39 |  |  | RV5 | 107 | SKV | 65 | VT4 | 80 |
| C8 | 8 | C30 | 3 | MR11 | 61 | R5 | 40 | R27 | 52 | RV6 | 108 | SKW | 65 | VT5 | 121 |
| C9 | 12 |  |  | MR12 | 61 | R6 | 41 |  |  | RV7 | 109 |  |  | VT6 | 81 |
| C10 | 9 | C33 | 235 | MR13 | 61 | R7 | 42 | R29 | 53 |  |  |  |  | VT7 | 79 |
| Cll | 10 |  |  | MR14 | 61 | R8 | 43 | R30 | 54 | RV9 | 110 | SWA | 117 | VT8 | 78 |
| C12 | 11 | FSI | 3 | MR15 | 58 | R9 | 42 | R31 | 55 | RV10 | 111 |  |  | VT9 | 78 |
| C13 | 13 | FS2 | 5 | MR16 | 62 | R10 | 45 | R32 | 99 | RV11 | 112 |  |  |  |  |
| $\mathrm{ClH}_{4}$ | 232 | FS 3 | 27 |  |  | R11 | 102 | R33 | 100 | RV12 | 112 |  |  |  |  |
| C15 | 15 |  |  |  |  | R12 | 46 | R34 | 39 | RV13 | 113 | SWE | 118 |  |  |
| C16 | 15 | Ll | 34 |  |  | R13 | 47 | R35 | 101 |  |  | SWF | 119 |  |  |
| C17 | 10 |  |  | MZ2 | 90 | R14 | 44 | R36 | 57 | RV15 | 114 | SWG | 118 |  |  |
| C18 | 16 | LP1 | 97 | MZ3 | 91 | R15 | 48 | R37 | 48 | RV16 | 115 |  |  |  |  |
| C19 | 8 |  |  | MZ4 | 94 | R16 | 19 | R 38 | 103 |  |  | SWM | 118 |  |  |
| C20 | 8 | MR1 | 236 | MZ 5 | 92 | R17 | 50 | R39 | 38 |  |  |  |  |  |  |
| C21 | 8 | MR2 | 236 | M26 | 93 | R18 | 50 |  |  | SKM | 116 | TR1 | 76 |  |  |
| C22 | 17 | MR3 | 236 |  |  | R19 | 50 |  |  | SKN | 66 | TR2 | 77 |  |  |

## MISCELLANEOUS MECHANIGAL ITEMS

| Clamp Assembly | No. 20 |
| :--- | :--- |
| Clip | No. 21 |
| Clip | No.22 |
| Clip (Transistor) | No.23 |
| Clip (Tip | No. 95 |
| Field Scan Board | No.24 |
| Frame Assembly | No.25 |
| Fuseholder | No.28 |

* For 240 V use No. 26

For 120 V use No. 233

T6768
List 3
CP

```
(Refer to Master Components List T6768 List 3)
                                    Cross Reference List
                                    for VB20-32162 Sh.1
```


## MISCELLANEOUS MECHANICAL ITEMS (Contd.)

| Grommet | No. 30 |
| :---: | :---: |
| Grommet | No. 31 |
| Gromuet | No. 32 |
| Grommet | No. 29 |
| Handle | N0. 33 |
| Insulator | No. 35 |
| Nut (Spindle Gripping) | No. 98 |
| Shading Generator | No. 64 |
| Sync Pulse Generator (Board 1) | No. 67 |
| Sync Pulse Generator (Board 2) | No. 68 |
| Tag Strip Assembly | No. 69 |
| Tag Strip Assembly | N'0.70 |
| Teg Strip Assembly | No. 71 |
| Teg Strip Assembly | No. 72 |
| Teg Strip Assembly | No. 73 |
| Tag Strip Assembly | No. 74 |
| Terminal | No. 120 |
| Terminal Block | No. 75 |
| Valveholder for Vl | No. 83 |
| Valve Retainer for Vl | No. 84 |
| Valve Retainer for XLI | N0. 85 |
| Valve Top Cap | No. 86 |
| Video Amplifier 1 | N0. 87 |
| Video Amplifier 2 | No. 88 |
| Washer | No. 89 |

(Refer to Master Components List T 6768 List 3)
Cross Reference List
for VB20-3216Z Sh. 1

"AMFIIA CONTTR"L INIT
(VBOO-3'1"-01)
(Hefer to Mast.er ('omponents List T6768 List 3)
Cro:s: Reference List
for VB?O-3216Z Shel


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Issue 1

T6768
List 3
(Refer t Master Components List T. 6768 List 2)
Cross Reference List for VB20-3215Z (Fig.107)

| Ref. | No. | Rep. | no. | Ref. | wo. | Rep. No. | Ref. | no. | Ref. ${ }^{\text {f }}$ No. | Ref. | no. | Rep. | no. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | c22 | 7 |  |  |  | R21 | 94 | R43 236 | SKB | 185 | SWF | 192 |
|  |  | C23 | 19 | MR5 |  | PLA: 75 |  |  | R44 233 | SKC | 186 | SWG | 191 |
|  |  | c24 | 16 | MR6 |  |  | R23 | 106 | RV] p | SKD | 186 | SWM | 193 |
| $C_{4}$ | 8 |  |  | MR7 |  | R3 101 | R24 | 158 | RV2 164 | SKE | 186 |  |  |
| C5 | 9 | C26 | 14 | MR8 | 81 | R4 101 | R25 | 104 | RV3 165 | SKF | 186 | TP1 | 187 |
|  |  | C27 |  | MR9: | 87 | R5 100 | R26 : | 97 | RV4 165 | SKG | 186 | TP2 | 188 |
| C7 | 11 | C28 | 20 | MRIO | 12.2 | R6 . 102 | R27 : | 95 | RV5 166 | SKH | 186 |  |  |
| C8 | 12 | C29 | :28 | MRII | 83 | R7 :193 |  |  | RV6 167 | SKJ | 186 |  |  |
| C9 | 13 |  |  | MRI2 |  | R8 | 129 | 238 | RV7 168 | SKK | 186 |  |  |
| C10 | 15 | C35 | 251 | MR13 |  | R9 :103 | R30 | 159 |  | SKL | 186 | VTI | 204 |
| Cll | 15 |  |  | MR14 |  | R10 107 | R31 | 107 | RV9 172 | SKM | 189 | VT2 | 204 |
| Cl2 | 16 | FSI | * | MR15 | 80 | Rll 231 | R32 | 154 | RVI0169 | SKR | 57 | VT3 | 207 |
| C13 | 26 | FS2 | ${ }_{3}$ | MR16 : | 79 | R12:108 | R33: | 96 | RV11,170 | SKS | 57 | VT4 | 206 |
| C14 | 241 |  |  |  |  | R13:156 | R34 | 100 | RV12170 | SKT | 57 | VT5 | 208 |
| C15 | 27 | LI | 68 |  |  | R14 250 |  |  | RVI3171 | SKU | 57 | VT6 | 205 |
| C16 | 27 |  |  |  |  | R25 94 |  |  |  | SKV | 57 | VT7 | 207 |
| C17 | 15 |  |  | MZ2 | 224 | R16:157 | R37 | 94 |  | SKW | 57 | VT8 | 204 |
| C18 | 18 | $\mathrm{I}_{4}$ | 68 | MZ3 | 225 | R17:105 | R38 | 107 | RV16164 |  |  | VT9 | 204 |
| C19 | 12 | L5 | 68 | $\mathrm{MZ}_{4}$ | 227 | Rl8:105 | R39 |  |  |  |  |  |  |
| C20 | 12 |  |  | MZ5 | 223 | R19 105 | $\mathrm{R}_{4}$ | 237 |  | SWA | 190 |  |  |
| 021 | 12 | LPI | 73 | MZ6 | 226 | R20:104 | $\mathrm{R}_{4} 2$ | 237 | SKA 184 | SWE | 191 |  |  |
|  |  |  | : |  |  |  |  |  |  |  |  |  |  |
|  |  |  | : |  |  |  |  |  |  |  |  |  |  |
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|  |  |  |  |  |  |  |  |  |  |  |  |  |  |

## MISCELLANEOUS ITEMS

Component Board Assembly including:
Ref. 36 Tag Board Assembly
Ref. 25 Tag Strip Assembly
Ref. 9 Dust Cap
Fuseboard Assembly including:
Ref. 24 Fuseholder
Tag Board Assembly
Clip
Ref. 5 Gasket
Ref. 12 Gasket
Ref. 10 Gasket
№. 56
No. 195
No. 199
No. 59
No. 62
No. 63
No. 196
No. 50
No. 64
No. 65
No. 66

3 For 240 V use No. 61 For l20V use No. 239

[^2]

V820-32162. SHi
ISSUE 12

SHADING GENERATOR
(B99-1033:-01)
(Refer io Master Components List T6768 List 2C)
Cross Reference List
for B99-00332

| Ref. | мо. | Rep. | No. | Ref. | ко. | Ref. | no. | Ref. | No. | Rep. | но. | ReP. | мo. | Ref. | по. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C1 | 2 | Cl5 | 12 | MR4 | 18 | R12 | 29 | R26 | 38 | R40 | 24 |  |  | VT9 | 57 |
| C2 | 2 | Cl6 | 3 | MR5 | 19 | R13 | 30 | R27 | 43 | R41 | 46 |  |  | VT10 | 56 |
| C3 | 3 | Cl7 | 13 |  |  | R14 | 31 | R28 | 39 | R42 | 44 | RV1 | 50 | VTIl | 58 |
| C4 | 3 | C18 | 14 | R1 | 20 | R15 | 32 | R29 | 40 | R43 | 46 | RV2 | 51 | VT12 | 58 |
| C5 |  | C19 | 14 | R2 | 21 | R16 | 32 | R30 | 41 | R44 | 48 | RV3 | 51 | VT13 | 59 |
| C6 | 5 | C20 | 7 | R3 | 22 | R17 | 33 | R31 | 42 | R45 | : 24 |  |  | VT14 | 53 |
| C7 | 6 | C21 | 7 | R4 | 23 | R18 | 34 | R32 | 28 | R46 | 28 | VTI | 53 |  |  |
| C8 | 7 | C22 | 3 | R5 | 24 | R19 | 25 | R33 | 44 | R47 | 41 | VT2 | 54 |  |  |
| C9 | 8 |  |  | R6 | 25 | R20 | 35 | R34 | 45 | R48 | 32 | VT3 | 55 |  |  |
| C10 | 9 |  |  | R7 | 26 | R21 | 27 | R35 | 4. | R49 | 47 | VT4 | 53 |  |  |
| C11 | 9 |  |  | R8 | 27 | R22 | 36 | R36 | 45 | R50 | 49 | VT5 | 53 |  |  |
| Cl2 | 10 | MR1 | 18 | R9 | 28 | R23 | 37 | R37 | 28 |  |  | VT6 | 56 |  |  |
| C13 | 11 | MR2 | 18 | R10 | 28 | R24 | 23 | R 38 | 32 |  |  | VT7 | 53 |  |  |
| C14 | 12 | MR3 | 18 | Rll | 28 | R25 | 32 | R39 | 46 |  |  | VT8 | 55 |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

MISCELLANEOUS MECHANICAL ITEMS

Board
Clip (Transistor)
Mounting Pads
Mounting Pad Terminal

No. 1
No. 15
No. 16
No. 17
No. 52


SYNC PULSE GENFRATOR (BOARD 1)
(B99-0028-01)
(Refer to Master Components List T6768 List 2B)
Cross Reference List
for B99-00282

| Ref. | no. | Ref. | No. | Ref. | No. | Ref. | No. | Ref. | no. | Ref. | мо. | Ref. | No. | Rep. | Mo. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Cl | 3 | C25 | 13 |  |  | R2 | 36 | R26 | 87 | R50 | 56 | R74 | 53 | TR2 | 78 |
|  |  | C26 | 14 | MR1 | 30 | R3 | 37 | R27 | 53 | R51 | 56 | R75 | 57 |  |  |
| C3 | 5 | C27 | 14 | MR2 | 31 | R4 | 38 | R28 | 54 | R52 | 53 | R76 | 56 | VTI | 81 |
| $\mathrm{Cl}_{4}$ | 6 | C28 | 15 | MR3 | 31 | R5 | 37 | R29 | 55 | R53 | 56 | R77 | 57 | VT2 | 80 |
| C5 | 7 | C29 | 13 | MR4 | 32 | R6 | 41 | R30 | 44 | R54 | 57 | R78 | 57 | VT3 | 80 |
| C6 | 8 | C30 | 13 | MR5 | 33 | R7 | 40 | R31 | 44 | R55 | 56 | R79 | 76 | VT4 | 81 |
| C 7 | 3 | C31 | 14 | MR6 | 33 | R8 | 41 | R32 | 56 | R56 | 57 | R80 | 47 | VT5 | 81 |
| C8 | 9 | C32 | 14 | MR7 | 32 | R9 | 42 | R33 | 57 | R57 | 54. |  |  | VT6 | 81 |
|  |  | C33 | 13 | MR8 | 33 | R10 | 43 | R34 | 56 | R58 | 55 |  |  | VT7 | 81 |
| C10 | 10 | C34 | 16 | MR9 | 33 | R11 | 38 | R35 | 57 | R59 | 44 |  |  | VT8 | 82 |
| C11 | 4 | C35 | 13 | MR10 | 33 | R1- | 44 | R36 | 53 | R60 | 4.4 |  |  | VT9 | 82 |
| C12 | 8 | C36 | 15 | MR11 | 33 | R13 | 39 | R37 | 54 | R61 | 56 |  |  | VT10 | 82 |
|  |  | C37 | 13 | MR12 | 33 | R14 | 45 | R38 | 55 | R62 | 56 |  |  | VT11 | 82 |
| C14 | 11 | C38 | 14 | MR13 | 33 | R15 | 38 | R39 | 4 | R63 | 53 |  |  | VT12 | 82 |
| C15 | 12 | C39 | 14 | MR14 | 33 | R16 | 46 | R40 | $4_{4}$ | R64 | 57 |  |  | VT13 | 82 |
| C16 | 13 | C 40 | 15 | MR15 | 33 | R17 | 47 | R41 | 56 | R65 | 56 | RV1 | 70 | VT14 | 82 |
| C17 | 14 | C41 | 13 | MR16 | 33 | R18 | 48 | R42 | 56 | R66 | 57 | RV2 | 71 | VT15 | 82 |
| C18 | 14 |  |  | MR17 | 33 | R19 | 38 | R43 | 57 | R67 | 54 | RV3 | 72 | VT16 | 82 |
| C19 | 15 |  |  |  |  | R20 | 49 | R1,4 | 57 | R68 | 54 | RV4 | 89 | VT17 | 82 |
| C20 | 13 |  |  |  |  | R21 | 50 | R45 | 56 | R69 | 55 | RV5 | 73 |  |  |
| C21 | 13 |  |  |  |  | R22 | 44 | R46 | 54 | R70 | 44 | RV6 | 72 |  |  |
| C 22 | 14 |  |  | MZ 1 | 83 | R23 | 51 | R47 | 55 | R71 | 1.4 |  |  |  |  |
| C23 | 14 | Ll | 25 |  |  | R24 | 88 | R48 | 44 | R72 | 56 |  |  |  |  |
| C24 | 15 | L2 | 26 | R1 | 35 | R25 | 39 | R49 | 44 | R73 | 56 | TR1 | 77 |  |  |

MISCELLANEOUS MECHANICAL ITEMS

Board
Clip
Mounting Pad
Mounting Pad
Terminal

No. 1
No. 24
No. 28
No. 29
No. 75

(B99-0029-01)
(Refer to Mister Components List T6768 List 2B)
Cross Reference List
for B99-00292

| Ref. | No. | Ref. | No. | Ref. | no. | ReP. | но. | ReP. | No. | Ref. | No. | Ref. | No. | Ref. | но. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Cl | 13 | C30 | 22 |  |  | R4 | 44 | R33 | 55 | R62 | 57 | R91 | 67 | VT2 | 82 |
| C2 | 14 | C31 | 12 | MR1 | 33 | R5 | 44 | R34 | 4 | R63 | 57 | R92 | 56 | VT3 | 82 |
| C3 | 15 | C32 | 21 | MR2 | 33 | R6 | 56 | R35 | 4 | R64 | 56 | R93 | 56 | VT4 | 82 |
| $\mathrm{C}_{4}$ | 14 | C33 | 18 | MR3 | 33 | R7 | 56 | R36 | 56 | R65 | 67 | R94 | 36 | VT5 | 32 |
| C5 | 13 | C34 | 8 | MR4 | 33 | R8 | 57 | R37 | 56 | R66 | 56 | R95 | 43 | VT6 | 82 |
| C6 | 13 | C35 | 19 | MR5 | 33 | R9 | 57 | R38 | 53 | R67 | 39 | R96 | 43 | VT7 | 82 |
| C7 | 14 | C36 | 19 | MR6 | 33 | R10 | 56 | R39 | 57 | R68 | 4 | R97 | 65 | VT8 | 82 |
| C8 | 14 | C37 | 22 | MR7 | 33 | R11 | 54 | R40 | 57 | R69 | 67 | R98 | 39 | VT9 | 82 |
| C9 | 15 | C38 | 22 | MR8 | 33 | R12 | 55 | R41 | 54 | R70 | 56 | R99 | 67 | VT10 | 82 |
| Cl0 | 13 | C39 | 5 | MR9 | 33 | R13 | 44 | R42 | 55 | R71 | 60 | R100 | 56 | VTll | 81 |
| Cll | 13 | C40 | 8 | MR10 | 33 | R14 | 44 | R43 | 44 | R72 | 61 | R101 | 69 | VT12 | 81 |
| C12 | 14 | C41 | 15 | MR11 | 33 | R15 | 56 | R44 | 4 | R73 | 4.4 | R102 | 37 | VT13 | 81 |
| C13 | 14 | C42 | 17 | MR12 | 33 | R16 | 56 | R45 | 56 | R74 | 62 | R103 | 54 | VT14 | 82 |
| $\mathrm{Cl}_{4}$ | 15 | C43 | 5 | MR13 | 33 | R17 | 53 | R46 | 56 | R75 | 56 | R104 | 68 | VT15 | 81 |
| C15 | 13 | C44 | 90 | MR14 | 33 | R18 | 57 | R47 | 53 | R76 | 56 |  |  | VT16 | 82 |
| C16 | 13 | C45 | 85 | MR15 | 33 | R19 | 57 | R48 | 57 | R77 | 56 |  |  | VT17 | 82 |
| C17 | 14 | C46 | 22 | MR16 | 33 | R20 | 56 | R49 | 57 | R78 | 46 |  |  | VT18 | 81 |
| 018 | 14 | C47 | 22 | MR17 | 33 | R21 | 54 | R 50 | 59 | R79 | 63 |  |  | VT19 | 82 |
| C19 | 15 |  |  | MR18 | 33 | R22 | 55 | R51 | 37 | R80 | 54 |  |  | VT20 | 81 |
| C20 | 16 | C49 | 14 | MR19 | 33 | R23 | 44 | R52 | 36 | R81 | 63 |  |  |  |  |
| C21 | 13 |  |  | MR20 | 33 | R24 | 44 | R53 | 56 | R82 | 56 |  |  | VT22 | 81 |
| C22 | 14 |  |  | MR21 | 33 | R25 | 56 | R 54 | 56 | R83 | 56 |  |  | VT23 | 81 |
| C23 | 14 |  |  | MR22 | 34 | R26 | 56 | R55 | 64 | R84 | 4.4 |  |  | VT24 | 81 |
| C24 | 15 |  |  |  |  | R27 | 53 | R56 | 43 | R85 | 4 |  |  | V'25 | 81 |
| C25 | 21 |  |  |  |  | R28 | 57 | R57 | 64 |  |  | RV1 | 74 |  |  |
| C26 | 13 |  |  |  |  | R29 | 57 | R58 | 43 | R87 | 57 | RV2 | 74 |  |  |
| C27 | 17 |  |  | Rl | 53 | R30 | 56 | R59 | 65 | R88 | 64 | RV3 | 74 |  |  |
| C28 | 20 | L1 | 26 | R2 | 54 | R31 | 39 | R60 | 66 | R89 | 43 |  |  |  |  |
| C29 | 23 | L2 | 27 | R3 | 55 | R32 | 54 | R61 | 43 | R90 | 66 | VTI | 82 |  |  |

## MISCELLANEOUS MECHANICAL ITEMS

Board<br>Mounting Pad Terminal

No. 2
No. 29
No. 75



## MISCELLANEOUS MECHANICAL ITEMS

| Board Assembly | No. 1 |
| :--- | :--- |
| Clamp Assembly | No. 7 |
| Cleat | No. 8 |
| Clip | No. 10 |
| Cover | No. 12 |
| Fuseholder | No. 18 |
| Grommet | No. 20 |
| Grommet | No. 21 |
| Insulator | No. 22 |
| Mounting Plate | No. 23 |
| Rectifier Fittings | No. 26 |
| Tag Board Assembly | No. 29 |
| Terminals | No. 31 |

Page 1 of 1
T6768
List 2A


POWER SUPPIY UNIT
(VB03-3<15-01)
(Refer to Master Components List T6768 List 2A)
Gros:; Reference List
for VEO3-32152

| Ret. Mo. | Rer. | но. | Ref. | ко. | Ref. | No. | Ref. | No. | Ref. | No. | Ref. | No. | Rep. | No. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Cl 5 | FS3 | 17 | MRI | 45 | MR5 | 45 | MR9 | 45 | RV2 | 28 |  |  |  |  |
| C2 4 |  |  | MR2 | 45 | MR6 | 45 |  |  |  |  |  |  |  |  |
| C3 4 | M | 16 | MR3 | 1.5 | MR7 | 45 |  |  | TR1 | 34 | VTl | 32 |  |  |
| - |  |  | MR1 ${ }_{4}$ | 45 | MR8 | 45 | R.V1 | 27 | TR2 | . 35 | VT2 | 32 |  |  |
| ! |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| - |  |  |  |  |  |  |  |  |  | : |  |  |  |  |
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| ! |  | ; |  | . |  |  |  | : |  | $\vdots$ |  |  |  | ; |
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| ; |  |  |  |  |  |  |  | ; |  | : |  |  |  |  |
|  |  |  |  |  |  |  |  | - |  |  |  |  |  | - |
|  |  |  |  |  |  |  |  | - |  |  |  |  |  |  |

MISCELLANEOUS MECHANICAL ITEMS
Board Assembly
No. 2
Clamp Assembly
Cleat
Clip
Cover
Fuseholder
Grommet
No. 7
No. 8
No. 11
No. 12
No. 18
Grommet
Insulator
Mounting Plate
Rectifier Fittings
Tag Board Assembly
Terminal
No. 20
No. 21
No. 22
No. 23
No. 26
No. 30
No. 31


NOTES
I * adjust to give correct output voltage
2 EXTERNAL CONNECTIONS GO TO TB2 ON
CAMERA CONTROL UNIT SEE VB2O-32152 SHI the lead nos going to corresponding nos ON TB2

| COMP | TYPE |  | COMP | TYPE |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| MR1 | BY×38-300 |  | MR7 | BY×38-300 |  |
| MR2 | BY×30-300 |  | MR8 | BYX38-300 |  |
| M93 | BYx $38-300$ |  | MRO | BYX 38300 |  |
| MR4 | BY×38-300 |  | MRIO | IGB | c. 7026 |
| MR5 | BYX 38.300 |  | VTI | OC28 | CV7085 |
| MRS | BY× 30300 |  | VT 2 | OC28 | cV7085 |

FIG.II3.


V32I SERIES



V32I SERIES VIDICON CAMERA CHANNEL

CAMERA CONTROL UNIT.
BACK PANEL SPADE TERMINATIONS. VBIO-3216-OI CIRCUIT


LINKS ON FIELD SCAN BOARD WHEN DRIVEN BY SYNC PULSE GENERATOR


LINKS ON FIELD SCAN BOARD WHEN USING RANDOM INTERLACE, CRYSTAL LOCKED LINE, FREE RUNNING FIELD.


LINK ON VIDEO 2 WHEN ORIVEN BY SYNC PULSE GENERATOR
 LINKS ON VIDEO 2 WHEN USING
RANDOM INTERLACE
(BOTH TYPES)


SYNC PULSE GENERATOR I SOCKET


CONNECTIONS TO BE MADE WHEN
USING RANDOM INTERLACE,
CRYSTAL LOCKED LINE, FREE RUNNING
FIELO AND ALSO MAINS LOCKED FIELO.










VIEW ON ARROW ' $C$ '.
SEE SHI







VIEW ON A



CONTROL \& CONNECTOR FUNCTIONS \begin{tabular}{|l|l}
\hline REF \& FUNCTION. <br>
\hline RVI \& <br>
\hline

 RVI VIDICON HEATER VOLTS 

\hline RV2 \& NUVISTOR HEATER VOLTS <br>
\hline

 SKAA NUVISTOR HEATER 

SKAB \& CURRENT METERING <br>
\hline SKAC \& VIDICON HEATER <br>
\hline

 

\hline SKAC \& CIDICON HEATER <br>
\hline SKAD \& CURENT METERING <br>
\hline LKA \& NUVISTOR HEATER <br>
\hline

 

\hline LKA \& NUVISNOR HEATER \& LINK <br>
\hline LKB \& VIDICOON HEAER \& LINK <br>
\hline

 

\hline LKB \& VIDICON HEATER LINK <br>
\hline FS3 \& FUSE OUTPUT <br>
\hline
\end{tabular}

$V 321$ SERIES
VIDICON CAMERA CHANNEL



## Part 2 <br> operation and maintenance



## Master Components Lists

The Master Components List at the end of this manual includes all the electrical components and selected mechanical components used in the equipment.

Components shown on individual circuit diagrams may be identified in the master list by means of the cross reference lists located adjacent to the circuit diagrams to which they refer.

## Chapter 1

OPERATION
Para.
General ..... 1
Operational Controls ..... 2
Preset Front Panel Controls ..... 3

## OPERATION

## General

1. It is assumed that the installation has been completed and that all preliminary adjustments have been made as detailed in Section 2, Chapter l. It should be remembered that any alteration made to the installation involving different lengths of camera cable will require a re-adjustment of the preset CABLE CORRECTION, VIDICON HFATER and NUVISTOR HEATER controls.

## Operational controls

2. The 321 series camera channel has only two basic operational controls. These are the ON/OFF switch at the control unit and a manual FOCUS control at the camera. When the optional remote focusing facility is provided the manual focus control is not required. Focus motor speed and focus motor reversing are controlled by two switches, SWC and SWD, mounted on the control unit front panel. Similarly, if the shutter and/or filter are fitted, these are controlled by switch SWB on the control unit. For details of these facilities see Appendioes.

## Pre-set front panel controls

3. The following controls are mounted on a panel recessed into the front of the control unit and are normally covered by a metal plate. Access to them is obtained by undoing the four captive securing screws:-

TARGET (RV4)
(Manual only)

TARGET LIMIT (RV16)

BEAM (RV2)

Controls the sensitivity of the vidicon.

Determines the maximum possible target volts under auto-target condition.

Varies the beam current density in the vidicon to control the peak-white detail. Set to a point just clockwise of that at which the whites commenoe crushing in maximum sensitivity condition.

| GADN (RV9) | Controls the gain of the video amplifiers in the control unit. Only used under low light conditions to produce a standard level output. Normally set to minimum in average conditions. |
| :---: | :---: |
| HEIGHT (RV5) | Adjusts the picture height. |
| BLACK LEVEL (RV6) | Determines the difference in potential between blanking level and picture black level. |
| VERTICAL SHIFT (RV7) | Moves the picture in the vertical direction. |
| WIDTH (RVIO) | Adjusts the picture width. |
| HORIZONTAL SHIFT (RV13) | Moves the picture in the horizontal direction. |
| $\begin{aligned} & \text { X-ALICN. (RVII) } \\ & \text { Y-ALIGN }(\text { RVI2 }) \end{aligned}$ | Used to align the vidicon beam accurately, in conjunction with the focus field to give optimum resolution. |
| FOCUS (RV3) | Focuses the scanning beam in the vidicon. |
| AUTO-TARGET SWITCH (SWE) | When SWE is switched ON automatic compensation is provided for changes in scene brightness. |
| AUTO-BLACK LEVEL SWITCH (SWG) | When SWG is ON the black level is automatically held constant to the level set by the black level control. |
| AUTO-ALIGN SWITCH (SWF) | Used, in conjunction with the $X$ and Y ALIGN controls to simplify beam alignment during setting up. |
|  | Note: The AUTO-ALIGN facility is only available when the SHADING GENERATOR is fitted. |

Note that the above controls should normally only require adjustment when the equipment is initially set up or after the vidicon tube has been changed.

## Chapter 2

## INITIAL SETTING UP

## List of Contents

Para.
General ..... 1
Test Card and Lighting ..... 2
Positioning of Camera (Point Source) ..... 3
Switching On ..... 4
Focus Adjustment ..... 5
Adjustment of HEIGHT and WIDTH ..... 6
Focusing and Alignment ..... 7
AUTO TARGET operation ..... 8
MANUAL TARGET operation ..... 10
BEAM control setting ..... 11
TARGET LIMIT control ..... 14

## General

Reference should be made to component layouts Figs. 124 and 125.

1. The purpose of this procedure is to obtain the correct setting of the preset controls. Once these settings have been obtained no benefit will result from a readjustment unless it becomes necessary to change the vidicon tube. However, it is advisable to check the settings at intervals of approximately three months. The procedure will be most readily carried out if the camera, the control unit and the associated monitor are grouped together and connected by the same lengths of cable which will be employed in the installation. In addition, setting up will be greatly facilitated if a good quality oscilloscope is available.

## Test card and lighting

2. For accurate setting of the height and width of the scanning raster on the vidicon tube it is recommended that the camera be positioned to view a brightly lit test chart (Marconi Resolution Chart No.1). Adequate lighting will be obtained from two 100 watt lamps, in reflectors, placed at a distance of two feet from the resolution chart so that the incident light strikes the test card at an angle of $45^{\circ} \mathrm{C}$.

## Positioning of camera

3. Place the camera on a suitable mounting tripod or bracket and clamp it securely in a horizontal position. Direct the camera towards a test chart and set about three feet away. Set the following controls on the camera control unit front panel as indicated.

AUTO-TARGET switch SWE to AUTO.
TARGET LIMIT control RV16 FULLY CLOCKWISE
BEAM control RV2 FULLY ANTICLOCKWISE
GAIN control RV9 FULLY ANTICLOCKWISE
AUTO-BLACK LEVEL switch SWG to AUTO
BLACK LEVEL control RV6 SLIGHTLY CLOCKWISE
Set the lens aperture to maximum.

## Switching on

4. Before switching the channel on check the following points:-
(a) Ensure that the installation is in accordance with the instructions given in Sect.2. Chap.1. It is important that, where possible, the correct cable lengths be used $t$ connect the three units as the setting of some of the internal preset controls is dependent on these lengths.
(b) Ensure that the camera and camera control unit are installed in a position to allow air to circulate around them. Failure to do this may result in the equipment operating at too high an ambient temperature resulting in poor picture quality and an incorrect setting of the controls.

Switch on the local mains supply and put the MAINS switch SWA on the control unit to ON . Switch on the light source and the monitor and allow a warming up period of $4-5$ minutes. Final adjustments should be made after a running time of 1 hour. If an oscilloscope is available monitor the video output at the test points on the C.C.U. front panel.

## Focus adjustment

5. Turn up the display monitor brightness and adjust the line and ficld hold controls, if necessary, to obtain a locked raster. Rotate the camera BEAM control clockwise until an image of the test chart appears on the monitor. The image may appear very blurred and show only as a change of brightness over different parts of the screen. Adjust the camera FOCUS controls for the best resolution of the test chart. A slight adjustment of BLACK LEVEL may be necessary at this point. Tho camera should be positioned so that the test chart fills the picture area on the monitor. Recheck optical focus after any movement of the camera. A final adjustment of the monitor focus may be necessary for the best result.

## Adjustment of HEIGHT and WIDTH

6. This operation will be simplified if the test chart is replaced by a plain white card of similar dimensions. Move the camera close enough to the card to ensure that the edges of the card do not appear on the monitor. Set the lens aperture to Tll. The scanned area of the camera tube is defined by a mask fitted over the end of the tube. Rotate the HEIGHT and WIDTH controls so that the outline of the mask appears on the monitor and then adjust them until the mask edges are just outside the picture area. Centring can be checked by noting whether any one edge disappears from view before its opposite edge. This is rectified by adjusting the HORIZONTAL OR VERTICAL SHIFT control, whichever is appropriate.

## Focusing and Alignment

7. To obtain correct operation of the vidicon tube it is necessary to ensure that the electron beam is properly aligned with respect to the magnetic focusing field. When alignment is correct alternate clockwise and anticlockwise rotation of the electrical FOCUS control (RV3), through a few degrees, will cause the picture to rotate slightly about its centre. This focus 'rocking' action is simulated by the Auto-Align Circuit. To correct the aligrment replace the test chart and observe the centre of the picture. Now adjust the $X$ and $Y$ ALIGNMENT controls (RVII \& RV12) alternately until the picture
rotates about the contre. Readjustment of picture centring may be necessary. Wher satisfactory alignment and centring are obtained switch off AUTO-ALIGN and make a final adjustment to the focus controls.

## AUTO TARGET operation

8. When operating under AUTO TARGET conditions a standard level output is maintained automatically, having been preset by RV2 on Video 2. The video output level may be changed, without readjusting RV2, by altering the value of R15 on Video 2. The sync level will require adjustment by means of RVI. Typical output levels for video and sync are given below:-

| Video | Sync | Value of Rl5 |
| :---: | :---: | :---: |
| 1 V |  |  |
| 0.75 V | 0.5 V | $180 \Omega$ |
| 0.7 V | 0.25 V | $240 \Omega$ |
|  | 0.3 V | $(270 \Omega$ and $2.2 \mathrm{k} \Omega$ in parallel) |
|  |  | $(270 \Omega$ and $5.6 \mathrm{k} \Omega$ in parallel) |

9. Automatic limitation of the target voltage is achieved by the dark current limiter, $\mathrm{RV}_{4}$ on Video 2, which is set to control the level at which VT19 conducts.

## MANUAL TARGET operation

10. With the AUTO TARGET switch OFF, the standard level video output is set by the TARGET control RV4. The appropriate sync amplitude is set by RV1 on Video 2, and R15 on this board must be selected according to the table in paragraph 8.

## BEAM control setting

11. Monitor the terminated video output at field frequency and adjust the black level for the required amount of set up (normally 0.05V). Rotate the BEAM control clockwise to discharge the target. This will be indicated by the signal amplitude remaining constant and the lack of clipping of the positive tips of the video signal.
12. Rotate the BEAM control $45^{\circ}$ clockwise, readjusting FOCUS control (RV3) if necessary.
13. If, during the life of the tube or when the channel is first switched on, the picture is clipped or negative, the beam can be increased by turning the BEAM control clockwise. Note, however, that excess beam will tend to impair resolution.

## TARGET LIMIT control

14. This control is primarily intended to limit the target voltage excursion under AUTO-TARGET conditions. To set the control correctly, close the iris or reduce scene brightness to the minimum level anticipated, but do not reduce beyond the point at which the video level just commences to decrease. Rotate the TARGET LIMIT control counterclockwise until the video amplitude just commences to decrease.
15. The TARGET LIMIT control should not be used to set the video output to the correct level. Video amplitude is set by means of RV2 on Video 2.
Z NOILDES

## Chapter 1

## INSTALLATION

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## General

1. The camera and control unit should always be mounted where they receive adequate ventilation. When exposed to temperatures below $-20^{\circ} \mathrm{C}$ (CCU) $/-40^{\circ} \mathrm{C}$ (CAMERA) or above $+55^{\circ} \mathrm{C}$ a special housing will be necessary.
2. The maximum distance between the camera and its control unit is governed by the h.f. attenuation and delay time of the video coaxial line in the camera cable. Provision is made on the control unit for correcting the attenuation of cable lengths up to a maximum of 1000 ft . Connections to the camera cable are shown in Table 2, Fig. 1. The cable correction control is RV2 on Video 1. Minimum correction is fully anticlocl:wise, while fully clockwise corrects for 1000 ft of cable. Set the control proportionally for shorter cables.
3. Certain changes are required if it is necessary to change the lind standard. These are as follows:-
$\mathrm{R}_{4} 9$ in the camera
R32 on the camera control unit R39 on Video 1

405 lines
10 ohms
47 ohms
33 ohms

Other standards
27 ohms
15 ohms
22 ohms

A change in the value of $R 39$ is only necessary where the camera is fitted with a silicon controlled rectifier. In addition to the changes above, where the sync. pulse generator boards are fitted changes are required as indicated in Table 1.

Table 1
Changes to Sync. Pulse Generator

| $\begin{aligned} & \text { LINE } \\ & \text { SYSTEM } \end{aligned}$ | 405 | 525 | 625 | 819 | 875 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{\|c} \hline \text { S.P.G.1 } \\ \text { B99-0028- } \\ \text { C10 } \end{array}$ | - | 6000 pf | 6000 pf | 6000 pf | 6000 pf |
| Cll | $0.15 \mu \mathrm{~F}$ | $0.047 \mu \mathrm{~F}$ | $0.047 \mu \mathrm{~F}$ | $0.047 \mu \mathrm{~F}$ | $0.047 \mu \mathrm{~F}$ |
| R78 | 100\% | 2.2 k 2 | $2.2 \mathrm{k} \Omega$ | $2.2 \mathrm{k} \Omega$ | 2.2 k 8 |
| R26 | 180\% | 6.88 | 6.88 | 6.88 | 1809 |
| IINKS | 12-15 | 12-13 | 12-13 | 12-13 | 12-13 |
|  | - | 14-15 | 14-15 | 14-15 | 14-15 |
|  | 18-20 | 17-18,20,21 | 17-18,19,20 | 17-20 | 17-20 |
|  | - | - | - | 16-21 | 16-21 |
|  | 23-24 | 23-24 | 23-24 | 22-23 | 22-23 |
| S.P.G. 2 |  |  |  |  |  |
| $\begin{gathered} \text { B99-0029 } \\ \text { C33* } \end{gathered}$ | 820 pf | 470 pf | 470 pf | 470 pf | 470 pf |
| C44 x | $0.1 \mu \mathrm{~F}$ | $0.03 \mu \mathrm{~F}$ | $0.03 \mu \mathrm{~F}$ | $0.03 \mu \mathrm{~F}$ | $0.03 \mu \mathrm{~F}$ |

Table 1 (Contd.)

| LINE |  |  | 625 | 819 | 875 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| SYSTEM | 405 | 525 | 625 |  |  |
| LINKS | $2-4,5$ | $2-3,4,5$ | $2-3,4,5$ | $1-3,5$ | $1-5$ |
|  | - | $6-7$ | $6-7$ | - | - |
|  | $8-9$ | $8-9$ | $8-9$ | - | - |

3 Nominal values, adjusted on Test.

## Power supplies

4. The heavy duty Camera Control Unit V3215 may be operated from $50-60 \mathrm{c} / \mathrm{s}$ mains, from $400 \mathrm{c} / \mathrm{s}$ supply or from 24 V d.c. The power supply units are interchangeable and are mounted at the rear of the camera control unit. On both versions the mains transformer, TRI, for the $50-60 \mathrm{c} / \mathrm{s}$ supply is provided with a range of taps on the primary winding. These may be selected to set the channel working on any nominal voltage likely to be encountered within the range 100-125V or 200-250V. The windings are connected in series for operation in the range 200-250 volt or in parallel for operation in the range 100-125 volts. Adjustment to the appropriate setting is made by altering the position of wire links on top of TRI. The $400 \mathrm{c} / \mathrm{s}$ power supply unit makes provision for only two nominal voltages i.e. 115 V and 200V. However there is adjustment on the two secondary windings which will take up transformer and component tolerances within the supply. The 24 V d.c. unit is similar to the $400 \mathrm{c} / \mathrm{s}$ power supply unit but incorporates a transistor chopper.
5. Stabilizing circuits have been incorporated to compensate for mains voltage variations up to $+7 \%,-10 \%$ of the nominal value. If the equipment is to be used in the vicinity of heavy electrical equipment the stability of the mains supply should be measured over one working period. If the measurements indicate a variation greater than $+7 \%$ or $-10 \%$ the channel should be connected to a known 'quiet' line or the mains supply should be run through a voltage regulator unit. If a regulator is used it should be of a type which will respond sufficiently rapidly to prevent voltage excursions outside these limits.

## CONNECTORS AND CABLES

## Camera

6. The camera cable is a 37 -core cable. In addition to carrying the video signal, the cable also supplies the field scanning waveform, the line pulse for operating the line scan generator in the camera and power for the camera and head amplifier. Where the optional facilities, i.e. remote focus, lens filter/sun shutter are incorporated, control
voltages for these are also fed along the camera cable. The cable also makes provision for remote line scan reversal and for a telephone line between camera and CCU. Connections to the camera cable are shown in Table 2 \& Fig. 1 and the various types of connector that may be used can be found in the equipment list in Part 1, Sect.1, Chap. 2 of the manual.

Table 2 Connections to camera cable

| Group | Pin. | Colour | Function | Remarks |
| :---: | :---: | :---: | :---: | :---: |
| 1 | U | Red | Focus Current |  |
|  | N | Blue | Focus Current |  |
|  | G | Black | Anode. +300 V |  |
|  | M | White | Beam Focus |  |
| 2 | a | Black | Earth |  |
|  | L | Brown | Nuvistor heater |  |
|  | b | Orange | -16.5V |  |
|  | S | Green | Field Scan |  |
|  | T | Blue | Line Scan |  |
|  | K | Grey | Field Scan |  |
| 3 | E | Black | Remote optical focus | Optional facility |
|  | \# | Screen |  |  |
| 4 | A | $\left.\begin{array}{c} \text { Co-axial } \\ \text { Blue Tracer } \end{array}\right\}$ |  |  |
|  | $F$ | $\left.\begin{array}{l} \text { Blue Tracer } \\ \text { Screen } \end{array}\right\}$ | Camera Blanking | Coaxial outer at +14.5 V |
| 5 | B | Unscreened |  |  |
|  |  | Blue | $+4.5 \mathrm{~V}$ |  |
| 6 | D | $\begin{aligned} & \text { Co-axial } \\ & \text { (No Tracer)) } \end{aligned}$ | Video in. |  |
|  | C | Screen |  |  |
| 7 | J | Unscreened |  |  |
|  |  | Orange | Douser | Optional facility |
| 8 | z | $\left.\begin{array}{c} \text { Co-axial } \\ \text { (Orange } \\ \text { Tracer } \end{array}\right)$ | Line Trigger |  |
|  | R | Screen ) |  | $\begin{aligned} & \text { Co-axial outer at } \\ & -16.5 \mathrm{~V} \text {. } \end{aligned}$ |
| 9 | f | Green | Remote optical focus | Optional facility |

Table 2. (Contd.)

| Group | Pin | Colour | Function | Remarks |
| :---: | :---: | :---: | :---: | :---: |
| 10 | $\begin{aligned} & \mathrm{d} \\ & \mathrm{X} \\ & \mathrm{e} \end{aligned}$ | Blue <br> Orange Green | Telephone X alignment Shading | Optional facility. |
|  | m k W | Brown Grey Black | Artificial earth <br> Y alignment <br> Beam |  |
|  | V | White | Line Scan reverse | Optional facility. |
|  | H P | Pink <br> Yellow | Horizontal Shift $+100 \mathrm{~V}$ |  |
| 11 | $\begin{aligned} & \mathrm{s} \\ & \mathrm{X} \end{aligned}$ | Brown <br> Screen | Vidicon Heater |  |
|  | c h r | Blue <br> Orange <br> Green | Filter <br> Spare <br> Spare | Optional facility. |
| 12 | $\begin{aligned} & p \\ & n \\ & j \\ & j \\ & \text { \# } \end{aligned}$ | Brown <br> Grey <br> Black <br> Screen | spare spare spare |  |
| 13 | $\begin{aligned} & \mathrm{g} \\ & \boldsymbol{Z} \end{aligned}$ | Grey Screen | Vidicon heater |  |

\# All screens are taken to a bonding clip together with outer screen and connected to pin 'a'.


Fig.1. Camera cable and comector.

## Power

7. Power to the CCU is supplied on a seven-way cable (for editions see equipment list). Normally only three ways in the cable are used. However, if it is desired to lock the field frequency to a separate (6.3V) supply the necessary voltage is brought into pin C of PLA (see CCU circuit diagrams Figs. 107 \& 108). Note that this facility is only available when the synchronizing pulse generator boards B99-0028 and B99-0029 are fitted.

## Remote control

8. The optional facilities which are fully described in the Appendices may, to special order, be operated from a remote control unit. For this purpose a 19-way remote control cable will be required. Connections to the remote control cable are shown in Table 3 and Fig.2. Editions of the cable are included in the equipment list.

NOTE: The connections shown may be allocated to other functions according to the requirements of individual applications.

Table 3. Connections to remote control cable. (SKB)

| Socket Pin. | Colour | Function | Remarks |
| :---: | :---: | :---: | :---: |
| A | Light Green | Horizontal Shift (RV13) | Optional Reverse Line Scan Facility. |
| B | Pink | -5.5V | Optional Reverse |
| C | Orange | Shutter/Filter Switch | Alternative to C.C.U. panel mount. |
| D | Violet | $-16.5$ | Optional Reverse <br> Line Scan facility. |
| E | Brown | To camera cable | Optional Reverse Line Scan facility. |
| F | Red/Brown | Picture polarity reversal. | Optional facility. |
| G | Red/Black | Remote optical focus switch | Alternative to C.C.U. panel mount. |
| H | Red/White | Spare |  |
| J | Black | Remote optical focus switch | Alternative to C.C.U. panel mount. |
| K | Red/Green | Spare | - |
| I | Red/Blue | Spare |  |
| M | Grey | Horizontal Shift (R22) | Optional Reverse Line Scan facility. |

Table 3. (Contd.)

| Socket Pin | Colour | Function | Remarks |
| :---: | :---: | :---: | :---: |
| N | Yellow | $+4.5 \mathrm{~V}$ | - |
| P | Green | S.P.G. Changeover | Optional Multi- |
|  |  | Relay (RLA) | Channel Facility. |
| R | Blue | Douser/Filter | Alternative to C.C.U. |
|  |  | Switch | panel mount. |
| S | Red | Remote Optical | Alternative to C.C.U. |
| T | Red/Yellow | Fpare | panel mount. |
| U | Screen | Earth |  |
| V | White | Douser/Filter <br> Switch | Alternative to C.C.U. panel mount. |



Fig. 2. Lemote control cable and connector.

## Control unit to monitor

?. The connection between the control unit and monitor is made with a standard 75 ohm coaxial connector. The type of cable used will be determined by the length and by the degree of picture degradation which can be tolerated. In general, an equalizer network will be required if the full bandwidth is to be maintained. In addition a distribution amplifier will be needed with very long cables to make up the l.f. losses associated with passive equalizer networks.

## Fuses

10. The control unit is fitted with three fuses; two for the mains supply and one for the d.c. output from the power supply unit. On the $100-125 \mathrm{~V}$ range, $50 \mathrm{c} / \mathrm{s}$ and $400 \mathrm{c} / \mathrm{s}$ the rating of the mains fuses FSI and FS2 is 1 amp . while on the $200-250$ volt ranges the rating is 500 mA . For 24 V d.c. supplies the rating is 3 amps. The rating of the output fuse FS3 is 2 amps. The main fuses are fitted inside the unit, near the front on the right hand side. The power unit output fuse is situated in the power unit, together with a spare.

## Connection of channel to supply

11. Check that the local mains supply and the control unit MATNS ON-OFF switches are both in the OFF position. Connect the mains lead of the control unit to the local supply using a connector of appropriate rating. The leads of the mains cable should be connected as follows:-
```
RED lead to MAINS live
BLUE lead to MAINS NEUTRAL
GREEN lead to EARTH
```

The connections are exactly the same whether the supply is $50 / 60 \mathrm{c} / \mathrm{s}$, $400 \mathrm{c} / \mathrm{s}$ or 24 V d.c. using a transistor chopper. It is possible, however, to operate the mobile camera control unit direct from a 24 V d.c. supply. Under these conditions an entirely separate source is required to provide 6.3 V at the vidicon heater. In addition some links must be made on the terminal block TBI on the underside of the control unit chassis (see component layout Fig.124). The links required are as follows:-

Link 11 to 3
Link 2 to PLA-F
Link 10 to 8

Take $24 V$ negative to PLA-A
Take 24 V positive to PLA-F
Take 6 V negative to PLA-E
Take 6 V positive to PLA-B

## INSTALLATION

## Insertion of vidicon into camera

12. I' is possible to replace vidicon tubes of the same length without removing the camera from its case. However, on initial installation and when fitting a different type of tube the position of the tube base holder will require adjustment and for this purpose the camera must be removed from its case. This is achieved by first removing the front mounting plate which is secured by two captive screws. The camera may now be removed from its case by pulling on the rear mounting plate.

## WARNING: When inserting or removing the Vidicon HANDLE WITH EXIREME CARE.

The Vidicon tube is fitted as follows:-
(a) Slacken the screws holding the vidicon base and move the base as far forward as possible. The base should be temporarily fixed in this position.
(b) Unscrew the front retaining ring.
(c) Ronove the vidicon tube mount assembly (Refer to Fig.3). It may lie nocessary to insert a screwdriver blade between the front housing and its seating and prise gently to remove the mount.
(d) The vidicon mount assembly can now be dismantled by undoing the lock ring at the rear.
(e) Assemble the parts of the tube mount assembly in the order shown in Fig.3. Tighten the assembly with the lock ring ensuring that the target connector is making good contact with the target connection on the vidicon tube. DO NOT OVERTIGHTEN.
(f) To ensure correct alignment of the vidicon base with the holder, the short pin on the tube should be lined up with the locating hole in the front housing. To avoid overtightening it is advisable to produce the adjustment by rotating the lock ring.
(g) The tube may now be inserted with the position of the holder adjusted until the front housing seats against the front bulkhead. Tighten the fixing screws.

## Heater voltage adjustments

13. Before proceeding with the initial setting-up of the channel it is necessary to adjust the voltages on the vidicon and nuvistor heaters by means of the controls RVI and RV15, respectively, on the control unit. Monitoring points are provided on both mobile and rack mounted control units and are labelled IKB and IKA. On the mobile units they are located on the power supply unit near the potentiometers and on the rack mounted version they are situated on the control panel. The adjustment should be made by removing the appropriate link and connecting a meter (Avo Model 8 or similar) between the sockets with the meter set to a current range. Switch on the mains and adjust RVI5 (nuvistor heater)


Fig. 3 Detail of vidicon mount
to give a reading of 135 mA d.c. Adjust RV] to give a value of current appropriate to the vidicon tube type being used. It should be remembered that the nuvistor heater is fed from a d.c. supply while the vidicon is fed from an a.c. supply on $50 \mathrm{c} / \mathrm{s}$ mains.

NOTE: Rack mounited units from serial No. 102 to 121 inclusive nere not fitted with monitoring points. The meter may be connected into the heater lines by breaking the circuit at the potentioneters. Access to these can be obtained by connecting the control panel assembly to the unit by means of the test leads B99-C $82-01$ ( 4 ft long) or B99-0682-02 (18 inch long).
14. If the heater voltage cannot be measured at the camera, the heater current may be set at LKA on the camera control unit according to table 4.

## INSTALLATION

Table 4
Heater current settings

| Cable Length | 95 mA | 150 mA | 300 mA | 600 mA | Heater Currents |
| :---: | ---: | :---: | :---: | :---: | :--- |
| 0 ft | 105 mA | 160 mA | 310 mA | 610 mA | ) |
| 500 ft | 106 mA | 161 mA | 312 mA | 616 mA | ) Link Currents |
| 1000 ft | 107 mA | 163 mA | 316 mA | 622 mA | $)$ |

## Operating Conditions

15. A number of link changes are required if it is desired to change the operating conditions. These are indicated in Table 5.

Table 5
Operating Conditions

16. In addition to those mentioned in Table 4, the following links may be required on Video 2 Board:-

Auto-target operation, positive picture only, link 9-10.
Auto-target operation, negative picture only, or picture polarity reversal link 10-11, 12-13. Break 36-37 (DO NOT OPERATE TARGET LIMIT AT MAXIMUM).
Auto-black level operation, signal restored to mask, link 6-7. Auto-black level operation, signal restored to picture blocks, link 6-8.
Dark current limiting, link 36-37.

## Chapter 2

MAINTENANCE

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## Camera Control Unit

1. Two extension boards are available to give free access to the nodules when carrying out measurements on the CCU. Type B99-0030-01 may be used for all modules except the sync. pulse generators, for which B99-0030-02 should be used. Voltages in Table 1 were taken with the camera cable disconnected, but with the boards fitted. A 270 ohms, $3 W$ resistor should be fitted between SKA-T and SKA-R to simulate line scan current.

Table 1
Voltages at Camera Control Unit Socket SKA

| Measure at 8KA | Function | Nominal | Min. | Max. | Control |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Clockwise | Anti-clockwise |
| a-R | Line Co-ax Outer (-16.5V) | 16.2 V | -15.8V | -16.8V | - | - |
| a-B | +4.5V | 4.3v | 3.9 V | 4.7 V | - | - |
| a-F | +14.5V | 14.0V | 11.6 V | 16.0V | - | - |
| a-P | +100V | 93v | 79 V | 107v | - | - |
|  |  |  |  |  | minimum range |  |
| m-a | $\begin{aligned} & \text { Artificial } \\ & \text { earth } \end{aligned}$ | SWE DOWN, RV4 clockwisé adjust RV16 |  |  | 100-130 | $<5$ |
|  |  | SWE DOWN, RV16 clockvise adjust RV4 |  |  | 100-130 | $<5$ |
| --6 | Anode | 284 | 260 | 312 | - | - |
| - | Beam | adjust Rv2 |  |  | <1 | 63-100 |
| m-M | Bean Focus | adjust Rv3 |  |  | 768-838 | 490-700 |
| $\mathrm{N}-\mathrm{U}$ | Focus Current | - | 175 m | 185 m | - | - |

NOTE: Foous current is measured between $S K A-N$ and $S K A-U$ with a maltirange meter on a current range.

## Waveforms

2. Waveforms should be obtainable as indicated in the following paragraphs. When the unit is operated from external drive it is essential that each input is terminated in 75 ohms.
(a) A field scan waveform should be obtainable between SKA-S and SKA-K. The h.t. indicator lamp should go out when either Field drive or Line drive is removed, showing that the scan protection circuit is operating. The lamp should also go out when the 270 ohm resistor between SKA-T and SKA-R is removed and light when the resistor is replaced.

## EQUIPMENT MAINTENANCE

(b) Terminate the Video Output socket, SJK, in 75 ohms and monitor the waveform. With the Black Level Switch in either the ON (automatic) position or OFF (manual) position it should be possible to set the black level to the correct setting i.e. 50 mV above blanking level. The PEAK WHITE Control, RV3 on Video 2 should be fully anti-clockwise and the sync amplitude should be set to 0.5 V for a 1.5 V composite output. Alternative sync levels are 0.3 V and 0.25 V for a 1 volt composite signal having 0.7 V video and 0.75 V video respectively. The value of Rl5 on Video 2 shows the level for which the channel is set (see Part 2.Sect.1.Chap.2). Adjust the level, if necessary, by means of RVI on Video 2.
(c) Camera blanking should be present at SKA-A and line trigger at SKA-Z. When a Shading Generator is fitted a shading signal should be present at SKA-C when the Shading ON-OFF switch (SWM) is 0 N .

## Differential Measurement of Video Response

3. On Video 1 board turn the CABLE CORRECTION Control (RV2) fully anti-clockwise. Add a bias potentiometer to Video 2 board as shown in Fig. 1.


Fig. 1 Bias Potentiometer

Insert the output from a video sweep generator between pins $C$ and $D$ of SKA and earth pin $C$ to the control unit chassis. Adjust the input to the unit for an output at SKL (terminated in 75 ohms ) of 0.5 V peak-topeak. Now set the external potentiometer to give an unclipped output. Readjust input if necessary. The video response should show a peak at approximately $9.5 \mathrm{Mc} / \mathrm{s}$ having a lift of 3 dB . It is possible to adjust RV2 (Cable Correction), if desired, by inserting the video at the camera end of the camera cable. Attenuate the input by 12 dB and turn RVI (Aperture Correction) fully anti-clockwise. C7,C9,Cl0 and Rl3 are selected according to the line standard in use and Ll on Video 1 is adjusted to produce a peak in the response, as shown in Table 2.

Table 2
Aperture Correction

| Line <br> System | $C 7$ | C9 | Cl0 | R13 | Peaking <br> Frequency | Lift <br> $(\mathrm{dB})$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| 405 <br> $625 / 525$ | 105 p | 37 p | 220 p | 68 p | 270 ohms | $4 \mathrm{Mc} / \mathrm{s}$ |
| $625 / 525$ | 33 p | 180 p | 33 p | 390 ohms | $7.75 \mathrm{Mc} / \mathrm{s}$ | 12 |
| maximum <br> resolution <br> 625 | $82 p$ | 330 ohms | $9.5 \mathrm{Mc} / \mathrm{s}$ | 12 |  |  |

The Aperture Correction control (RV1) is normally left fully clockwise i.e. no aperture correction.

## Auto Black Level Circuit

4. There is no quick method of checking the operation of the auto black level circuit, but the following method gives a complete check.
(a) Remove the 75 ohm termination from the line drive socket and connect the Dark Current Simulator circuit shown in Fig. 2.


Fig. 2 Dark Current Simulator
(b) Connect the slider of the 500 ohm potentiometer to SKA-D and the common line to SKA-C. Monitor the waveform at the Video Output socket, SKL, and switch to Manual Black Level control.
(c) Determine the range required on the 500 ohm potentiometer to give a shift in black level of 500 mV . Switch to Auto Black Level control and reset black level to 50 mV above blanking level.
(d) For the same range on the potentiometer, determine the shif't in black level. This should not exceed 30 mV and is typically 15 mV . The measurement is best performed with the oscilloscope time base locked to line frequency.

## Camera Tests

5. Waveforms should be present as shown on the circuit diagram Fig.103. The Beam control, RV2 (Fig.107) should adjust the voltage on the Vidicon base pin 2 in a negative direction relative to pin 7. There should be between +260 V and +213 V on pin 5 relative to pin 7 . Pin 6 should be positive to pin 7 and adjustable to +750 V by the Focus Control RV3 (Fig.107).

## Camera Response

6. Camera response is normally checked on a resolution chart. The camera should resolve a minimum of 700 lines. A method using a sweep generator is given below. Remove the camera from its case and take out the Vidicon tube. Connect the output of the Vidicon Simulator (Fig.3) between the grid pin of VI and earthy end of C4 (Figs. 103 and 123). The layout of the simulator is important. The capacitance to earth and end-tomend of the 15 K resistors must be reduced to a minimum. Monitor the output between test points 12 and 13 . Set up the sweep generator


Fig. 3 Vidicon Simulator
for differential gain measurements and adjust the output of the generator to IV peak-to-peak. Set C9 to mid-position and adjust Ll with an insulated trimming tool for not more than $1 d B$ down to $9 \mathrm{Mc} / \mathrm{s}$ and approximately $3 \partial B$ down at $11 \mathrm{Mc} / \mathrm{s}$. The response should roll off smoothly but earthly arrangements may affect the response at the high frequency end. The minimum acceptable bandwidth is 3 dB down at $9 \mathrm{Mc} / \mathrm{s}$ and +0.5 dB to $8 \mathrm{Mc} / \mathrm{s}$. The peak-to-peak video envelope at Tl2 should lie between 200 and 300 mV .
7. Disconnect the sweep generator, replace the Vidicon tube and set up the camera to view a Marconi Resolution Chart No.l. Now examine streaking after the horizontal black lines. Set the monitor gain to maximum and adjust the monitor brightness control to show any shading immediately following the black-white transitions. Adjust C9 on the head amplifier for minimum streaking.
8. Setting Overall Gain
(a) Remove the sync pulse generator boards or drives if extermally driven and replace the field scan board by a dumny board constructed as indicated in Fig. 4.
(b) Remove the camera from its case and lift off one end of ClO on the head amplifier board. Add the bias potentiometer to Video 2 board as in Para.3. If this test is made with a Vidicon tube fitted, the vidicon heater link should be removed to avoid scan burns. Turn the front panel gain control fully anti-clockwise.
(c) Feed 6.3 V r.m.s. at $50 \mathrm{c} / \mathrm{s}$ into a potential divider as shown in Fig.5. Adjust the 50 K variable to give 0.5 V peak-to-peak at the junction of the 50 K variable and the l00 resistor. Connect the free end of the $3 \times 1 \mathrm{MR}$ resistor chain to the top of $R 1$ on the head amplifier printed board. Connect the earth line to any convenient earth point of the camera. Ensure that the nuvistor heater current is 135 mA .
(d) Adjust the bias potentiometer for an unclipped sine wave at the video output socket SKI and then adjust RV3 on Video 1 for 500 mV peak-to-peak output, using a 1.5 V composite signal (IV video, 0.5 V sync). When the video output is to be 0.75 V or 0.7 V , the potentiometer RV3 should be adjusted to give 375 mV or 350 mV respectively. Ensure that the correct value of resistor is being used for RI5 on Video 2. (See Part 2, Sect.1, Chap.2.)

## Setting Dark Current Limiter

9. With the vidicon tube fitted, adjust the heater current to 105 mA . Switch to AUTO-TARGET and set the lens to T4. Set up the camera to view a resolution chart (Marconi test chart No.l. Fit a 3908 resistor in place of the link between Tags 11 and 13 on Video 1 . Use maximum light level on the vidicon faceplate to minimize dark current. Switch AUTOBLACK ON and rotate TARGET LIMIT control fully clockwise.
10. Monitor the atrificial earth voltage to earth. (With Video 2 extended, this can be monitored at the collector of VT12.) Rotate RV4 on Video 2 until the target volts just start to decrease. Remove the 390 resistor, replace the link and cap the camera lens.
11. The artificial earth voltage will now rise to between -60 and -80 V , dependent upon the cathode current and maximum target voltage taken by the vidicon. A low reading would indicate that the vidicon requires replacement.
12. Reset the TARGET LIMIT control as detailed in Part 2, Sect.1, Chap.2, Para. 16 and lock RV4 with a dab of paint.


Fig. 4 Dummy Scan Board


Fig. 5 Gain Test Jig

## Linearity and Geometry Tests

13. With the Vidicon tube fitted and the heater current adjusted to the correct value, set up the camera to view a grating chart (Marconi test Chart No.4). Now proceed as follows:-
(a) Connect in the output from a grating generator and adjust the number of vertical and horizontal grating generator bars to 25. It is essential that the grating generator should be synchronized from the same drives as the camera channel. Adjust the camera scans so that the mask is just not in view. The camera and chart should be positioned accurately so that the two outside vertical lines and the two outside horizontal lines of the two displays are coincident at their centres.
(b) The Field Linearity is adjusted by means of RV1 and RV2. on the scan board and the Line Linearity is adjusted by means of the taps on the transformer TRI in the camera. This should only be necessary after a major component change. The degree of non-linearity should not exceed $1 \%$. The resistor RVI on the camera is set to the point which just avoids clipping the line scan waveform when the width is correctly set and must be set to avoid displacement of alternate lines.

## Video 1 (Figs. 104 and 123)

## Clamp Pulse

14. The width of the clamp pulse at PLR-2 should be between 2 and 3 $\mu s e c s$. The leading edge, at the $50 \%$ amplitude point, should be delayed with respect to the leading edge of line drive by 3 to $4 \mu \mathrm{~s}$. A similar, positive, pulse should be seen at T3I.

## Camera Blanking

15. Camera blanking, consisting of line frequency pulses and a single field frequency pulse of not less than 6.5 V amplitude should be obtainable at C26. The line pulse width should be less than that of system blanking and the field pulse width approximately $400 \mu \mathrm{~S}$.

## Video 2

16. The automblack level circuit may be checked as indicated in para.4. The auto-target circuit may be checked by viewing a brightly lit test chart at a lens setting of $T 4$ and varying the black level manually between 0 V and 0.8 V as measured at the terminated output socket SKL. There should be no change in the level of peak white relative to blanking when operating with positive picture only i.e. Tags 9 and 10 linked. A check may also be obtained by viewing a reasonably well lit scene at a lens setting of about T4. If the lens stop is now closed by several stops the monitor should recover its normal brightness in about 1 sec . This test may be used with either positive or negative pictures. The video circuits are best checked with a camera as the signal source and typical amplitudes with a 1.5 V composite output are shown on the circuit diagram. No adjustment for frequency response is provided.
17. The Scan Failure Protection Circuit is designed to protect the vidicon tube in the event of scan failure. Where the channel is operated from external drives the circuit may conveniently be checked by turning down the beam control RV2 and removing line or field drive. The h.t. generator should stop and the H.T. ON light go out. When investigating apparent failure of the h.t. generator it should be remembered that the fault may be due to field or line scan failure. Where the channel is operated from the sync pulse generator boards or on random interlace, there is no simple method of checking the protection circuit. It is not sufficient to attempt a check by removing, for example, the Field Scan board as this will break the interlock circuit and remove the feed to the series regulator, VTI to $\mathrm{VT}_{4}$ on the Camera Control Unit chassis. A check may be applied by operating the Field Scan board in the extension board and adopting the following procedure:-

Reference should be made to Figs. 106 and 118
(a) Random Interlace.

Break the link between tags 22 and 23. This will remove the feed from the Xtal Oscillator, VTl2, to the blocking oscillator VT13 and thus check the operation of the line scan protection circuit. Field scan may be checked by breaking the link between tags 8 and 9 unless the channel is mains locked in which event the link between 7 and 9 should be broken. In each check the h.t. generator should stop and the H.T. ON light go out.
(b) Sync Pulse Generator Operation

Break the link between tags 25 and 27 to stop the feed of line drive to the line scan generator. Replace the link and break the link between tags 6 and 7 to stop field drive being fed to the delay multivibrator VT8 and VT9.

## Field Scan

18. Field scan linearity adjustment (RV1 and RV2) is fully described in para.9. The field frequency pulse at $T 1$ should be approximately 400 uS wide. The delay range, relative to field drive obtainable by means of RV4 should be, from less than $200 \mu$ secs. to more than 400 $\mu \mathrm{secs}$. This delay determines the time interval between field drive and the start of field scan. The delay is normally set to approximately $300 \mu \mathrm{~s}$ between the leading edge of field drive and the leading edge of the pulse at Tl.
19. When operating on random interlace the control RV4 is used to lock the field frequency multivibrator to the local mains frequency. Adjustment should be adequate to lock the multivibrator to either 50 or $60 \mathrm{c} / \mathrm{s}$ mains. The line frequency pulse width is adjusted by RV5 and should be at least $5 \mu \operatorname{secs}$. The line frequency is adjusted by RV6. These two controls are slightly interdependent.

## Shading

20. Waveforms should be obtainable as on the circuit diagram. With the auto-align switch $0 N$ there should be at least 60 V half field frequency voltage at C17.

## Sync Pulse Generators Nos. 1 and 2

## Master Oscillator

21. To set up the master oscillator it is recommended that sync pulse generator No.I (B99-0028) be connected in the free running condition (i.e. tag 4 linked to tag 3) and that tag 25 be connected to tag 26.

Adjust RV5 (Xtal lock) to give 0.65 volt d.c. with respect to earth at T26. Now adjust the twice line period by means of RV3 ( 2 x line period), monitoring at TlO , to the appropriate timing as indicated in Table l. A typical waveform is shown in Fig. 6.

Table 3
Twice Line Oscillator Period

| Line System | Half Line Period <br> $(\mu \mathrm{sec})$. |
| :---: | :---: |
| 405 | 49.40 |
| 525 | 31.75 |
| 625 | 32 |
| 819 | 24.42 |
| 875 | 19.45 |



Fig. 6 Master Oscillator Waveform
NOTE: If the correct frequency is not obtainable with the potential at T26 set to 0.65 V , RV5 may be adjusted, in conjunction with RV3, to obtain the correct frequenoy providing the final voltage is within the limits +0.5 to +0.8 V . The final voltage should be noted, as the correct frequency will always be obtained with this value.

## Counter Chain

22. Check at $T 20$ on sync pulse generator No.l and $T 5$ on sync pulse generator No.2, that the counter chain is indicating the correct division ratio for the system in use. (See Table 4 and Fig.7).

Table 4
Frequency Division

| Line <br> System | Number of Spikes |  |
| :--- | :---: | :---: |
|  | T20 (S.P.G.1) | T5 (S.P.G.2) |
| 405 | 15 | 27 |
| 525 | 21 | 25 |
| 625 | 25 | 25 |
| 819 | 7 | 117 |
| 875 | 7 | 125 |



## Fig. 7 Typical Divider Waveform

## Mains Locked Condition

23. The mains lock circuit is set up on test to lock to $50 \mathrm{c} / \mathrm{s}$ mains. To lock the circuit to $60 \mathrm{c} / \mathrm{s}$ mains ensure that T26 is linked to T27 and connect 74 to T3. Monitor the waveform at T5 using an oscilloscope triggered at mains frequency. Ficld pulses will be observed 'running through' at a rate corresponding to the difference frequency between that of the mains and the generator field pulse. Maintain a low pulse amplitude (less than 30 mV ) by means of RV2 and adjust RV1 for zero slip rate. Disconnect $\mathrm{T} 4-\mathrm{T} 3$ and reconnect $\mathrm{T} 4-\mathrm{T} 2$. Check by monitoring at T 5 that the field pulse is now locked to the mains.


Fig. 8 Mains Lock Waveform
34. RV6 (Divide by two) should be adjusted to provide two vertical step edges on the staircase waveform at Tll as indicated in Fig.9.


Fig. 9 Divide-by-two

## Line Blanking

25. Line blanking width is adjusted by means of RV4 on sync pulse generator 1 to be within the limits shown below:

| Line System | Pulse Width (usec). |
| :--- | :---: |
| 405 | 17.5 to 20 |
| Other Systems | 11.5 to 14 |

Output amplitude should be between 1.9 V and 2.5 V peak-to-peak (nominally 2V). The rise time for the leading edge should be $0.25 \mu s e c s$. and for the trailing edge $0.3 \mu \mathrm{secs}$.

## Pield Blanking

26. Field blanking width is adjusted by means of RV3 on sync pulse generator 2 to be within $1000 \mu \mathrm{secs}$. and $2000 \mu \mathrm{secs}$. The output amplitude should be between 1.9 V and 2.5 V peak-to-peak (nominally 2 V ). The rise time for the leading and trailing edges should be $0.5 \mu s e c s$. maximum.

## Line Drive Output Pulse

27. No adjustment is provided for the line drive pulse width which should be between $6 \mu \mathrm{secs}$, and $8.5 \mu \mathrm{secs}$. with an amplitude between 1.9 V and 2.5 V (nominally 2 V peak-to-peak). The rise time for the leading edge should be less than $0.25 \mu \mathrm{secs}$. and for the trailing edge less than $0.6 \mu \mathrm{secs}$.

## Line Sync

28. The line sync pulse width is adjusted by means of RV2 on sync pulse generator 2 to be within the limits shown below:-

| Line System | Pulse Width |  |
| :--- | :---: | ---: |
|  | Min. | Max. |
|  |  |  |
| 405 | 6 | 11 |
| 0 thers | 3.5 | 5.5 |

The output amplitude should be between 1.9 V and 2.5 V (nominally 2 V peak-to-peak). The rise time for the leading edge should be less than $0.25 \mu \mathrm{sec}$. and for the trailing edge less than $0.3 \mu \mathrm{sec}$.

## Field Drive Output Pulse and Field Sync

29. The field drive output pulses should have an amplitude between 1.9 V and 2.5 V (nominally 2 V peak-to-peak) and rise times as follows:-

$$
\begin{aligned}
& \text { Leading edge, less than } 0.5 \mu \mathrm{sec} . \\
& \text { Trailing edge, less than } 2 \mu \mathrm{sec.}
\end{aligned}
$$

The field drive width can be determined by RVI in the field drive multivibrator VTII and VTl2 on sync pulse generator 2. However, it is recommended that the field pulse multivibrator be operated with a link between tags 6 and 7 on sync pulse generator 2. This ensures that the field sync includes exactly eight broad pulses and RVI should have no effect. The output amplitude and rise times for field sync are as for line sync.

## Front Porch

30. The sync pulses should be delayed with respect to the start of line blanking by an amount between 1.3 and $2 \mu s e c s$.

## Operation with Crystal Lock

31. Sync pulse generator 1 should be adjusted as indicated in para.16. Now link T6 to T7 and T8 to T9. Monitor the waveform at T8 and adjust RV5 to the centre of the range in which the master oscillator waveform is locked to the crystal input trigger as shown in Fig.10.


Fig. 10 Crystal Lock
APPEND

## RANDOM INTERLACE FILTER KIT <br> TYPE B99-1219-01

Introduction

1. The Random Interlace Filter Kit is used with the Vidicon Camera Channel Type V32l when the channel is operating under random interlace conditions and it is desired to lock the field frequency to the mains supply. The kit consists of the following items:-

Description and Identity
Choke Bracket B99-1224-50
Choke Assembly B99-0040-01
Screw 2-56 UNC Pan Head, $\frac{1}{4}{ }^{\prime \prime}$
Nut 2-56 UNC
Washer 8BA, single coil spring PF74101/308
Wire 14/.0076 PVC PWI213/66
Wire sopper tinned . 0022D swg. PWIl3l/8

Quantity
I
1
PF47241/308
PF45101/302 2 6 6 24" $1 \frac{1}{2}^{\prime \prime}$
2. Fitting Kit to Mobile Camera Control Unit Type V3215

Note that the 2 screws, 2 of the nuts, 2 of the washers and the choke bracket are not required.
(a) Remove the camera control unit from its case. The four fixing screws are located at the front of the control unit, one in each corner.
(b) View the unit, from the rear, i.e. the power unit end and a cut out will be seen at the right hand side of the power unit chassis adjacent to the potentiometer RVI. The choke assembly is mounted on two brackets immediately behind the cut out, by means of the nuts provided. An 8BA washer should be placed under each nut.
(c) The choke should be wired as shown in Fig.l. using P.V.C. covered flexible wire. The existing lead on the 7 V tap should be unsoldered and reconnected to terminal 4 on the choke. Terminals 1 and 4 should be linked with the tinned copper wire while terminal 2 should be connected to the $O V$ tap with the P.V.C. covered flexible wire. The other lead on the OV tap already exists. Connect a link between SGl/7 and F.Scan/5.

T6,768
Apendix 1


Fig.1.
3. Fitting Kit to Rack Mounted Camera Control Unit Type V3216

Reference should be made to Figs. 2 and 3.
(a) Remove the back panel to provide access to the mounting position for the filter.
(b) Fit the choke bracket to the camera control unit chassis using the holes near resistor R39 and the screws, washers and nuts provided.
(c) Fit the choke to the bracket and wire as shown in Fig. 3 using P.V.C. covered flexible wire.


Fig. 3.
4. Where it is desired to operate with the line frequency crystal controlled a crystal Type Q01653A should be fitted in the C.C.U. For the position of the crystal holder reference should be made to Figs. 122 and 123 for the Mobile Camera Control Unit Type V3215 and to Figs. 124 and 125 for the Rack Mounted Camera Control Unit Type V3216. The frequency depends on the line standard in use and typical frequencies are:-

$$
\begin{aligned}
& 20.250 \mathrm{kc} / \mathrm{s} \text { for } 405 \text { lines } \\
& 31.500 \mathrm{kc} / \mathrm{s} \text { for } 525 \text { lines } \\
& 31.250 \mathrm{kc} / \mathrm{s} \text { for } 625 \text { lines } \\
& 40.950 \mathrm{kc} / \mathrm{s} \text { for } 819 \text { lines }
\end{aligned}
$$

$$
\text { APPENDIX } 2
$$

## PICTURE POLARITY

REVERSAL KIT TYFE B99-1076
Introduction

1. The Picture Polarity Reversal Kit is used with the Vidicon Camera Channel Type V321 and makes provision for reversing picture polarity from a remote position. There is no provision for mounting the control switch on the Camera Control Units V3215 or V3216 and the switch must be connected via the remote control socket SKB. The kit consists of the following items:-

Description and Identity
Relay WIS.11363/B Ref.1 RLB I
Switch, Lever, 3 amp. 250V PC71301/1 SWH
Screw, 4-40 UNC Pan Head $\frac{1}{4}$ " PF47241/308
Stiffener 4-40 UNC PF45402/2
Washer, shakeproof, 6BA
Sleeving, pink
PM9055/001

Quantity

1
2
2
2
$4^{\prime \prime}$

Fitting Relay to Printed Wiring Board B99-0038-01
(Video 1)
2. Reference should be made to Figs. 1 and 2.


The relay should be fixed to the printed wiring board B99-0038-01 (Video l), with the screws provided, in the position shown in Fig.l. The relay should be wired to tags 7 to 13 as shown in Fig. 2 and the wires should then be covered with P.V.C. sleeving and the unused wire cut back to approximately $\frac{1}{4} \mathrm{in}$, then bent to form a loop. The control switch, SWF should be connected between pins $F$ and $N$ of SKB on the camera control unit. For full details of cennections to SKB reference should be made to table 2 in the Installation section of the manual and to Figs. 107 (V3215) and 108 (V3216).

$$
\begin{aligned}
& \text { m } \\
& \text { 즣 } \\
& \text { 훈 }
\end{aligned}
$$

## LINE SCAN REVERSAL KIT

TYPE B99-1067
Introduction

1. The Line Scan Reversal kit is used with the Vidicon Camera Channel Type V321 and makes provision for reversing line scan from a remote position. There is no provision for mounting the control switch on the Camera Control Units V3215 or V3216 and the switch must be connected via the Remote Control socket SKB. The kit consists of the following items:-

Description and Identity
Relay WIS.11363/B Ref.I
Switch, Lever, Double Pole
Changeover, PC71301/2
Resistor, variable, 2.5K PC67401/25
Screw, 4-40 UNC Pan Head
Sleeve

Circuit Designation
RLA
SWK
RV14
-

Quantity 1 1 1 2 8

Fitting Relay to Camera Type V32ll
2. Reference should be made to Fig.l.
(a) Remove the front mounting ring by undoing the two stainless steel screws and remove the camera from its case.
(b) Shorten the leads on the relay and form into hooks as indicated in Fig.l. Fit relay to the rear of the bulkhead using the screws provided and the tapped holes close to the tagboard. A single drop of 'Loctite', grade $H$ should be applied to the screw threads before insertion.
(c) Connect as shown in Fig.l. using P.V.C. covered flexible wire. Ensure that all wiring lies within the circumference of the bulkhead.
(d) Replace camera in case and fit the front mounting ring.

Control Switch SWK and Line Shift Control RV14
3. SWK and RV14 should be wired as shown in Fig.107 (V3215) or Fig. 108 (V3216).


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FITTING LINE SCAN REVERSAL RELAY V321 SERIES CAMERA CHANNEL.

FIG. 1.

## REMOTE SUN SHUTTER KIT

TYPE VB00-4033
Introduction

1. The Remote Sun Shutter Kit is used with the Vidicon Camera Channel Type V321 and makes provision for operating a sun shutter which protects the Vidicon faceplate from intense light sources. The sun shutter is a fail-safe device and is operated by a three position switch having a central off position. The shutter is in position between the lens and the Vidicon faceplate when the switch is in the central position. Provision is made for fitting the control switch to the front panel of either Camera Control Unit V3215 or Camera Control Unit V3216. The kit comprises the following items:-

Description and Identity Circuit Designation Qty

| Shutter Shaft | B99-0498-50 | - | 1 |
| :---: | :---: | :---: | :---: |
| Shutter | B99-0610-50 | - | 1 |
| Spur Gear | B99-0613-51 | - | 1 |
| Spacer | B99-0948-50 | - | 1 |
| Collar W | W.11812/C Sh.1.Ref. 2 | 25HA | 1 |
| Adaptor Plate | B99-0630-50 | - | 1 \% |
| Adaptor | B99-0609-50 | - | 2 * |
| Circlip, External | PH64702/7 | - | 1 |
| Bracket | B99-0839-50 | - | 1 \# |
| Cover, Splash-proof | WIS. 9495 C Ref. 1 | - | 1 |
| Resistor, Wire Wound | PC67008/7, 100 ohms 3W, $9 \%$ | R55 | 1 |
| Switch Double Pole, 3 Positions | WIS.9025/C Ref. 4 | SWB | 1 |
| Switch Micro, 5 amp. | WIS.6908/C Ref. 1 | SWV | 1 \% |
| Ledex Assembly | B99-0893-02 | L5 | 1 \% |
| Screw 6BA.Csk.Hd. | PF13611/308 |  | 3 * |
| Screw 2-56 UNC Pan Hd. | . PF47241/308 |  | 1 |
| Screw 2-56 UNC Pan Hd. | . PF47241/316 |  | 2 \% |
| Screw 4-40 UNC |  |  |  |
| Socket (Hex). Set | PF47471/2 |  | 1 |
| Nut 6BA Hex. Full | PF12101/306 |  | 1 \% |
| Nut 2-56 Hex. | PF45101/302 |  | 2 \% |
| Washer 8BA Small | PF74011/308 |  | 2 \% |
| Washer 8BA Crinkle | PF74121/1 |  | 1 |
| Cable 14/.0048 Insul. Pink |  |  | 18 |

Items shown thus \# are supplied already assembled.

T6768
Apperıdix 4

To Assemble Sun Shutter in Camera V32ll
Reference should be made to Fig. 4 .
2. The Front Mounting assembly is removed by unscrewing the two stainless steel screws at the front. This allows the case to be slid off the front end.
3. The earth clamps on the main tie rods are slackened by undoing the clamping screws and the lead screw is unscrewed from the yoke assembly. In the case of the manual focus, this is achieved by anti-clockwise rotation of the focua knob. If a remote focus unit is fitted, cam assemblies on the tie rods must also be slackened and the lead screw is disengated from the yoke assembly by applying 28 V d.c. to terminals 1 and 2 of the terminal board at the rear of the camera. Remove main tie rods.
4. The pillars supporting the tagboard assemblies and the short tie rods are disengaged from the bulkhead to allow access to it from both sides. The preassembled part of the sun shutter (containing the ledex assembly) is fitted to the bulkhead and secured with the appropriate screw after applying a single drop of 'Loctite' grade $H$ to the screw threads.
5. The following parts are assembled as shown in Fig.3:- shutter shaft; shutter; collar; 8BA crinkle washer; 2-56 UNC pan head screw. The camera is reassembled except for the case and front mounting ring; the cam assemblies are reassembled on the main tie rods and adjusted so that one is positioned to operate its microswitch when the yoke assembly is just short of coming into contact with the front ring assembly. The other is positioned to obtain $\frac{1}{2}$ inch movement of the yoke from its maximum forward position. This is described in more detail in the instruction for fitting the remote focus unit (Appendix 6). The lead screw is re-engaged.
6. The spur gear is held in position in mesh with the solenoid gear and the shutter shaf't assembly inserted through the appropriate hole in the front cheek of the yoke assembly to pass through the 'oilite' bush in the bulkhead and into the gear. The circlip is fitted into the groove provided on the shaft which is then checked for free rotation with the front ring assembly temporarily attached. The spur gear, positioned against the shoulder on the shaft is secured with the set screw ( $4-40$ UNC) after positioning it so that the shutter is placed centrally under the lens mount hole in the front ring when the solenoid is not energized. A single drop of 'Loctite' grade $H$ is applied to the thread of the screw.
7. The shutter assembly is wired as shown in Fig.l. and tested by applying 24 V d.c. to terminals 3 and 4 of the terminal board. The shutter should fully uncap the lens mount hole and hold when the supply voltage drops to 21 V .


Fig.l.
8. The front mounting ring is removed, the camera assembled in the case and the mounting ring is secured in position.

The shutter operation is tested as before by applying 24 V d.c. to pins $J$ and $B$ of the camera connector and checking that it holds when the supply drops to 21V.
9. The remaining items of the sun shutter are fitted to the camera control units V3215 or V3216. The three position switch is fixed in the hole provided in the camera control unit and connected to SKB as indicated in Fig.2. If a remote control unit is in use the switch is connected electrically to the same points via the Remote Control cable (B99-1052) from the plug inserted in SKB, the switch being mounted in a remote unit and wired to convenient tags which are connected to the outgoing cable.


Fig. 2.

Additional Information on fitting both
Sun Shutter and Lens Filter in Camera V321
10. The bracket and microswitch are removed from the sun shutter assembly and a 1 inch diameter spacer fitted in place. The sun shutter microswitch is then fitted to the bracket on the filter ledex assembly.

The sun shutter and lens filter are then assembled as described in their separate fitting instructions and wired as indicated in Fig. 3.


Fig. 3.

The operation of both assemblies is tested as described in the separate fitting instructions and the camera is reassembled.

If the lens filter is to be fitted with a sun shutter already in position, the sun shutter is removed and the procedure as above is followed. In a similar way, the above procedure is carried out if a sun shutter is to be fitted to a camera already having a lens filter.

It is to be noted that when a sun shutter and filter are both fitted, they both operate from the same switch, the centre off position moving the sun shutter in front of the vidicon tube. One of the 'on' positions removes the sun shutter away from the front of the tube and the other position does this and, in addition, moves the filter in front of the tube. Thus, one of the three position switches supplied with each kit of parts will not be required. The bracket supplied with the sun shutter is not used.


# LENS FILTER ASSEMBLY <br> TYPE VBOO-4034 

Introduction

1. The Lens Filter Assembly is used with the Vidicon Camera Channel Type V321 and makes provision for operating a neutral density filter to increase the light handling range of the camera. The filter is operated by a three position switch having a central off position. The filter is in position between the lens and vidicon faceplate when the switch is operated from the central position. Provision is made for fitting the control switch to the front panel of either Camera Control Unit V3215 or V3216. The kit comprises the following itens:-

Description and Identity
Circuit Designation Quantity

| Shutter Shaft | B99-0498-51 | - | 1 |  |
| :---: | :---: | :---: | :---: | :---: |
| Filter Frame | B99-0901-50 | - | 1 |  |
| Circlip, External | PH64702/7 | - | 1 |  |
| Spur Gear | B99-0613-51 | - | 1 |  |
| Spacer | B99-0948-50 | - | 1 |  |
| Collar W. | W.11812/C Sh.l.Ref. 1 | 25HA | 1 |  |
| Adaptor Plate | B99-0630-50 | - | 1 | \% |
| Adaptor | B99-0910-50 | - | 1 | * |
| Adaptor | B99-0664-50 | - | 1 | * |
| Bracket Assembly | B99-0923-01 | - | 1 | \% |
| Cover Splash-proof WI | WIS.9495/C Ref. 1 | - | 1 |  |
| Cable 14/.0048 Insul. P | . Pink | - | 18 | ins. |
| Resistor Wire Wound, P | PC67008/7 100 ohms 3W, 9 | R56 | 1 |  |
| Switch D.P. 3 position | ons WIS.9025/C Ref. 4 | SWB | 1 |  |
| Switch Micro 5 amp | WIS.6908/C Ref. 1 | SWX | 1 | \% |
| Ledex Assembly | B99-0893-01 | L6 | 1 | * |
| Screw 6BA Round Hd. | PF13641/310 | - | 1 | * |
| Screw 2-56 UNC Pan.Hd. | d. PF47241/308 | - | 1 |  |
| Screw 2-56 UNC Pan Hd. | d. PF47241/316 | - | 2 | \% |
| Screw 4-40 UNC Socket (Hex). Set | t $\mathrm{PF} 47471 / 2$ | - | 1 |  |
| Nut 6BA Hex. Full | PF12101/306 | - | 1 | \% |
| Nut 2-56 Hex. | PF45101/302 | - | 2 | * |
| Washer 8BA Small | PF74011/308 | - | 2 | * |
| Washer 8BA Crinkle | PF74121/1 | - | 1 |  |
| Screw 6BA Csk.Head. | PFI3611/310 | - | 1 |  |

Items shown thus $\%$ are supplied already assembled.

т6768
Appendix 5

To Assemble Lens Filter in Camera V3211
Reference should be made to Fig. 4.
2. The Front Mounting ring assembly is removed by unscrewing the two stainless steel screws at the front. This allows the case to be slid off the front end.
3. The earth clamps on the main tie rods are slackened by undoing the clamping screws and the lead screw is unscrewed from the yoke assembly. In the case of manual focus, this is done by anti-clockwise turning of the focus knob. If a remote focus unit is fitted, cam assemblies on the tie rods must also be slackened and the lead screw is disengaged from the yoke assembly by applying 28 V d.c. to terminals 1 and 2 of the terminal board at the rear of the camera. The long tie rods are removed.
4. The pillars supporting the tagboard assemblies and the short tie rods are disengaged from the bulkhead to allow access to it from both sides. The preassembled part of the filter (containing the Ledex assembly) is fitted to the bulkhead and secured with the appropriate screws after applying a single drop of 'loctite' grade $H$ to the screw threads.
5. The following parts are assembled as shwon in Fig.3; filter shaf't; filter holder; collar; 8BA crinkle washer; 2-56 UNC pan head screw. The camera is reassembled except for the case and front mounting ring, the cam assemblies are reassembled on the main tie rods and adjusted so that one is positioned to operate its microswitch when the yoke assembly is just short of coming into contact with the front ring assembly. The other is positioned to obtain $\frac{1}{2}$ inch movement of the yoke from its maximum forward position. This is described in more detail in the instructions for fitting the remote focus unit. The lead screw is re-engaged.
6. The spur gear is held in position in mesh with the solenoid gear and the Filter shaft assembly is inserted through the appropriate hole in the front cheek of the yoke assembly to pass through the 'oilite' bush in the bulkhead into the gear. The circlip is fitted into the groove provided on the shaf't which is then checked for free rotation with the front ring assembly temporarily attached. The spur gear, positioned against the shoulder on the shaft is secured with the set screw (4-40 UNC) after positioning it so that the filter is placed centrally under the lens mount hole in the front ring when the solenoid is energized. A single drop of 'Loctite' grade $H$ is applied to the thread of the screw.
7. The filter assembly is wired as shown in Fig.1. The wiring is tested by applying 24 V d.c. to terminals 4 and 6 of the terminal board when the filter frame should lie centrally under the lens mount hole and hold when the supply drops to 21 V .


Fig. 1.
8. The front mounting ring is removed, the camera assembled in the case and the front mounting is secured in position.
The operation of the filter assembly is tested as before by applying 24 V d.c. to pins $C$ and $B$ of the camera connector and checking that it holds when the supply drops to 21V.
9. The remaining items of the filter assembly are fitted to the camera control units V3215 or V3216. The three position switch is fixed in the hole provided in the camera control unit and connected to SKB as indicated in Fig. 2. If a remote control unit is in use, the switch is connected electrically to the same points via the Remote control cable (B99-1052) from the plug inserted in SKB, the switch being mounted in a remote unit and wired to convenient tags which are connected to the outgoing cable.


Fig. 2.

Additional Information on fitting both
Sun Shutter and Lens Filter in Camera V321
10. The bracket and microswitch are removed from the sun shutter assembly and a 1 inch diameter spacer fitted in place. The sun shutter microswitch is then fitted to the bracket on the filter ledex assembly.

The sun shutter and lens filter are then assembled as described in their separate fitting instructions and wired as indicated in Fig. 3.


Fig. 3.

The operation of both assemblies is tested as described in the separate fitting instructions and the camera is reassembled.

If the lens filter is to be fitted with a sun shutter already in position, the sun shutter is removed and the procedure as above is followed. In a similar way, the above procedure is carried out if a sun shutter is to be fitted to a camera already having a lens filter.

It is to be noted that when a sun shutter and filter are both fitted, they both operate from the same switch, the centre off position moving the sun shutter in front of the vidicon tube. One of the 'on' positions removes the sun shutter away from the front of the tube and the other position does this and, in addition, moves the filter in front of the tube. Thus, one of the three position switches supplied with each kit of parts will not be required. The bracket supplied with the sun shutter is not used.


## FITTING INSTRUCTIONS FOR REMOTE FOCUS UNIT TYPE V4012

## Introduction

1. The Remote Focus Unit Type $V 4012$ is used in conjunction with the V321 series Camera Channel where remote operation of the optical
focusing is required. The unit is supplied as a kit of parts comprising a permanent magnet d.c. motor, switches and all necessary parts for fitting. For a complete item list see the Master Components Lists in the manual $T .6768$. A small quantity of Loctite is provided for sealing screws and nuts. This must not be applied to moving parts.

## 2. Fitting Unit to Camera Type V321I

Reference should be made to Fig. 4 (B.99.1308/1/1)
(a) The Front Mounting Ring assembly should be removed by unscrewing the two stainless steel screws at the front of the camera. This allows the case to be slid off the camera.
(b) Disengage the lead screw by rotating the manual focus control anticlockwise.
(c) The earth clamps on the long tie rods must be slackened by undoing the clamping screws and the tie rods unscrewed with the aid of a tommy bar inserted into the holes provided.
(d) Join the two parts of the cam assembly by means of the 4-40 UNC, $\frac{5}{8}$ inch screws, placing a double coil spring washer between the two parts. Insert a 4-40 UNC, $\frac{1}{4}$ inch screw into each part of the two cam assemblies.
(e) Now view the camera from the rear and slide one of the tie rods through the earth clamp and the right-hand cam assembly positioning the assembly approximately as shown in Fig. 4. Repeat for the left-hand assembly.
(f) Replace front mounting ring assembly.
(g) Assemble limit switches and actuators to yoke as shown in Fig. 4 using the 2-56 UNC pan head screws.
(h) Remove the manual focus shar't and fluted knob from the rear mounting assembly af'ter removing the circlip on the shaft.
(j) Fit the $\frac{1}{4}-28$ UNiP par head screw, the Seloc wasner and the $\frac{1}{4}-28$ UNF nut to the rear mounting ring a:sembly as shown.
(k) Fit tne remote focus motor assembly to the bulkhead usirg the 10-32 UNF screws and stiffnuts.

## FITTING INSTRUCTIONS FOR REMOTE FOCUS UNIT TYPE V4012

## Camera Wiring

3. Wire the unit as shown in Fig.l using the cable provided. A green spot on the motor indicates the side to which the black lead is connected. The cables to the microswitches should be run along the existing cableform and be tied to it. Wire to SWZ first and take the wires to SWY under the head amplifier board. The positions of L3, L7, C37 and C38 are indicated on the tagboard at the rear of the camera.


## Fig. 1 Camera Wiring

## Positioning Cam Assemblies

4. Position the left-hand cam assembly approximately so that the microswitch operates when the yoke is just short of coming into contact with the front mounting ring assembly. Apply 28 V d.c. to terminals 1 and 2 to drive the yoke assembly forward and position the cam assembly as accurately as possible. Clamp the stop to the tie rod. Clear the microswitch actuator from the cam by reversing the supply leads on terminals 1 and 2. Fine adjustment of cam position can now be made by means of the screw joining the cam to the stop. When the final position has been estallished clamp the cam to the tie rod. Repeat the above procedure for the right-hand cam assembly to obtain $\frac{1}{2}$ inch of yoke movemer.t from the forward position.
5. Remove the front mounting ring assembly, replace the camera in its case and replace the front mounting ring assembly.

Fitting Switches to Camera Control Unit Type V3215
6. Fit SWD (Remote Optical Focus) and SWC (Focus speed) in appropriate positions on the panel and wire as shown in Fig.2. The colour coded cables will be found wired to SKB and sleeved ready for use. The zener diode is to be mounted on the heat sink located on pillars between SKB and PLA.


Fig. 2 Wiring for Control Unit Type V3215
Fitting Switches to Camera Control Unit Type V3216
7. Fit SWD (Remote Optical Focus) and SWC (Focus speed) in appropriate positions on the control unit panel and wire as shown in Fig.3. The colour coded cables are brought out from the cableform and are sleeved ready for use. The zener diode is wired between the tags on switch SWC.


Fig. 3 Wiring for Control Unit Type V3216

## Remote Control Unit

8. It is possible to locate the control switches in a position remote from the camera control unit by making use of socket SWB. Wiring for this is shown on the Camera Control Unit circuit diagrams, Figs. 107 and 108 of the manual T. 6768 .


# MASTER COMPONENTS LIST 

FOR
HEAVY DUTY CAMGRA ( 321 SERIES)

$$
(V B 00-3211-01)
$$

## NOTES:

1. Component schedules are presented in the form of a master components list, which includes all components used in this equipment. Each component is identified by means of a spares reference number, column 1. in addition to the normal part identity.
2. Components shown on individual circuit diagrams may be identified in the master list by means of the cross-reference tables associated with each circuit diagram. The numbers given are the spares reference numbers.
3. For spares ordering purposes it is only necessary to quote the exact reference at the top of this page together with the spares reference number. Individual part identities can be given as a cross check if desired, but not necessary.
4. Prices are subject to change without notice.
5. All items reference $P C$ are standardised items and comply with Government specifications where these exist.
6. All items reference WIS are manufactured by component or other suppliers to a Marconi specification which, where appropriate, complies with a Government specification.
7. All items reference $W$ are manufactured by MWT and while materials and practices are in accordance with appropriate Government specifications, these items cannot be regarded as 'Standard Items'.
P.T.O.
8. The following abbrevia $\ddagger$ ions are used throughout this Master Lists

| cap. | capacitor | uH | microhenry |
| :---: | :---: | :---: | :---: |
| carb. | carbon | pF | micromicrofarad |
| c.r.t. | cathode-ray tube | mH | millihenry |
| cer. | ceramic | mA | milliampere |
| c.o. | changeover | min | mirute |
| coax. | coaxial | min. | minimum |
| coeff. | coefficient | m.c. | moving coil |
| CV | Common Valve | mld. | moulded |
| comp. | composition | neg. | negative |
| $\mathrm{c} / \mathrm{s}$ | cycles per second | No. | number |
| dB | decibel | osc. | oscillator |
| dia. | diameter | pap. | paper |
| d.c. | direct current | \% | per cent |
| d.p. | double pole | pos. | positive |
| d.t. | double throw | potr. | potentiometer |
| elyc. | electrolytic | prim. | primary (winding) |
| enam. | enamelled | r.f. | radio frequency |
| e.h.t. | extra high tension | rect. | rectifier |
| fig. | figure | ref. | reference |
| fil. | filament | res. | resistor |
| $f t$ | foot (feet) | res.var. | resistor variable |
| freq. | frequericy |  | (potentiometer) |
| f.s.d. | full scale deflection | rev/min | revolutions per |
| gal | gallon |  | minute |
| H | henry | sect. | section |
| h.s. | high stability | sil.mica | silver mica |
| h.p. | horse power | s.p. | single pole |
| h | hour | s.t. | single throw |
| in | inch | sp.gr. | specific gravity |
| indr. | inductance, self inductor | $\begin{aligned} & \text { s.w.g. } \\ & \text { temp. } \end{aligned}$ | standard wire gauge temperature |
| insul. | insulated | F | fahrenheit |
| insulr. | insulator | terml. | terminal |
| $\mathrm{kc} / \mathrm{s}$ | kilocycles per second | transf. | transformer |
| $k$ ohms | kilohm | tub. | tubular |
| kW | kilowatt | var. | variable |
| kV | kilovolt | vit. | vitreous |
| kVA | kilovolt-amp | V | volt |
| lin. | linear | VA | volt-ampere |
| lg. | long | W | watt |
| max. | maximum | W.W. | wirewound |
| $\mathrm{Mc} / \mathrm{s}$ | megacycles per second | yd | yard |
| M ohms | megohms |  |  |
| metd. | metallised |  |  |
| u | micro |  |  |
| uF | microfarad |  |  |


| No. | Description and Identity | Oty. | Price <br> Each <br> F.O.B.U.R <br> $£$ <br> Sterling | Scale |
| :---: | :---: | :---: | :---: | :---: |
| 1 | Bearing block B99-0469-50 | 1 | 23.50 |  |
| 2 | Bearing bush WIS.6948-C-1-3 (now PC.15552-3) | 1 | 0.10 |  |
| 3 | Board assy. (head amplifier) B99-0447-01 | ¢1 | 206.00 |  |
| 4 | Bush B99-0895-50 | 2 | 1.70 |  |
| 5 | Cap. pap. $0.04 \mathrm{uF} \div 20 \%=50 \mathrm{~V}$ YC. 19307-10 | 2 | 0.25 |  |
| 6 | Cap. metd. $0.05 \mathrm{WF} \pm 20 \%$ 350V WIS. $7190-\mathrm{C}-1-5$ (now PC.19814-5) <br> Cap. metd. $0.05 \mathrm{uF} \pm$, 0\% 1000V WIS.10399-C-RI (now PC.19310-1) | 0 | 0.35 |  |
| 8 | Cap. mיtd. $0.5 \mathrm{UF} \pm 20 \% 250 \mathrm{~V}$ WIS. 1190-C-1-9 (now PC.19813-9) | 2 | 0.35 |  |
| 9 | Cap. metd. luF $\pm 20 \%$ 250V WIS.7190-C-1-1 (now PC.19813-1) | 1 | 0.50 |  |
| 10 | Cap. elyc. $50 \mathrm{uF} \pm 20 \% 70 \mathrm{~V}$ PC. $18438-1$ | 1 | 6.30 |  |
| 11 | Cap. elyc. $500 \mathrm{uF} \pm 20 \% 6 \mathrm{~V} \mathrm{PC} .19441-10$ | 2 | 7.45 |  |
| 12 | Cap. elyc. 500uF $\pm 20 \% 6 \mathrm{~V}$ PC. 19406-9 | 1 | 7.50 |  |
| 13 | Cap. pap. 0.002uF 250 V PC. $19307-1$ | 1 | 0.25 |  |
| 14 | Cap. elyc. 3.6uF $\pm 20 \%$ 1才9V PC. 19464-1 | 2 | 11.00 |  |
| 15 | Cap. resin encapsulated $1000 \mathrm{pF} \pm$ 多 50 V WIS. $10076-\mathrm{B}-\mathrm{R} 7$ (now PC.18811-7) | 4 | 0.55 |  |
| 16 | Cap.elyc. 47uF : $20 \%$ 6V WIS.11495-R10 (now 5/PC.18415-11) | 2 | 0.80 |  |
| 17 | Cap. elyc. 2.2uF $\pm 20 \%$ 20V WIS.11495-R 5 ( now 5/PC.18415-2) | 1 | 0.75 |  |
| 18 | Cap. resin encapsulated $20 \mathrm{pF} \pm 2 \mathrm{pF} 50 \mathrm{~V}$ WIS $.0076-\mathrm{B}-\mathrm{R} 42$ (now PC. 18979-42) | 1 | 0.50 |  |
| 19 | Cap. elyc. 10UF $\pm 2 \%$ 20V WIS.11495-R2 (now 5/PC.18415-22) | 1 | 0.80 |  |
| 20 | Cap. elyc. 68uF $\pm 20 \% 15 \mathrm{~V}$ WIS.11495-R11 (now 9/PC.18415-14) | 1 | 1.25 |  |
| 21 | Cap. elyc. 150 UF $\pm 20 \%$ 6V WIS.11495-R13 (now 5/PC.18415-17) | 1 | 1.45 |  |
| 22 | Cap. resin encapsulated $820 \mathrm{pF} \pm 50 \mathrm{~V}$ WIS. $10076-\mathrm{R}-\mathrm{R} 29$ (now PC.18811-29) | , | 0.50 |  |
| 23 | Cap. elyc. 47uF $\pm 20 \%$ 20V WIS.11495-R12 (now 5/PC.18415-12) | 1 | 1.45 |  |
| 24 | Cap. 68pF +2 pF 50 V WIS. $10076-\mathrm{B}-\mathrm{R} 19$ (now PC.18979-19) | 1 | 0.50 |  |
| 25 | Cap. 27pF $\pm 2 \mathrm{pF} 50 \mathrm{~V}$ WIS. $10076-\mathrm{B}-\mathrm{R} 41$ (now PC.18979-41) | 1 | 0.50 |  |
| 26 | Cap. var. 6.5pF WIS.5268-C-R2 (now PC. 20090-2) | 1 | 0.40 |  |
| 27 | Circlip PH.64702-9 | 1 | 0.20 |  |
| 28 | Calmp ring B99-0485-50 | 1 | 41.50 |  |
| 29 | Calop ring assy. B99-0487-01 | 1 | 14.00 |  |
| 30 | Clip (transistor) WIS. $10705-\mathrm{C-1-1}$ | 1 | 0.10 |  |
| 31 | Coil (align) W. 53770-C-Ed.A | 1 | 4.80 |  |
| 32 | Coil assy. (focus/align) B99-0462-01 | f1 | 442.00 |  |
| 33 | Coil assy. (field) B99-0830-01 | -1 | 95.50 |  |
| 34 35 | Coil assy. (horizontal) W. 54249-B-I-A | 2 | 12.00 |  |
| 35 | Coil assy. (line) B99-0831-01 | ¢1 | 53.50 |  |
|  | ```f Individual items in this list * st l``` |  |  | C |


| no. | Description and ldentity | Qty. | Price Each F.0.B.U.K $£$ Sterling | Scale |
| :---: | :---: | :---: | :---: | :---: |
| 36 | Coil assy. (vertical) W. 54250-B-1-A | 2 | 12.00 |  |
| 37 | Collector ring B99-0473-50 | 1 | 5.20 |  |
| 38 | Drive screw B99-0472-50 | 1 | 7.10 |  |
| 39 | Focus shaft (manual) B99-0582-50 | 1 | 4.55 |  |
| 40 | Former assy. B99-0463-01 | 1 | 45.50 |  |
| 41 | Heat sink B99-0900-50 | 1 | 3.60 |  |
| 42 | Indr. lluH W.62309-B-Sll7 | 1 | 2.90 |  |
| 43 | Insulr. WIS .11699-B-1-2 | 11 | 0.10 |  |
| 4 | Knob (fluted) PH.46501-1 | 1 | 0.30 |  |
| 45 | Lens mount B99-0471-51 | 1 | 7.10 |  |
| 46 | Mounting ring assy. (front) B99-0686-01 | 1 | 16.50 |  |
| 47 | Mounting ring assy. (rear) B99-0674-01 | 1 | 26.00 |  |
| 48 | Plug 37-way Ȧmphenol 69-3102E-28-21P (639) WIS.11429-B-1-1 | 1 | 4.85 |  |
| 49 | Plug button PC.15901-14 | 1 | 0.22 |  |
| 50 | Pot core assy. WIS.8968-C-S 42 | 1 | 26.00 |  |
| 51 | Pot core assy. WIS.8968-C-S43 | 1 | 26.00 |  |
| 52 | Rect. Transitron 2N 1602 | 0 |  |  |
| 53 | Rect. Hughes HSll01 (now IN643) | 2 | 0.55 |  |
| 54 | Rect. Muliard OA200 | 1 | 0.10 |  |
| 55 | Rect. Hughes HG5085 | 7 | 0.20 |  |
| 56 | Rect. Texas IS 417 | 1 | 0.80 |  |
| 57 | Res. metal oxide 1.5 k ohms $\pm$ \% 0.125 W PC. $66626-18$ | 1 | 0.10 |  |
| 58 | Res. w.w. 27 ohms $\pm$ \% 1.5W PC.67007-31 | 1 | 0.20 |  |
| 59 | Res. comp 47 ohms $\pm$ \% 0.125 W PC . 66623-9 | 1 | 0.10 |  |
| 60 | Res. metal oxide 100 ohms $\pm$ \# 0.5 W PC.66637-89 | 1 | 0.10 |  |
|  | Res. metal oxide 1 k ohm $\pm$ P\% 0.5W WIS.9518-B-R3 ( $\mathrm{Cow} \mathrm{PC.66637-4)}$ | 1 | 0.10 |  |
| 62 | Res. metal oxide 5.6 k ohms $\pm 2 \% 0.5 \mathrm{~W}$ PC.66637-85 | 3 | 0.10 |  |
| 64 | Res. metal oxide 56 k ohms $\pm 1 \% 0.5 \mathrm{~W}$ PC. $66637-149$ Res. metal oxide 100 k ohms $\pm 1 \% 0.5 \mathrm{~W}$ PC.66637-125 | 2 | 0.10 |  |
| 65 | Res. metal oxide 120 ohms $\pm$ 牫 0.125 W PC.66626-4 | 2 | 0.10 |  |
|  | Res. metal oxide 270 ohms $\pm$ \$ 0.125 W PC. $66626-8$ | 1 | 0.10 |  |
| 67 68 |  | 1 | 0.10 0.10 |  |
| D | + + per ten |  | T6768 <br> Ljst 1 <br> RD |  |


| Mo． | Description and Identity |  | $\begin{array}{\|c\|} \hline \text { Price } \\ \text { Each } \\ \text { F.O.B.U.K } \\ \& \\ \hline \text { Eterling } \\ \hline \end{array}$ | Scale |
| :---: | :---: | :---: | :---: | :---: |
| 69 | Res．metal oxide 1.8 k ohms $\pm 0.5 \mathrm{~W}$ WIS．9518－B－R5（now PC．66637－81） | 1 | 0.10 |  |
| 70 | Res．metal oxide 82 ohms $\pm 50.125 \mathrm{~W}$ PC．66626－2 | 1 | 0.10 |  |
| 71 | Fes．metal oxide 47 k ohms $:$ 何 0.25 W PC．66626－36 | 2 | 0.10 |  |
| 72 | Res．metal oxide 8.2 k ohms $\pm 0.125 \mathrm{~W}$ PC．66626－27 | 1 | 0.10 |  |
| 73 |  | 5 | 0.10 |  |
| 74 | Res．metal oxide 1.8 k ohms $\pm$ 牰 0.125 W PC．66626－19 | 3 | 0.10 |  |
| 75 | s．metal oxide 180 ohms $\pm$ 號 0.125 W PC．66626－6 | 2 | 0.10 |  |
| 7 | Res．met，s oxide 470 ohms $\pm$ \％ 0.125 W PC．66626－11 | 1 | 0.10 |  |
| 77 | Res．metal oxide 22 k ohms $\pm$ 多 0.125 W PC．66626－32 | 1 | 0.10 |  |
| 78 | Res．metal oxide 3． 3 k ohms $\pm 5 \mathrm{y}$ ． 125 W PC．66626－22 | 3 | 0.10 |  |
| 9 | Res．metal oxide 1.5 k ohms $\pm$ 免 0.125 W PC．66626－18 | 1 | 0.10 |  |
| 80 | Res．metal oxide 390 ohms $\pm 50.125 \mathrm{~W}$ PC．66626－10 | 2 | 0.10 |  |
| 81 | Res．metal oxide 33 k ohms $\pm$ \％ 0.125 W PC．66626－34 | 1 | 0.10 |  |
| 82 | Res．metal oxide 1 k ohm $\pm$ \％ 0.125 W PC．66626－16 | 1 | 0.10 |  |
| 83 | Res．metal oxide 18 k ohms $\pm 9 \% 0.125 \mathrm{~W}$ PC．66626－31 | 2 | 0.10 |  |
| 84 | Res．metal oxide 6.8 k ohms $\pm 0.125 \mathrm{~W}$ PC． $66626-26$ | 1 | 0.10 |  |
| 85 | Res．metal oxide 68 ohms $\leq 50.125 \mathrm{~W}$ PC．66626－1 | 1 | 0.10 |  |
| 86 | Res．metal oxide 1.2 k ohms $\pm$ 鸟 0.125 W PC．66626－17 | 1 | 0.10 |  |
| 87 | Res．comp． 10 ohms $\pm \% 0.125 \mathrm{~W}$ PC．66623－1 | 1 | 0.10 |  |
| 88 | Res．w．w． 1 ohm $\pm$ \％2．5W PC．67091－2 | 1 | 0.10 |  |
| 89 | Res．thermistor 200 ohms $=$ \％PC．66931－1 | 1 | 1.70 |  |
| 90 | Socket special 9－way WIS．11634－B－R1 | 1 | 7.75 |  |
| 91 | Socket assy．B99－0483－01 | ¢ | 11.00 |  |
| 92 | Socket WIS ．6774－C－R2 | 1 | 1.20 |  |
| 93 | Split ring B99－0478－50 | 1 | 4.55 |  |
| 94 | Spring B99－0884－50 | 1 | 6.55 |  |
| 95 | Tag board B99－0579－50 | 1 | 45.50 |  |
| 96 | Tag board B99－0580－50 | 1 | 54.00 |  |
| 97 | Tag board assy．B99－0611－01 | $\nrightarrow 1$ | 43.00 |  |
| 98 | Tag board assy．B99－0612－01 | $\nrightarrow 1$ | 74.00 |  |
| 99 | Tag board assy．B99－0578－01 | ＋1 | 13.00 |  |
| 100 | Tag board assy．B99－0577－01 | ＋1 | 13.00 |  |
| 101 | Termi．PH．77001－1 | 54 | ＋0．20 |  |
| 102 | Terml．WIS．4287－B－R6 | 5 | ＋0．20 |  |
| 103 | Terml．board assy．B99－1016－01 | 1 | 20.00 |  |
| 104 | Transf．potting assy．B99－0632－01 | A | 62.00 |  |
| 105 | Transistor BEY18（PS－100142） | 1 | 1.00 |  |
| $\begin{aligned} & \text { T67 } \\ & \text { Lis } \end{aligned}$ |  |  | er ten | E |




| no. | Description and identity | Oty. | Price <br> Each <br> F.O.B.U.K <br> £ <br> Sterling |
| :---: | :---: | :---: | :---: |
| 4017 | Spacer B99-0948-50 | 1 | 21.50 |
| 4018 | Spur Genr B99-0613-51 | 1 | 14.30 |
| 4019 | Switch, Micro WIS.6908-C-R1 | 1 | 1.00 |
| 4020 | Washer 8BA Small PF. 74011-308 | 2 | +0.20 |
| 4021 | Washer 8BA Crinkle PF.74121-1 | 1 | +0.20 |
|  | Appendix 5 Lens Filter Assy. Kit of Parts |  |  |
| 5001 | Adaptor B99-0910-50 | 1 | 20.00 |
| 5002 | Adaptor B99-0664-50 | 1 | 2.50 |
| 5003 | Adaptor Plate B99-0630-50 | 1 | 21.50 |
| 5004 | Bracket Assy. B99-0923-01 | 1 | 80.00 |
| 5005 | Circlip PH.64702-7 | 1 | +0.20 |
| 5006 | Collar W. 11512-C-1-2 2 HA | 1 | 4.50 |
| 5007 | Cover WIS. 9495-C-RI | 1 | 0.10 |
| 5008 | Filter Frame B99-0901-50 | 1 |  |
| 5009 | Ledex Assy. B99-0893-01 | 1 | 59.50 |
| 5010 | Nut 6BA PF.12101-306 | 1 | +0.20 |
| 5011 | Nut 2-56 HEX. PF.45101-302 | 2 | +0.20 |
| 5012 | Res. W/W 100 ohms $\pm 5 \%$ SW PC. 67008-1 | 1 | 0.10 |
| 1588 | $\dagger$ | pe | $r$ ten |
| H |  |  | T6/68 List 1 CA |


| nc | Description and Identity | Oty. | $\begin{array}{\|c\|} \hline \text { Prioe } \\ \text { Each } \\ \text { F.O.B.U.K } \\ \mathcal{L} \\ \text { Sterling } \\ \hline \end{array}$ |
| :---: | :---: | :---: | :---: |
| 5013 | Screw 6BA CSK. PF.13611-308 | 1 | +0.20 |
| 5014 | Screw 2-56 PAN ${ }^{\prime \prime}{ }^{\prime \prime}$ PF.47241-308 | 1 | +0.20 |
| 5015 | Screw 2-56 PAN $\frac{1}{2}$ PPP.47241-316 | 2 | +0.20 |
| 5016 | Screw, Socket Hd. PF.47471-2 | 1 | +0.20 |
| 5017 | Shutter Shaft B99-0498-51 | 1 | 32.00 |
| 9718 | Spacer B99-0498-50 | 1 | 16.50 |
| 5019 | Spur Gear B99-0613-51 | 1 | 14.00 |
| 5020 | Switch, Micro WIS.6908-C-R1 | 1 | 0.95 |
| 5021 | Washer 8BA Small PF.74011-308 | 2 | +0.20 |
| 5022 | Washer 8BA Crinicle PF.74121-1 | 1 | +0.20 |
|  | Appendix 6 <br> Remote Foous Unit <br> Kit of Parts |  |  |
| 6001 | Actuator WIS.6908-C-2-4 | 2 | 0.35 |
| 6002 | Cam Assy. L.H. B99-0845-01 | 1 | 109.00 |
| 6003 | Cam Assy. R.H. B99-0846-01 | 1 | 109.00 |
| 6004 | Cap. Pap. 0.04uF $\pm 20 \%$ 250V PC. 19307-10 | 2 | 0.25 |
| 6005 | Indr. $1.2 \mathrm{mH} \pm 20 \% \mathrm{WH} .56565-\mathrm{C}-\mathrm{S} 51$ | 2 | 13.00 |
| 6006 | Lock Washer WIS.6964-C-R8 | 1 | 0.10 |
| 6007 | Motor and Bracket Assy. B99-2214-01 | 1 |  |
| 6008 | Nut PF. 52101-350 | 1 | +0.20 |
| 1888 | + | +per ten |  |
| $\begin{aligned} & \text { T676 } \\ & \text { rist } \\ & \text {;A } \end{aligned}$ |  |  | J |



## MASTER COMPONENTS LIST <br> FOn <br> MOBILE CAMERA CONTROL UNIT <br> (VB-20-3215-01)

| No. | Deseription and ldantliy | Oty. | $\begin{aligned} & \text { Price Each } \\ & \text { F-OB. U.K. } \\ & £ \\ & \text { Sterling } \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| 1 | Board B-99-0038-50 | 1 | 49.00 |
| 2 | Board B-99-0037-50 | 1 | 49.00 |
| 3 | Board B-99-0031-50 | 1 | 55.50 |
| 4 | Board assy. (F.scan) B-99-0031-01 | +1 | 240.00 |
| 5 | Board assy. (Video 1) B-99-0038-01 | ¢1 | 285.00 |
| 6 | Board assy. (Video 2) B-99-0037-01 | A | 279.00 |
| 7 | Cap. sil. mice 120 FF $\pm 5 \%$ 50V WIS-10076-B-22 now PC-18811-22 | 2 | 0.50 |
| 8 | Cap. elyc. $50 \mathrm{WF}+100 \%-20 \%$ 12V PC-18409-7 | 4 | 0.10 |
| 9 | Cap. elyc. $50 \mathrm{UF}+100 \%-20 \%$ 50V PC-18409-24 | 1 | 0.10 |
| 10 | Cap. elyc. 2000uF $+50 \%-20 \% 6 \mathrm{~V}$ PC-18409-5 | 1 | 0.10 |
| 11 | Cap. elyc. $5000 \mathrm{uF}+50 \%-20 \%$ 6V PC-18409-6 | 1 | 0.30 |
| 12 | Cap. elyc. $1000 \mathrm{uF}+50 \%-20 \% 25 \mathrm{VPC}-18409-19$ | 4 | 0.20 |
| 13 | Cap. elyc. $500 \mathrm{WF}+100 \%-20 \% 25 \mathrm{~V}$ PC $-18409-18$ | 1 | 0.10 |
| 14 | Cap. elyc. $50 \mathrm{uF}+100 \%-20 \% 25 \mathrm{VPC}-18409-15$ | 7 | 0.10 |
| 15 | Cap. elyc. $25 \mathrm{uF}+100 \%-20 \% 25 \mathrm{VPC}-18409-14$ | 7 | 0.10 |
| 16 | Cap. elyc. $16 \mathrm{uF}+100 \%-20 \% 150 \mathrm{VPC}-18406-9$ | 2 | 0.20 |
| 17 | Cap. elyc. $4 \mathrm{UF}+50 \%-20 \% 350 \mathrm{~V}$ PC-18402-4 | 0 |  |
| 18 | Cap. elyc. $8 u^{F}+50 \%-20 \%$ l50V WIS-6333-C-25 | 1 | 1.10 |
| 19 | Cap. elyc. 1000 UF $+50 \%-20 \%$ 12V PC-184.09-11 | 1 | 0.10 |
| 20 | Cap. elyc. $250 \mathrm{uF}+100 \%-20 \% 25 \mathrm{VPC}-18409-17$ | 1 | 0.10 |
| 21 | Cap. elyc. $8 \mathrm{uF}+100 \%-20 \%$ 50V PC-18409-21 | 10 | 0.20 |
| 22 | Cap. elyc. $100 \mathrm{uF}+100 \%-20 \%$ 6V PC-18409-1 | 4 | 0.10 |
| 23 | Cap. elyc. $250 \mathrm{WF}+100 \%-20 \%$ VV PC-18409-2 | 3 | 0.10 |
| 24 | Cap. elyc. $25 \mathrm{uF}+100 \%-20 \%$ 50V PC-18409-23 | 1 | 0.20 |
| 25 | Cap. elyc. 100uF 12V PC-18409-8 | 3 | 0.10 |
| 26 | Cap. metd. 2 UF $\pm 20 \%$ 250V WIS-7190-C-3 now PC-19813-3 | 1 | 0.65 |
| 27 | Cap. 0.25uF $\pm 20 \%$ l000V WIS $-10399-C-2$ now PC-19310-2 | 2 | 0.60 |
| 28 | Cap. pap. 0.01uF $\pm 20 \% 250 \mathrm{VPC}-19307-7$ | 3 | 0.20 |
| 29 | Cap. pap. 0.04uF $\pm 20 \% 250 \mathrm{~V}$ PC-19307-10 | 5 | 0.25 |
| $\begin{aligned} & \mathrm{T} 676 \\ & \mathrm{CP} \end{aligned}$ | -2 $\quad+$ Individual componenis in this list |  | $\begin{gathered} A \\ \text { Nos. } 1-600 \end{gathered}$ |


| No. | Description and Identity | Oty. | Price Each F.O.B. U.K $£$ Sturling |
| :---: | :---: | :---: | :---: |
| 93 | Relay WIS-11363-B-1-1 | 0 |  |
| 94 | Res. :omp. 1 M ohm $\pm 2 \%$ 0.25W PC-6662 $4-61$ | 3 | 0.10 |
| 95 | Hes. comp. 10 ohms $\pm 2 \% 0.25 \mathrm{~W}$ PC-66621,-1 | 1 | 0.10 |
| 96 | Hes. comp. 12 ohms $\pm 200.25 \mathrm{WiC}-666.4-2$ | 1 | 0.10 |
| 97 | Res. comf. 680 k ohms $\pm 2 \% 0.25 \mathrm{~W}$ PC -66624.59 | 0 | 0.10 |
| 98 | Res. metal oxide 68 ohms $\pm 5 \% 0.5 \mathrm{~W}$ PC-66626-1 | 3 | 0.10 |
| $9 ?$ | Res. metal oxide 680 ohms $\pm 10.60 .5 \mathrm{~W}$ PC-66637-92 | 5 | 0.10 |
| 100 | Res. metal oxide 560 ohms $\pm 1 \% 0.5 \mathrm{~W}$ PC-66,637-78 | 3 | 0.10 |
| 101 | Res. metal oxide 330 ohms $\pm 1 \% 0.5 \mathrm{~W}$ PC-66637-88 | 4 | 0.10 |
| 10? | Res. metal oxide 470 ohms $\pm 1 \% 0.5 \mathrm{~W}$ F C-66637-93 | 6 | 0.10 |
| 103 | Res. metal oxide 2.2 k ohms $\pm 1 \% 0.5 \mathrm{~W}$ PC-6663/-5 | 7 | 0.10 |
| 104 | Res. metal oxide 1 k ohm $\pm 1 \%$ 0.5W WIS-9518-B-3 now PC-66637-4 | 11 | 0.10 |
| 105 | Res. metal oxide 1.2 k ohms $\pm 1 \% 0.5 \mathrm{~W}$ PC-666,37-80 | 6 | 0.10 |
| 106 | Res. metal oxide 10 k ofms $\pm 100.5 \mathrm{~W}$ PC-66637-86 | 11 | 0.10 |
| 107 | Res. metal oxide 220 ohms $\pm 1 \% 0.5 \mathrm{~W}$ WIS-9518-B-78 now PC-66637-144 | ' | 0.10 |
| 108 | Res. metal oxide 330 k ohms $\pm 2 \%$ 0.5W WIS-9518-B-116 now $1 \%-66,331-14$ | 1 | 0.20 |
| 109 | Res. metal oxide 1.8 k ohms $\pm 1 \% 0.5 \mathrm{~W}$ WIS-9518-B-5 now PC-66637-81 | 4 | 0.20 |
| 110 | Res. metal oxide 270 ohms $\pm 5 \% 0.125 \mathrm{~W}$ PC-66626-8 | 5 | 0.10 |
| 111 | Res. metal oxide 100 ohms $\pm 1 \% 0.5 \mathrm{~W}$ ГC-6,6637-89 | 6 | 0.10 |
| 112 | Res. metal oxide 5.6 k ohms $\pm 1 \% 0.5 \mathrm{~W}$ PC-66637-85 | 4 | 0.10 |
| 11.3 | Res. metal oxide 820 ohms $\pm 1 \% 0.5 W$ WIS-9518-B-2 now PC-66637-79 | 4 | 0.10 |
| 114 | Res. metal oxide 390 ohms $\pm 1 \% 0.5 W$ WIS-9518-B-22 now PC-66637-96 | 6 | 0.10 |
| 115 | Res. metal oxide 220 k ohms $\pm 1 \%$ 0.5W WIS-9518-B-14 now PC-66637-90 | 1 | 0.20 |
| 116 | Res. metal oxide 3.3 k ohms $\pm 1 \% 0.5 \mathrm{~W}$ WIS-9518-B-7 now PC-66637-83 | 6 | 0.10 |
| 117 | Res. metal axide 15 k ohms $\pm 1 \%$ 0.5W WIS-9518-R-37 now 1C-66637-108 | 2 | 0.10 |
| 118 | Res. metal oxide 560 ohms $\pm 5 \% 0.125$ W PC-66626-12 | 4 | 0.10 |
| 119 | Res. metal oxide 150 ohins $\pm 1 \% 0.5 W$ WIS-9518-B-86 now PC-66637-148 | 3 | 0.10 |
| 120 | Res. metal oxide 120 ohms $\pm 1 \% 0.5 \mathrm{~W}$ WIS-9518-B-16 now PC-66637-91 | 6 | 0.10 |
| 121 | Res. metal oxide 6.8 k ohms $\pm 1 \% 0.5 \mathrm{~W}$ WIS-9518-B-34 now PC-66637-106 | 6 | 0,10 |
| 122 | Res. metal oxide 18 k ohms $\pm 1 \% 0.5 \mathrm{~W}$ WIS-9518-B-20 now PC-66637-94 | 2 | 0.10 |
| 123 | Res. metal oxide 2.7 k ohms $\pm 1 \%$. 5 W WIS-9518-B-6 now PC-66637-82 | 5 | 0.10 |
| 124 | Res. comp. 82 ohms $\pm 2 \%$ 0.125 P PC-66623-12 | 1 | 0.10 |
| 125 | Res. metal oxide 1.5 k ohms $\pm 1 \% 0.5 \mathrm{~W}$ WIS-9518-B-27 now PC-66637-35 | 9 | 0.10 |
| 126 | Res. metal oxide 33 k ohms $\pm 1 \% 0.5 \mathrm{~W}$ WIS-9518-B-42 now PC-66637-113 | 3 | 0.10 |
| 127 | Res. metal oxide 4.7 k ohms $\pm 1 \% 0.5 \mathrm{~W}$ WIS $9518-\mathrm{B}-8$ now PC-66637-84 | 7 | 0.10 |
| 128 | Res. metal oxide 12 k ohms $\pm 1 \% 0.5 \mathrm{~W}$ WIS-951-B-36 now PC-66637-107 | 3 | 0.10 |
| 129 | Res. metal oxide 8.2 k ohms $\pm 1 \%$ 0.5W WIS-9518-B-35 now PC-66637-75 | 1 | 0.10 |
| 130 | Rer. comp. 47 ohms $\pm 200.125 \mathrm{~W}$ PC-66623-9 | 2 | 0.10 |
| 131 | Res. comp. 22 ohms $\pm 200.125 \mathrm{WPC}-66623-5$ | 2 | 0.20 |
| 132 | Hes. comp. 10 ohms $+2 \%$ 0.125W PC-66623-1 | 2 | 0.10 |
| 133 | Res. metal oxide 150 k ohms $\pm 1 \% 0.5 \mathrm{~W}$ WIS-9518-B-15 now PC-66637-24 | 1 | 0.10 |
| 1888 |  |  |  |
| D |  |  | $\begin{aligned} & \text { T } 6768-2 \\ & C F \end{aligned}$ |


| No. | Description and Idenility | Qty. | $\begin{gathered} \text { Price Each } \\ \text { F.OB. U.K. } \\ £ \\ \text { Sterling } \end{gathered}$ |
| :---: | :---: | :---: | :---: |
| 134 | Res. comr. 56 ohms $\pm 2 \% 0.125 \mathrm{~W}$ PC-66623-10 | 1 | 0.10 |
| 135 | Res. metal oxide 180 ohms $\pm 1 \% 0.5 \mathrm{~W}$ WIS $-9518-\mathrm{B}-76$ now PC-66637-142 | 4 | 0.10 |
| 136 | Res. metal oxide 82 ohms $\pm 5 \% 0.125 \mathrm{~W} \mathrm{PC}-66626-2$ | 1 | 0.10 |
| 137 | Res. comp. 68 ohms $\pm 2 \% 0.25 \mathrm{~W}$ PC-66624-11 | 1 | 0.10 |
| 138 | Res. metal oxide 330 k ohms $\pm 1 \% 0.5 W$ WIS-9518-B-67 now PC-66637-137 | 2 | 0.10 |
| 139 | Res. metal oxide l00k ohms $\pm 1 \% 0.5 \mathrm{~W}$ PC-66637-125 | 4 | 0.10 |
| 140 | Res. comp. 100 ohms $\pm 2 \% 0.125 \mathrm{~W}$ PC-66623-13 | 1 | 0.10 |
| 341 | Res. metal oxide 47 k ohms $\pm 1 \%$ 0.5W WIS-9518-B-45 now PC-66637-116 | 6 | 0.10 |
| 142 | Res. metal oxide 56 k ohms $\pm 1 \% 0.5 \mathrm{~W}$ PC-66637-149 | 2 | 0.10 |
| 143 | Res. metal oxide 22 k ohms $\pm 1 \%$ 0.5W WIS -9518-B-39 now PC-66637-110 | 4 | 0.10 |
| 144 | Res. metal oxide 100 k ohms $\pm 5 \% 0.125 \mathrm{~W}$ PC-66626-40 | 1 | 0.10 |
| 145 | Res. metal oxide 330 onms $\pm 5 \% 0.125 \mathrm{~W}$ PC-66626-9 | 1 | 0.10 |
| 146 | Res. metal oxide lok ohms $\pm 5 \%$ 0.125 F PC-66626-28 | 1 | 0.10 |
| 147 | Res. metal oxide 12 k onms $\pm 5 \% 0.125 \mathrm{~W}$ PC-66626-29 | 1 | 0.10 |
| 148 | Res. metal oxide 39 k ohms $\pm 1 \%$ 0.5W WIS-9518-B-44 now PC-66637-115 | 2 | 0.10 |
| 149 | Res. metal oxide 270 k ohms $\pm 1$ \% 0.5 W WIS-9518-B-65 now PC-66637-135 | 2 | 0.10 |
| 150 | Res. metal oxide 180 k ohms $\pm 1 \%$ 0.5W WIS-9518-B-60 now PC-66637-130 | 0 |  |
| 151 | Res. metal oxide 3.9 k ohms $\pm 1 \% 0.5 \mathrm{~W}$ WIS-9518-B-33 now PC-66637-105 | 1 | 0.10 |
| 152 | Res. metal oxide 270 ohms $\pm 10 \% 0.5 N$ WIS $9518-\mathrm{B}-77$ now PC-66637-143 | 1 | 0.10 |
| 153 | Res. comp. 27 ohms $\pm 280.125 \mathrm{~W}$ PC-66623-6 | 1 | 0.20 |
| 154 | Res. W.W. 33 ohms $\pm 5 \%$ 1.5W PC-67007-4 | 1 | 0.20 |
| 155 | Res. w.w. 10 ohms $\pm 5 \%$ 5W PC-67008-1 | 1 | 0.10 |
| 156 | Res. 680k ohms $\pm 2 \%$ 交 W PC-66714-16 now PC-66422-33 (Now PC-66331-16) | 1 | 0.35 |
| 157 | Res. 1.5 M ohms $\pm 1 \% 1 \mathrm{~W}$ Morganite FC-75 ( $100 \mathrm{p} . \mathrm{p} . \mathrm{m} .{ }^{\circ} \mathrm{C}$ ) | 1 | 1.15 |
| 158 | Res. w.w. 68 ohms $\pm 5 \%$ 1. 5 W PC-67007-6 | 1 | 0.20 |
| 159 | Res. 820k ohms $\pm 2 \%$ 1-PC.-66331-18 | 1 | 0.35 |
| 160 | Res. w.w. 22 ohms $\pm 5 \%$ 1.5W PC-67007-3 | 1 | 0.10 |
| 161 | Res. w.w. 10 ohms $\pm 5 \%$ 1.5W PC-67007-1 | 1 | 0.20 |
| 162 | Res. W.w. 18 ohms $\pm 5 \%$ 1. 5W PC-67007-28 | 1 | 0.20 |
| 163 | Res. W.w. 1.5 ohms $\pm 5 \%$ 2.5W PC-67091-3 | 1 | 0.10 |
| 164 | Res. var. IM ohm 0.25 W PC-67202-37 | 2 | 0.60 |
| 165 | Res. var. 500k ohms 0.25W PC-67202-33 | 2 | 0.85 |
| 166 | Res. var. 100 k ohms 0.25W PC-67202-25 | 1 | 0.55 |
| 167 | Res. var. 1 k ohm 0.25 W PC-67202-1 | 1 | 0.95 |
| 168 | Res. var. 10 k ohms 0.25 W PC-67202-13 | 1 | 0.40 |
| 169 | Res. var. 50 ohms 2.5W PC-67403-13 (Now PC-68233-5) | 1 | 0.95 |
| 170 | Res. var. 500 ohms 0.5W PC-67401-17 | 2 | 0.65 |
| 171 | Res. var. 2.5k ohms 0.5W FC-67401-25 | 1 | 0.65 |
| 172 | Res. var. 75 ohms $\pm 5 \%$ IW PC-67527-1,2 | 1 | 0.70 |
| 173 | Res. var. 350 ohms $\pm 20 \% 0.25 \mathrm{~W}$ WIS-6707-C-14 now PC-67207-19 | 1 | 1.70 |
| 174 | Res. var. 500 ohms $\pm 20 \% 0.25$ W WIS $-6707-\mathrm{C}-7$ now PC-67207-12 | 2 | 1.70 |
| 175 | Res. var. 250 ohms $\therefore 20 \% 0.25$ W WIS-6707-C-13 now PC-67207-18 | 5 | 0.70 |


| No. | Description and Identily | Qty. | Price Each F.O.B. U.K. £ Sterling |
| :---: | :---: | :---: | :---: |
| 176 | Res. var. 1 k ohm $\pm 20 \% 0.25 \mathrm{~W}$ PC-67207-1 | 2 | 0.80 |
| 171 | Res. var. 10 k ohms $\pm 20 \% 0.25 \mathrm{~W}$ PC-67207-4 | 1 | 0.80 |
| 178 | Res. var. 250 k ohms $\pm 20 \%$ 0.25W PC-67207-8 | 1 | 0.85 |
| 179 | Res. var. 100 ohms $\pm 20 \%$ 0.25W WIS-6707-C-8 now PC-67207-13 | 1 | 0.65 |
| 180 | Screen B-99-1073-50 | 1 | 0.85 |
| 181 | Screw captive B-99-0695-50 | 4 | 1.50 |
| 182 | Screw captive B-99-1036-50 | 4 | 1.45 |
| 183 | Shading fenerator B-99-0033-01 | \#1 |  |
| 184 | Socket 37-way WIS-114,29-B-2 | 1 | 5.70 |
| 185 | Sucket 19-way WIS-11425-B-1 now PC-58261-1 | 1 | 3.90 |
| 186 | Socket PC-60038-1 | 9 | 0.80 |
| 187 | Socket WIS-6562-C-4 now PC-58167-4 | 1 | 0.10 |
| 188 | Socket WIS-6562-C-6 now PC-58167-6 | 1 | 0.10 |
| 189 | Socket \& cable WIS-11634-B-1 | 1 | 6.70 |
| 190 | Switch WIs-5103-C-28 | 1 | 0.60 |
| 191 | Switch WIS-5103-C-2 | 2 | 0.50 |
| 192 | Switch WIS-8730-C-40 | 1 | 2.90 |
| 193 | Switch PC-11302-2 | 1 | 1.00 |
| 194 | Sync. pulse generator B-99-0028-01 B-99-0029-01 | *1 |  |
| 195 | Tag board assy. B-99-0506-01 | 1 | 42.50 |
| 196 | Tag board assy. B-99-0691-01 | 1 | 36.50 |
| 197 | Tag board assy. B-99-0598-01 | 1 | 30.00 |
| 198 | Tag strip assy. B-99-0890-01 | 1 | 22.00 |
| 199 | Tag strip assy. B-99-0507-01 | 1 | 23.00 |
| 200 | Terml. PH-76801-1 | 134 | +0.20 |
| 201 | Terml. block 12-way Wecoway List No.WE-401-LFN | 1 | 0.35 |
| 202 | Transf. gssy. B-99-0569-01 | $\nrightarrow$ | 33.50 |
| 203 | Transf. WIS-11716-C-1 | 1 | 29.00 |
| 204 | Transistor Mullard ()C-28 | 4 | 1.00 |
| 205 | Transistor Mullard $0 \subset-23$ | 1 | 1.55 |
| 206 | Transistor Mullard OC-35 | 1 | 0.80 |
| 207 | Transistor Mullard 0C-84 | 1 C | 0.30 |
| 208 | Transistor Mullard 0C-205 | 4 | 1.40 |
| 209 | Transistor Mullard AFZ-12 | 3 | 1.10 |
| 210 | Transjistor Str BSY-27 | 10 | 0.70 |
| 1588 |  |  |  |
| $F$ | $\nmid$ Indivjdial vomponents in this list <br> * Optional - for details see MCL 2B <br> + Optional - for details see MCL 2C | + per ten | $\begin{aligned} & \mathrm{T} 6768-2 \\ & \mathrm{CP} \end{aligned}$ |





| No. | Dascriplion and identity | Qty. | $\begin{array}{\|l\|} \hline \text { Price Each } \\ \text { FO.B. U.K. } \\ \& \\ \text { Sterling } \end{array}$ |
| :---: | :---: | :---: | :---: |
| 4001 | ```APPENDIX 4 SUN SHUTTER ASSEMBLY KIT OF PARTS \\ Switch d.p. 3 posn. WIS-9025-C-4``` | 1 | 0.90 |
| 5001 | ```APPENDIX 5 \\ LENS FILTER ASSEMBLY KIT OF PARTS \\ Switch d.p. 3 posn. WIS-9025-C-4``` | 1 | 0.90 |
|  | APFENDIX 6 REMOTE POCUS UNIT KIT OF PARTS |  |  |
| 6001 | Cover WIS-9495-C-1 | 2 | 0.20 |
| 6002 | Res. W.w. 33 ohms $\pm 5 \%$ SW PC-67008-4 | 1 | 0.10 |
| $\left\|\begin{array}{l} 6003 \\ 6004 \end{array}\right\|$ | Switch 3 posn. WIS-9025-C-1-2 Switch WIS-5103-C-28 | 1 | 0.70 0.60 |
| 6005 | Zener diode Z-3-B-12 | 1 | 1.45 |
| 1588 |  |  |  |
| K |  |  | $\begin{aligned} & \text { T6768-2 } \\ & C P \end{aligned}$ |

## LASTER COMPONENTS LIST

FOR
POWFR SUPPLY UNIT (VBO1-3215-01)
POWER SUPPLY UNIT
POWER SUPPLY UNIT $\left.\begin{array}{l}\text { VBO2- } 3215-01\end{array}\right)$

## NOTES:

1. Component schedules are presented in the form of a master components list, which includes all components used in this equipment. Each component is identified by means of a spares reference number, column l. in addition to the normal part identity.
2. Components shown on individual circuit diagrams may be identified in the master list by means of the cross-reference tables associated with each circuit diagram. The numbers given are the spares reference numbers.
3. For spares ordering purposes it is only necessary to quote the exact reference at the top of this page together with the spares reference number. Individual part identities can be given as a cross check if desired, but not necessary.
4. Prices are subject to change without notice.
5. All items reference $P C$ are standardised items and comply with Government specifications where these exist.
6. All items reference WIS are manufactured by component or other suppliers to a Marconi specification which, where appropriate, complies with a Government specification.
7. All items reference $W$ are manufactured by MWT and while materials and practices are in accordance with appropriate Government specifications, these items cannot be regarded as 'Standard Items'.
P.T.O.

T6768
List 2A

```A
```

CP
8. The following abbreviations are used throughout this Master Lists

| cap. | capacitor | uH | microhenry |
| :---: | :---: | :---: | :---: |
| carb. | carbon | pr | micromicrofarad |
| c.r.t. | cathode-ray tube | mH | millihenry |
| cer. | ceramic | mA | milliampere |
| c.0. | changeover | min | minute |
| coax. | coaxial | min. | minimum |
| coeff. | coefficient | m.c. | moving coil |
| CV | Common Valve | mld. | moulded |
| comp. | composition | neg. | negative |
| c/s | cycles per second | No. | number |
| dB | decibel | osc. | oscillator |
| dia. | diameter | pap. | paper |
| d.c. | direct current | \% | per cent |
| d.p. | double pole | pos. | positive |
| d.t. | double throw | potr. | potentiometer |
| elyc. | electrolytic | prim. | primary (winding) |
| enam. | enamelled | r.f. | radio frequency |
| e.h.t. | extra high tension | rect. | rectifier |
| fig. | figure | ref. | reference |
| fil. | filament | res. | resistor |
| $f t$ | foot (feet) | res.var. | resistor variable |
| freq. | frequency |  | (potentiometer) |
| f.s.d. | full scale deflection | rev/min | revolutions per |
| gal | gallon |  | minute |
| H | henry | sect. | section |
| h.s. | high stability | sil.mica | silver mica |
| h.p. | horse power | s.p. | single pole |
| h | hour | s.t. | single throw |
| in | inch | sp.gr. | specific gravity |
| indr. | inductance, self inductor | $\begin{aligned} & \text { s.w.g. } \\ & \text { temp. } \end{aligned}$ | standard wire gauge temperature |
| insul. | insulated | F | fahrenheit |
| insulr. | insulator | terml. | terminal |
| kc/s | kilocycles per second | transf. | transformer |
| $k$ ohms | kilohm | tub. | tubular |
| kW | kilowatt | var. | variable |
| kV | kilovolt | vit. | vitreous |
| kVA | kilovolt-amp | V | volt |
| lin. | linear | VA | volt-ampere |
| lg. | long | W | watt |
| max. | maximum | W.W. | wirewound |
| $\mathrm{Mc} / \mathrm{s}$ | megacycles per second | yd | yard |
| M ohms | megohms |  |  |
| metd. | metallised |  |  |
| u | micro |  |  |
| uF | microfarad |  |  |


|  | no. | Description | : Value | $\begin{gathered} \text { Tol }: ~ \\ 8 \\ 4 \end{gathered}$ | Rtg. | 1 dentity |  | $\begin{gathered} \text { vantity } \\ \text { Ref. } \end{gathered}$ |  |  | Iscale |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | Board assembly |  |  |  | B99-1027-01 |  | -1 |  |  |  |
|  | 2 | Board assembly |  | : |  | B99-1014-01 |  |  | $t_{1}$ | 76.00 |  |
|  | 3 | Cap. elyc. | 2500ur | +100 -20 | 50 V | PC.18407-6 | 2 |  |  | 1.00 |  |
|  | 4 | Cap. elyc. | 1500ur | +100: | 50V | PC. 18407-5 |  | 2 | 2 | 0.65 |  |
|  | 5 | Cap. metd. | 0.5uF |  | 350V | WIS.7190-C-11 |  |  |  |  |  |
|  |  | Cap. meta. |  |  |  | (now PC.19814-11) | 1 | 1 | 1 | 0.70 |  |
|  | 6 | Clamp assembly |  |  |  | B99-0823-01 | 1 |  |  | 11.00 |  |
|  | 7 | Clamp assembly |  |  |  | B99-0806-01 |  | 1 | 1 | 15.00 |  |
|  | 8 | Cleat |  |  |  | PH.23801-10 |  | 2 | 2 | 0.10 |  |
|  | 9 | Clip |  |  |  | PH. 23801-6 | 1 |  |  | +0.20 |  |
|  | 10 | Clip |  |  |  | $\left\lvert\, \begin{aligned} & \text { WIS. } 4056-\mathrm{C}-1 \\ & (\text { now PC. } 265535-2) \end{aligned}\right.$ |  | 1 |  |  |  |
|  | 11 | Clip |  |  |  | PC.43308-1 |  |  | 1 | 0.10 |  |
|  | 12 | Cover | , |  |  | B99-1074-50 |  | 1 | 1 | 5.00 |  |
|  | 13. | Cover |  |  |  | B99-1015-50 | 1 |  |  | 2.90 |  |
|  | 14 | Fan |  |  |  | WIS.11554-B-1-1 | 1 |  |  | 63.50 |  |
|  | 15 | Fan |  |  |  | WIS.11555-B-1 |  | 1 |  | 82.00 |  |
|  | 16 | Fan |  |  | 28 Vdc | WIS.11333-B-1 |  |  | 1 | 46.00 |  |
|  | 17 | Fuse |  |  | 2 A | WIS . 2947-B-R9 | 2 | 2 | 2 | +0.20 |  |
|  | 18 | Fuseholder |  |  |  | WLS.1952-C-1 | 2 | 2 | 2 | 0.10 |  |
|  | 19 | Grommet |  |  |  | PH. 36501-7 | 1 |  |  | +0.20 |  |
|  | 20 | Grommet |  |  |  | PH. 36501-9 |  | 1 | 1 | +0.20 |  |
|  | 21 | Grommet |  |  |  | PH. 36501-5 |  | 3 | 3 | +0.20 |  |
|  | 22 | Insulr. | ! |  |  | WIS.11699-B-1-3 |  | 2 | 2 | 0.10 |  |

O
REf. 1 = Type VBO1-3215-01 Ref. $2=$ Type VBO2-3215-01 Ref. $3=$ Type VB03-3215-01 $\dagger$
$\nmid$ Components included in this list \&M.O.C.

+ per ten



# MASTER COMPONENTS LIST 

FOR
SYNC PULSE GENERATOR (BOARDS 1\&2)
(B99-0028-01 \& B99-0029-01)

## NOTES:

1. Component schedules are presented in the form of a master components list, which includes all components used in this equipment. Bach component is identified by means of a spares reference number, column 1. in addition to the normal part identity.
2. Components shown on individual circuit diagrams may be identified in the master list by means of the cross-reference tables associated with each circuit diagram. The numbers given are the spares reference numbers.
3. For spares ordering purposes it is only necessary to quote the exact reference at the top of this page together with the spares reference number. Individual part identities can be given as a cross check if desired, but not necessary.
4. Prices are subject to change without notice.
5. All items reference PC are standardised items and comply with Government specifications where these exist.
6. All items reference WIS are manufactured by component or other suppliers to a Marconi specification which, where appropriate, complies with a Government specification.
7. All items reference $W$ are manufactured by WNT and while materials and practices are in accordance with appropriate Government apecifications, these items cannot be regarded as 'Standard Items'.
P.T.O.

T6768
List 2B
CP
4-6-70
8. The following, alhrtviations are used throughout this Master Lists

| cap. | cnpacitor | uH | microhenry |
| :---: | :---: | :---: | :---: |
| carb. | carbon | pF | micromicrofarad |
| c.r.t. | cathode-ray tube | mH | millihenry |
| cer. | ceramic | mA | milliampere |
| c.o. | changeover | min | mirute |
| coax. | coaxial | min. | minimum |
| coeff. | coefficient | m.c. | moving coil |
| CV | Common Valve | mld. | moulded |
| comp. | composition | neg. | negative |
| c/s | cycles per second | No. | number |
| dB | decibel | osc. | oscillator |
| dia. | diameter | pap. | paper |
| d.c. | direct current | \% | per cent |
| d.p. | double pole | pos. | positive |
| d.t. | double throw | potr. | potentiometer |
| elyc. | electrolytic | prim. | primary (winding) |
| enam. | enamelled | r.f. | radio frequency |
| e.h.t. | extra high tension | rect. | rectifier |
| fig. | figure | ref. | reference |
| fil. | filament | res. | resistor |
| $f t$ | foot (feet) | res.var. | resistor variable |
| freq. | frequency |  | (potentiometer) |
| f.s.d. | full scale deflection | rev/min | revolutions per |
| gal | gallon |  | minute |
| H | henry | sect. | section |
| h.s. | high stability | sil.mica | silver mica |
| h.p. | horse power | s.p. | single pole |
| h | hour | s.t. | single throw |
| in | inch | sp.gr. | specific gravity |
| indr. | inductance, self inductor | $\begin{aligned} & \text { s.w.g. } \\ & \text { temp. } \end{aligned}$ | standard wire gauge. temperature |
| insul. | insulated | F | fahrenheit |
| insulr. | insulator | terml. | terminal |
| $\mathrm{kc} / \mathrm{s}$ | kilocycles per second | transf. | transformer |
| $k$ ohms | kilohm | tub. | tubular |
| kW | kilowatt | var. | variable |
| kV | kilovolt | vit. | vitreous |
| kVA | kilovolt-amp | V | volt |
| lin. | linear | VA | volt-ampere |
| lg. | long | W | watt |
| max. | maximum | w.w. | wirewound |
| $\mathrm{Mc} / \mathrm{s}$ | megacycles per second | yd | yard |
| M ohms | megohms |  |  |
| metd. | metallised |  |  |
| u | micro |  |  |
| UP | microfarad |  |  |


| no. | Description and ldentity | Pty. | $\begin{array}{\|c\|} \text { Price Each } \\ \text { F.OB. U.K } \\ \mathcal{L} \\ \text { Sterling } \end{array}$ | Scale |
| :---: | :---: | :---: | :---: | :---: |
| 1 | Board B99-0028-50 | 1 | 27.00 |  |
| 2 | Board B99-0029-50 | 1 | 27.00 |  |
| 3 | Cap. elyc. 1000 uF $+50 \%-20 \%$ 12V PC. 18409-11 | 2 | 0.10 |  |
| 4 | Cap. resin encapsulated $6000 \mathrm{pF} \pm 5 \%$ 50V PC.18811-44 | I | -10.00 |  |
| 5 | Cap. pap. 0.04uF $\pm 20 \%$ 250V PC.19307-10 | 3 | 0.25 |  |
| 6 | Cap. resin encapsulated $680 \mathrm{pF} \pm 5 \%$ 50V PC. $18811-28$ | 1 | +10.00 |  |
| - | Cap. elyc. $250 \mathrm{uF}+100 \%-20 \%$ 12V PC.18409-9 | 1 | 0.10 |  |
| 8 | Cap. elyc. 50uF $+100 \%-20 \%$ 12V PC. $18409-7$ | 4 | 0.10 |  |
| 9 | Cap. elyc. $100 \mathrm{UF}+100 \%-20 \%$ 6V PC. $18409-1$ | 1 | 0.10 |  |
| 10 | Cap. polyester 0.047UF $\pm 10 \%$ 125V WIS.9584-C-R11 PC.19505-11 | 1 | 0.80 |  |
| 11 | Cap. resin encapsulated $2700 \mathrm{pF} \pm 5 \%$ 50V PC. $18811-3 \mathrm{C}$ | 1 | +10.00 |  |
| 12 | Cap. resin encapsulated $4700 \mathrm{pF} \pm 5 \%$ 50V PC.18811-31 | 2 | +10.00 |  |
| 13 | Cap. resin encapsulated $330 \mathrm{pF} \pm 5 \% 50 \mathrm{~V}$ o/d PC.19832-1 | 19 | 0.40 |  |
| 14 | Cap. resin encapsulated $220 \mathrm{pF} \pm 5 \%$ 50V PC.18811-1U | 21 | +10.00 |  |
| 15 | Cap. pap. 0.001uF $\pm 20 \%$ 750V PC.19309-11 | 11 | 0.35 |  |
| 16 | Cap. resin encapsulated 100pF $\pm 5 \%$ 50V PC.18811-21 | 2 | +10.00 |  |
| 17 | Cap. resin encapsulated $150 \mathrm{pF} \pm 5 \%$ 50V PC.188il -23 | 2 | +10.00 |  |
| 18 | Cap. resin encapsulated $470 \mathrm{pF} \pm 5 \%$ 50V PC.18811-R | 1 | +10.00 |  |
| 19 | Cap. resin encapsulated 120pF $\pm$ 9\% 50V PG18811-22 | 2 | 0.50 |  |
| 20 | Cap. resin encapsulated 0.02uF $\pm 5 \%$ 50V PC.18811-32 | 1 | A10.00 |  |
| 21 | Cap. resin encapsulated $560 \mathrm{pF} \pm 5 \%$ 50V PC. $18811-27$ | 2 | 0.50 |  |
| 22 | Cap. elyc. 25uF $+100 \%-20 \%$ 25V PC.18409-14 | 5 | 0.10 |  |
| 23 | Cap. pap. $0.005 \mathrm{FF} \pm 20 \%$ 250V PC. 19307-5 | 1 | 0.25 |  |
| 24 | Clip B40-0182-50 | 5 | 0.25 |  |
| 25 | Indr. $2 \cdot 5 \mathrm{H}+50 \%-0 \%$ B99-0653-01 | 1 | 36.00 |  |
| 26 | Indr. 5 mH W. $56565-\mathrm{C}-\mathrm{S9}$ | 2 | 3.10 |  |
| 27 | Indr. $2.7 \mathrm{mH} \pm 5 \% \mathrm{~W} .56565-\mathrm{C}-\mathrm{S47}$ | 1 | 2.75 |  |
| 28 | Mounting pad WIS.11188-C-Rlnow PC.787502-1 | 1 | 0.10 |  |
| 29 | Mounting pad WIS.10646-C-R1 now PC.787501-1 | 38 | 0.10 |  |
| 30 | Rect. Mullard OA10 (PS-100437) | 1 | 0.35 |  |
| 31 | Rect. Mullard OA200 (PS-100448) | 2 | 0.10 |  |
| 32 | Rect. Mullard OA7 (PS-100436) | 2 | 0.30 |  |
| 33 | Rect. Hughes HG5004 (PS-100326) | 33 | 0.20 |  |
| 34 | Rect. Hughes HSll03 (PS-100335) | 1 | 0.65 |  |
| 35 | Res. comp. 10 ohms $\pm 2 \% 0.125 \mathrm{~W}$ PC.66623-1 | 1 | 0.10 |  |
| 36 | Res. comp. l20k ohms $\pm 2 \%$ 0.125 P PC.66623-50 | 2 | 0.10 |  |
| 37 | Res. metal oxide 47 k ohms $\pm 5 \%$ 0.125w PC.66626-36 | 3 | 0.10 |  |
| 38 | Res. metal oxide 470 ohms $\pm 5 \%$ 0.125W PC.66626-11 | 4 | 0.10 |  |
| 39 | Res. metal oxide 1 k ohm $\pm 5 \%$ 0.125W PC.66626-16 | 6 | 0.10 |  |
| T6768List 28CP |  |  |  | C |
|  |  | + M.O.C. |  |  |


| no. | Description and Identity | Oty. | Price Each <br> FO.B. U.K. <br> £ <br> Sterling | Scale |
| :---: | :---: | :---: | :---: | :---: |
| 40 | Res. metal oxide 820 ohms $\pm$ \% 0.125 W PC.66641-55 | 1 | 0.10 |  |
| 41 | Res. metal oxide 100 ohms $\pm 5 \%$ 0.125W PC.66626-3 | 2 | 0.10 |  |
| 42 | Res. comp. $\pm 2 \%$ 0.125W PC.66亿23- | $\phi_{1}$ |  |  |
| 43 | Res. metal oxide 1.5 k ohms $\pm 5 \%$ 0.125W PC.66626-18 | 7 | 0.10 |  |
| 44 | Res. metal oxide 3.3k ohms $\pm 5 \% 0.125 \mathrm{~W}$ PC.66626-22 | 26 | 0.10 |  |
| 45 | Res. metal oxide 220 ohms $\pm 2 \%$ 0.125W PC.60́641-57 | 1 | 0.10 |  |
| 46 | les. metal oxide 330 ohms $\pm 5 \% 0.125 \mathrm{~W}$ PC.66626-9 | 2 | 0.10 |  |
| 47 | Res. comp. 27 ohms $\pm 2 \% 0.125 \mathrm{~W}$ PC. $66623-6$ | 2 | 0.20 |  |
| 48 | Res. comp. 47 ohms $\pm 2 \% 0.125 \mathrm{~W}$ PC.66623-9 | 1 | 0.10 |  |
| 49 | Res. comp. 270 ohms $\pm 2 \% 0.125 W$ PC.66623-18 | 1 | 0.10 |  |
| 50 | Res. metal oxide 2.7 k ohms $\pm 5 \% 0.125 \mathrm{~W}$ PC.66626-21 | 1 | 0.10 |  |
| 51 | Res. metal oxide 120 ohms $\pm 5 \% 0.125 \mathrm{~W}$ PC,66626-4 | 1 | 0.10 |  |
| 52 | Res. comp. 18 ohms $\pm 2 \% 0.125 \mathrm{~W}$ PC.66623-4 | 0 |  |  |
| 53 | Res. metal oxide 4.7 k ohms $\pm 5 \%$ 0.125 W PC.66626-24 | 10 | 0.10 |  |
| 54 | Res. metal sxide 22 k ohms $\pm 5 \% 0.125 \mathrm{~W}$ PC.66626-32 | 13 | 0.10 |  |
| 55 | Res. metal oxide 560 ohms $\pm 5 \% 0.125 W$ PC.66626-12 | 10 | 0.10 |  |
| 56 | Res. metal oxide 10 k ohms $\pm 5 \% 0.125 \mathrm{~W}$ PC.66626-28 | 41 | 0.10 |  |
| 57 | Res. metal oxide 2.2 k ohms $\pm 5 \%$ 0.125W PC.66626-20 | 24 | 0.10 |  |
| 58 | Res. metal oxide 150 ohms $\pm 5 \% 0.125 \mathrm{~W}$ PC.66626-5 | 0 |  |  |
| 59 | Res. metal oxide 100 k ohms $\pm 5 \%$ 0.125W PC.66626-40 | 1 | 0.10 |  |
| 60 | Res. metal oxide 680 ohms $\pm 5 \%$ 0.125W PC.66626-14 | 1 | 0.10 |  |
| 61 | Res. metal oxide 33 k ohms $\pm 5 \%$ 0.125W PC.66626-34 | 1 | 0.10 |  |
| 62 | Res. metal oxide 1.2 k ohms $\pm 5 \% 0.125 \mathrm{~W}$ PC.66626-17 | 1 | 0.10 |  |
| 63 | Res. metal oxide 39k ohms $\pm 5 \%$ 0.125W PC.66626-35 | 2 | 0.10 |  |
| 64 | Res. metal oxide 18k ohms $\pm 5 \%$ 0.125 W PC.66626-31 | 3 | 0.10 |  |
| 65 | Res. comp. 56 ohms $\pm 2 \% 0.125 \mathrm{~W}$ PC.66623-10 | 2 | 0.10 |  |
| 66 | Res. metal oxide 3.9 k ohms $\pm 5 \% 0.125 \mathrm{~W}$ PC.66626-23 | 2 | 0.10 |  |
| 67 | Res. metal oxide 68 ohms $\pm 5 \% 0.125 \mathrm{~F}$ PC.66626-1 | 4 | 0.10 |  |
| 68 | Res. metal oxide 12 k ohms $\pm 5 \%$ 0.125W PC.66626-29 | 1 | 0.10 |  |
| 69 | Res. metal oxide 56 k ohms $\pm 5 \%$ 0.125w PC.66626-37 | 1 | 0.10 |  |
| 70 | Res. var. 250 ohms $\pm 20 \%$ 0.25W WIS.6707-B-Rl3 now PC.67207-20 | 1 | +10.00 |  |
| 71 | Res. var. 10 k ohms $\pm 20 \% 0.25 \mathrm{~W}$ PC.67207-4 | 1 | 0.80 |  |
| 72 | Res. var. 1 k ohm $\pm 20 \% 0.25 \mathrm{~W}$ PC.67207-1 | 2 | 0.80 |  |
| 73 | Res. var. 500 ohms $\pm 20 \% 0.25$ W WIS. $6707-\mathrm{B}-\mathrm{R} 7$ now PC.67207-12 | 1 | 1.75 |  |
| 74 | Res. var. 5k ohms $\pm 20 \% 0.25 \mathrm{~W}$ PC. 67207-3 | 3 | 0.90 |  |
| 75 | Terml. PH.76801-1 | 70 | 0.10 |  |
| 76 | Thermistor assembly B99-0911-01 | 1 | 3.25 |  |
| $\begin{aligned} & 77 \\ & 78 \end{aligned}$ | $\begin{aligned} & \text { Transf. B99-0652-01 } \\ & \text { Transf. B99-0657-01 } \end{aligned}$ | 1 | $\begin{array}{r} 9.60 \\ 41.00 \end{array}$ |  |
|  | + 6 Yalue selected on Test |  |  |  |
| D |  | m. 0. |  | t $2 B$ |



# MASTER COMPONENTS LIST 

## FOR

SHADING GENERATOR (B99-0033-01)

OPTIONAL ITEM

NOTES:

1. Component schedules are presented in the form of a master components list, which includes all components used in this equipment. Each component is identified by means of a spares reference number, column 1. in addition to the normal part identity.
2. Components shown on individual circuit diagrams may be identified in the master list by means of the cross-reference tables associated with each circuit diagram. The numbers given are the spares reference numbers.
3. For spares ordering purposes it is only necessary to quote the exact reference at the top of this page together with the spares reference number. Individual part identities can be given as a cross check if desired, but not necessary.
4. Prices are subject to change without notice.
5. All items reference PC are standardised items and comply with Government specifications where these exist.
6. All items reference WIS are manufactured by component or other suppliers to a Marconi specification which, where appropriate, complies with a Government specification.
7. All items reference $W$ are manufactured by MWT and while materials and practices are in accordance with appropriate Government specifications, these items cannot be regarded as 'Standard Items'.
P.T.O.
8. The following abbreviations are used throughout this Master Lista

| cap. | capacitor | uH | microhenry |
| :---: | :---: | :---: | :---: |
| carb. | carbon | pF | micromicrofarad |
| c.r.t. | cathode-ray tube | mH | millihenry |
| cer. | ceramic | mA | milliampere |
| c.o. | changeover | min | minute |
| coax. | coaxial | min. | minimum |
| coeff. | coefficient | m.c. | moving coil |
| CV | Common Valve | mld. | moulded |
| comp. | composition | neg. | negative |
| $\mathrm{c} / \mathrm{s}$ | cycles per second | No. | number |
| dB | decibel | osc. | oscillator |
| dia. | diameter | pap. | paper |
| d.c. | direct current | \% | per cent |
| d.p. | double pole | pos. | positive |
| d.t. | double throw | potr. | potentiometer |
| elyc. | electrolytic | prim. | primary (winding) |
| enam. | enamelled | r.f. | radio frequency |
| e.h.t. | extra high tension | rect. | rectifier |
| fig. | figure | ref. | reference |
| fil. | filament | res. | resistor |
| ft | foot (feet) | res.var. | resistor variable |
| freq. | frequency |  | (potentiometer) |
| f.s.d. | full scale deflection | rev/min | revolutions per |
| gal | gallon |  | minute |
| H | henry | sect. | section |
| h.s. | high stability | sil.mica | silver mica |
| h.p. | horse power | s.p. | single pole |
| h | hour | s.t. | single throw |
| in | inch | sp.gr. | specific gravity |
| indr. | inductance, self inductor | $\begin{aligned} & \mathrm{s} \cdot \mathrm{w} \cdot \mathrm{~g} \bullet \\ & \text { temp. } \end{aligned}$ | standard wire gauge temperature |
| insul. | insulated | F | fahrenheit |
| insulr. | insulator | terml. | terminal |
| $\mathrm{kc} / \mathrm{s}$ | kilocycles per second | transf. | transformer |
| $k$ ohms | kilohm | tub. | tubular |
| kW | kilowatt | var. | variable |
| kV | kilovolt | vit. | vitreous |
| kVA | kilovolt-amp | V | volt |
| lin. | linear | VA | volt-ampere |
| $1 g$. | long | W | watt |
| max. | maximum | W.w. | wirewound |
| Mc/s | megacycles per second | yd | yard |
| M ohms | megohms |  |  |
| metd. | metallised |  |  |
| u | micro |  |  |
| uF | microfarad |  |  |


| No. | Description and Identity 0 | Qty. | $\|$Price <br> Each <br> F.O.B.U.K <br> S <br> Sterling |
| :---: | :---: | :---: | :---: |
| 1 | Board B99-0033-50 | 1 |  |
| 2 | Cap. elyc. $25 \mathrm{uF}+100 \%-20$ | 2 | 0.10 |
| 3 | Cap. polyester luF $\pm 20 \% 250 \mathrm{~V}$ WIS. $7190-\mathrm{C-R1}$ (now PC. 19813-1) | 4 | 0.50 |
| 4 | Cap. resin encapsulated $820 \mathrm{pF} \pm 5 \%$ 50V WIS. $10076-$ B-R29 (now PC. 18811-29) | 1 | 0.50 |
| 5 | Cap. elyc. 8uF $+100 \%-20 \%$ 50V PC. 18409-21 | 1 | 0.20 |
| 6 | Cap. pap. $0.03 \mathrm{uF} \pm 20 \% 250 \mathrm{~V}$ PC. 19307-9 | 1 | 0.25 |
| 7 | Cap. polyester 0.25 UF $\pm 20 \%$ 250V WIS. $1790-\mathrm{C}-\mathrm{R} 8$ (row PC. 19813-8) | 3 | 0.30 |
| 8 | Cap. pap. 0.02uF $\pm 20 \% 250 \mathrm{~V}$ PC. $19307-8$ | 1 | 0.25 |
| 9 | Cap. elyc. $50 \mathrm{uF}+100 \%-20 \%$ I2V PC. $18409-7$ | 2 | 0.10 |
| 10 | Cap. elyc. 100uF $+100 \%-20 \%$ 25V PC. 18409-16 | 1 | 0.10 |
| 11 | Cap. pap. $0.04 \mathrm{uF} \pm 20 \%$ 250V PC. $19307-10$ | 1 | 0.25 |
| 12 | Cap. pap. $0.01 \mathrm{uF} \pm 20 \% 250 \mathrm{~V}$ PC. $19307-7$ | 2 | 0.25 |
| 13 | Cap. elyc. 0.1UF $\pm 20 \% 800 \mathrm{~V}$ WIS. $11343-\mathrm{B}-\mathrm{Rl}$ (now PC. 19325-1) | 1 | 4.00 |
| 14 | Cap. elyc. 250uF $+100 \%-20 \%$ 6V PC.18409-2 | 2 | 0.10 |
| 15 | Clip $\mathrm{B}_{4} \mathrm{O}-0182-50$ | 10 | 0.20 |
| 16 | Mounting pad WIS. 10646-C-R1 (now PC. 787502-1) | 3 | 0.10 |
| 17 | Mounting pad WIS.11188-C-R1 (now PC. $787502-1$ ) | 1 | 0.10 |
| 18 | Rect. PS. 100326 (Hughes HG5004) | 4 | 0.20 |
| 19 | Rect. PS. 100448 (Mullard OA200) | 1 | 0.10 |
| 20 | Res. metal oxide 15 k ohms $\pm 1 \%$ 0.5W WIS.9518-B-R37 (now PC.66637-108) | 1 | 0.10 |
| 21 | Res. metal oxide 68 k ohms $\pm 1 \%$ 0.5W WIS.9518-B-R48 (now PC.66637-119) | 1 | 0.10 |
| 22 | Res. metal oxide 5.6 k ohms $\pm 5 \% 0.125 \mathrm{~W}$ PC. $66626-25$ | 1 | 0.10 |
| 23 | Res. metal oxide 4.7 k ohms $\pm 1 \%$ 0.5W WIS. 9518 -B-R8 (now PC. 6663784 ) | 2 | 0.10 |
| 24 | Res. metal oxide 8.2 k ohms $\pm 1 \%$ 0.5W WIS.9518-B.-R 35 (now PC.66637-75) | 3 | 0.10 |
| 25 | Res. metal oxide 22 k ohms $\pm 1 \%$ 0.5W WIS.9518-B-R 39 (now PC.66637-110) | 2 | 0.10 |
| 26 | Res. metal oxide 680 ohms $\pm 1 \% 0.5 \mathrm{~W}$ PC. 66637-92 | 1 | 0.10 |
| 27 | Res. metal oxide 3.9 k ohms $\pm 1 \%$ 0.5W WIS.9518-B-R33 (now PC.66637-105) | 2 | 0.10 |
| 28 | Res. metal oxide 2.2 k ohms $\pm 1 \%$ 0.5W PC. 66637-5 | $t$ | 0.10 |
| 29 | Res. metal oxide 100 ohms $\pm 1 \% 0.5 \mathrm{~W}$ PC. $66637-89$ | 1 | 0.10 |
| 30 | Res. metal oxide 1.8 k ohms $\pm 5 \%$ 0.125W PC.66626-19 | 1 | 0.10 |
| 31 | Res. comp. 22 ohms $\pm 2010.125 \mathrm{~W}$ PC. 66623-5 | 1 | 0.10 |
| 32 | Res. metal oxide 1 k ohm $\pm 1 \%$ 0.5W WIS. 9518-B-R3 (now PC. 66637-4) | 5 | 0.10 |
| 33 | Res. metal oxide 1.8 k ohms $\pm 1 \% 0.5 \mathrm{~W}$ WIS.9518-B-R5 (now PC.66637-81) | 1 | 0.10 |
| 34 | Res. metal oxide 2.7k ohms $\pm 1 \%$ 0.5W WIS.9518-B-R6 (now PC.66637-82) | 1 | 0.10 |
| 35 | Res. metal oxide 330 ohms $\pm 1 \% 0.5 \mathrm{~W}$ PC.66637-88 | 1 | 0.20 |
| 36 | Kes. metal oxide 56 k ohms $\pm 1 \% 0.5 \mathrm{~W}$ PC. $66637-149$ | 1 | 0.10 |
| 37 | Res. metal oxide 6.8 k ohms $\pm 1 \% 0.5 \mathrm{~W}$ WIS.9518-B-R34 (now PC.66637-106, | 61 | 0.10 |
| 38 | Res. metal oxide 120 ohms $\pm 1 \%$ 0.5W WIS.9518-B-RI6 (now PC.66637-91) | 1 | 0.10 |

1888

## $\dagger$



## MASTER COMPONENTS LIST

## FOR

RACK MOUNTED CAMERA CONTROL UNIT TYPE V 3216

$$
\begin{gathered}
\text { (VB00-3216-01) } \\
\text { including } \\
\text { POWER UNIT } \\
\text { (VBO1-3216-01) }
\end{gathered}
$$

## NOTES:

1. Component schedules are presented in the form of a master components list, which includes all components used in this equipment. Each component is identified by means of a spares reference number, column 1. in addition to the normal part identity.
2. Components shown on individual circuit diagrams may be identified in the master list by means of the cross-reference tables associated with each circuit diagram. The numbers given are the spares reference numbers.
3. For spares ordering purposes it is only necessary to quote the exact reference at the top of this page together with the spares reference number. Individual part identities can be given as a cross check if desired, but not necessary.
4. Prices are subject to change without notice.
5. All items reference PC are standardised items and comply with Government specifications where these exist.
6. All items reference WIS are manufactured by component or other suppliers to a Marconi specification which, where appropriate, complies with a Government specification.
7. All items reference $W$ are manufactured by MWT and while materials and practices are in accordance with appropriate Government specifications, these items cannot be regarded as 'Standard Items'.
P.T.O.

T6768
A
List 3
Nos. 1-6030
8. The following aboreviations are used throughout this Master Lista

| cap. | capacitor | uH | microhenry |
| :---: | :---: | :---: | :---: |
| carb. | carbon | pF | micromicrofarad |
| c.r.t. | cathode-ray tube | mH | millihenry |
| cer. | ceramic | mA | mildiampere |
| c.o. | changeover | min | mirute |
| coax. | coaxial | min. | minimum |
| coeff. | coefficient | m.c. | moving coil |
| CV | Common Valve | mld. | moulded |
| comp. | composition | neg. | negative |
| c/s | cycles per second | No. | number |
| dB | decibel | osc. | oscillator |
| dia. | diameter | pap. | paper |
| d.c. | direct current | \% | per cent |
| d.p. | double pole | pos. | positive |
| d.t. | double throw | potr. | potentiometer |
| elyc. | electrolytic | prim. | primary (winding) |
| enam. | enamelled | r.f. | radio frequency |
| e.h.t. | extra high tension | rect. | rectifier |
| fig. | figure | ref. | reference |
| fil. | filament | res. | resistor |
| ft | foot (feet) | res.var. | resistor variable |
| freq. | frequency |  | (potentiometer) |
| f.s.d. | full scale deflection | rev/min | revolutions per |
| gal | gallon |  | minute |
| H | henry | sect. | section |
| h.s. | high stability | sil.mica | silver mica |
| h.p. | horse power | s.p. | single pole |
| h | hour | s.t. | single throw |
| in | inch | sp.gr. | specific gravity |
| indr. | inductance, self inductor | s.W.g. temp. | standard wire gauge temperature |
| insul. | insulated | F | fahrenheit |
| insulr. | insulator | terml. | terminal |
| $\mathrm{kc} / \mathrm{s}$ | kilocycles per second | transf. | transformer |
| $x$ ohms | kilohm | tub. | tubular |
| kW | kilowatt | var. | variable |
| kV | kilovolt | vit. | vitreous |
| kVA | kilovolt-amp | V | volt |
| lin. | linear | VA | volt-ampere |
| lg. | long | W | watt |
| max. | maximum | W.w. | wirewound |
| $\mathrm{Mc} / \mathrm{s}$ | megacycles per second | yd | yard |
| m ohms | megohms |  |  |
| metd. | metallised |  |  |
| u | micro |  |  |
| $u F$ | microfarad |  |  |



| No. | Description and Identity | Oty. | Price <br> Each <br> F.O.B.U.K <br> $£$ <br> Sterling | Scale |
| :---: | :---: | :---: | :---: | :---: |
| 36 | Plug 32-way PC. 57060-1 | 2 | 1.50 |  |
| 37 | Res. metal oxide lok ohms $\pm 1 \% 0.5 W$ PC. 66637/86 | 11 | 0.10 |  |
| j8 | Res. metal oxide 68 ohms $\pm 5 \% 0.125$ P PC.66626-1 | 3 | 0.10 |  |
| 39 | Res. metal cride 330 ohms $\pm 1 \% 0.5 W$ PC. $66637 / 88$ | 5 | 0.10 |  |
| 40 | Res. metal oxide 560 ohms $\pm 1 \% 0.5 W$ PC. $66637 / 78$ | 2 | 0.10 |  |
| 41 | Res. metal oxide 470 ohms $\pm 1 \% 0.5 W$ FC. 66637/93 | 4 | 0.10 |  |
| 42 | Res. metal oxide 2.2 k ohms $\pm 1 \% 0.5 \mathrm{~W}$ PC. $66637 / 5$ | 7 | 0.10 |  |
| 43 | Res. w.w. 10 ohms $\pm 5 \%$ 3\% PC.67008-1 | 1 | 0.10 |  |
| 4 | Res. comp. 680k ohms $\pm 2 \%$ 0.25W PC.66624-59 | 1 | 0.10 |  |
| 45 | Res. metal oxide 1 k ohm $\pm 1 \% 0.5$ WIS.9518-B-R3 (now PC.66637/4) | 12 | 0.10 |  |
| 46 | Res. metal oxide 470 k ohms $\pm 1 \%$ 0.5W PC. $66637 / 4 \mathrm{C}$ | 1 | 0.10 |  |
| 47 | Res. metal oxide 560 k ohms $\pm 1 \%$ lW PC.66422-33 | 6 | 0.35 |  |
| 48 | Res. comp. 1M ohm $\pm 2 \% 0.25 \mathrm{~W}$ PC.66624-61 | 3 | 0.10 |  |
| 49 | Res. metal oxide 1.5M ohms $\pm 1 \%$ 1w Morganite F.C. 75 ( 100 P.P.MOC) | , | 0.10 |  |
| 50 | Res. metal oxide l. 2 k ohms $\pm 2 \%$ 0.5w PC.66637/80 | 6 | 0.10 |  |
| 51 | Res. w.w. 68 ohms $\pm 5 \%$ l.5W PC.67007-6 | 1 | 0.20 |  |
| 52 | Res. comf. 10 ohms $\pm 2 \% 0.25 \mathrm{~W}$ PC.66624-1 | 1 | 0.10 |  |
| 53 | Res. metal oxide 680 ohms $\pm 1 \%$ 0.5W PC. $66637 / 92$ | 6 | 0.10 |  |
| 54 | Res. metal oxide 820 k ohms $\pm 101 \mathrm{~F}$ PC. $66714 / 21$ | $\frac{1}{5}$ | 0.25 |  |
| 55 | Res. metal oxide 220 ohms $\pm 1 \%$ 0.5w WIS.9518-B-R78 | 5 | 0.10 |  |
| 56 | Res. comp. 82 ohms $\pm 2 \%$ 0.125W PC.66623-12 | 2 | 0.10 |  |
| 57 | Res. W.w. 2.2 ohms $\pm 5 \%$ SW PC.67008-25 | 2 | 0.20 |  |
| 58 | Rect. Plessey 20AS | 4 | 0.30 |  |
| 59 | Rect. Plessey 10G4 (now IS107) | 2 | 0.50 |  |
| 60 | Rect. Plessey 40AS | 1 | 0.35 |  |
| 61 | Rect. Plessey 8G7 | 4 | 0.70 |  |
| 62 | Rect. Mullard OAZ02 | 2 | 0.10 |  |
| 63 | Rect. Mullard BYZ13 | 0 | 0.50 |  |
| 64 | Shading generator B99-0033-01 | 61 | 222.00 |  |
| 65 | Socket WIS.9935-RI | 7 | 2.80 |  |
| 66 | Socket 32-way PC. 57061-1 | 2 | 1.75 |  |
| 67 | Sync pulse generator B99-0028-01 | $+1$ |  |  |
| 68 | Sync pulse generator B99-0029-01 | +1 | 340.00 |  |
| 69 | Tag strip assembly B99-0832-01 | 2 | 21.00 |  |
| 70 | TEg strip assembly B99-0833-01 | 2 | 21.00 |  |
| 71 | Tag strip assembly B99-0834-01 | 2 | 21.00 |  |
| 72 | Tag strip assembly B99-0835-01 | 2 | 21.00 |  |
| 73 | Tag strip assembly B99-0836-01 | 1 | 21.00 |  |
|  | + $\quad$ O Optional item - see MCL T6768 List 2C |  |  | 768 |
| D | + Optional item - see MCL T6768 List 2B |  |  | $\text { ist } 3$ |


| no. | oescription and identity | Pty. | Price <br> Each <br> F.O.B.U.K <br> E <br> Sterling | Scale |
| :---: | :---: | :---: | :---: | :---: |
| 74 | Tag strip assembly B99-0837-01 | 1 | 21.50 |  |
| 75 | Terml. block W.21970-C-RI | 1 | 6.70 |  |
| 76 | Transf. WIS.5697-S511 | 1 | 12.00 |  |
| 77 | Transf. B99-0569-01 | $+1$ | 33.50 |  |
| 78 | Transistor Mullard 0C28 | 4 | 1.00 |  |
| 79 | Transistor Mullard 0C84 | 17 | 0.30 |  |
| 80 | Transistor Mullard OC35 | 1 | 0.80 |  |
| 81 | Trensistor Mullard OC23 |  | 2.75 |  |
| 82 | Valve G.E.C. SCl/800 | 1 |  |  |
| 83 | Valveholder PC.81811-1 | 1 | 0.10 |  |
| 84 | Valve retainer PC.82502-2 | 1 | 0.25 |  |
| 85 | Valve retainer PC.82504-1 | 1 | 0.10 |  |
| 86 | Valve top cap PC.24510-1 | 1 | 0.30 |  |
| 87 | Video amplifler No.1 B99-0038-01 | 11 |  |  |
| 88 | Video amplifier N0.2 B99-0037-01 | 1 |  |  |
| 89 | Washer WIS.11539-C-RI | 16 | 0.90 |  |
| 90 | Zener diode Semitron Z1A16 | 1 | 2.05 |  |
| 91 | Zener diode Semitron Z1B4.3 | 1 | 0.60 |  |
| 92 | Zener diode Semitron Z3B12 | 1 | 1.45 |  |
| 93 | Zener diode Semitron Z3B4.7 | 1 | 1.45 |  |
| 94 | Zener diode Mullard OAZ204 | 1 | 0.40 |  |
| 95 | Clip PC.265501-2 | 3 | +0.20 |  |
| 96 | Crystal Q01653A | 0 |  |  |
| 97 | Lamp WIS.9646-B-R9 | 1 | 0.50 |  |
| 98 | Nut (spindle gripping) PH.71104-1 | 14 | 0.10 |  |
| 99 | Res. W.w. 33 ohms $\pm 9 \% 1.5 W$ PC. 67007-4 | 1 | 0.20 |  |
| 100 | Res. comp. 22 ohms $\pm 2 \%$ 0.25W PC.66624-5 | 1 | 0.10 |  |
| 101 | Res. w.w. 56 ohms $\pm 5 \%$ 1.5W PC. 67007-37 | 1 | 0.10 |  |
| 102 | Res. W.W. 47 ohms $\pm 5 \%$ 3W PC. 67008-5 | 1 | 0.10 |  |
| 103 | Res. W.W. 220 ohms $\pm 5 \%$ 1.5W PC.67007-9 | 1 | 0.10 |  |
| 104 | Res. var. 10 ohms $\pm 10 \%$ 20W PC. 67405-33 | 1 | 2.75 |  |


| Mo． | Description and Identity | oty． | $\begin{gathered} \text { Price } \\ \text { Each } \\ \text { F.O.B.U. } \\ \mathcal{L} \\ \text { Storline } \end{gathered}$ | Scale |
| :---: | :---: | :---: | :---: | :---: |
| 105 | Res．var． 1 M ohm $\pm 20 \%$ 0．25W PC．67208－37 | 1 | 1.00 |  |
| 106 | Res．var．500k ohms $\pm 20 \% 0.25 \mathrm{~W}$ PC．67202－33 | 2 | 0.85 |  |
| 107 | Res．var． 100 k ohms $\pm 20 \% 0.25 \mathrm{~W}$ PC． $67208-25$ | 1 | 0.60 |  |
| 108 | Res．var． 1 k ohm $\pm 20 \% 0.25 \mathrm{~W}$ PC．67208－2 | 1 | 0.60 |  |
| 109 | Res．var．10k ohms $\pm 20 \% 0.25 \mathrm{~W}$ PC．67208－13 | 1 | 0.65 |  |
| 110 | Res．var． 75 ohms $\pm$ 现 1W PC．67527－42 | 1 | 0.60 |  |
| 111 | Res．var． 50 ohms $\pm 10 \%$ 2．5W PC．67403－13 | 1 | 0.95 |  |
| 112 | Res．var． 500 ohms $\pm 10 \%$ SW PC．68238－8 | 2 | 0.65 |  |
| 113 | Res．var．2．5k ohms $\pm 10 \%$ 0．5W PC．67401－25 | 1 | 0.65 |  |
| 114 | Res．var． 25 ohms $\pm 10 \% 0.5 \mathrm{WPC.67401-1}$ | 1 | 0.65 |  |
| 115 | Res．var．1M ohm $\pm 10 \% 0.25$ W PC．67202－37 | 1 | 0.60 |  |
| 116 | Socket 9－way WIS．11634－B－R1 | 1 | 6.95 |  |
| 117 | Switch PC．71302－2 | 1 | 1.00 |  |
| 118 | Switch WIS．5103－C－R2 | 3 | 0.50 |  |
| 119 | Switch WIS．8730－C－S40 | 1 | 2.90 |  |
| 120 | Terml．PH．76902－1 | 10 | ＋0．20 |  |
| 121 | Transistor Mullard 0C205 | 4 | 1.40 |  |
| 122 | Random interlace choke B99－0C40－01 | 0 |  |  |
| 123 | Cap．0． $5 \mathrm{uF} \pm 20 \% 63 \mathrm{~V}$ WIS．11983－B－Ref．2（now PC．19593－2） | 1 | 0.55 |  |
| 12！ | Cap．Elyc． 4 uF＋50\％－20\％450V PC．18406－1 | 1 | 0.10 |  |
| 125 | Cap．Pap．0．02uF $\pm 20 \%$ 250V PC．19307－8 | 2 | 0.20 |  |
| 126 | Cap．Elyc．50uF＋100\％－20\％25V PC．18409－15 | 6 | 0.10 |  |
| 127 | Cap．Metd．luF $\pm 20 \%$ 250V PC．19813－1 | 5 | 0.40 |  |
| 128 | Cap．Elyo．100uF＋100\％－20\％6V PC．18409－1 | 5 | 0.10 |  |
| 129 | Cap．Elyc． $250 \mathrm{uF}+100 \%-20 \%$ 6V PC．18409－2 | 4 | 0.10 |  |
| 130 | Cap．Elyc． 8 FF $+100 \%-20 \%$ 50V PC．18409－21 | 11 | 0.10 |  |
| 131 | Cap．Gap．0．001uF $\pm 20$ \％500V PC．19308－3 | 4 | 0.20 |  |
| 132 | Cap．Metd．O．1uF 250V PC．19813－7 | 2 | 0.25 |  |
| 133 | Cap．Elyc．25uF $+100 \%$－20\％25V PC．18409－14 | 1 | 0.10 |  |
| 154 | Cap．Resin Encapsulated 3300pF $\pm$ 瑷 50V \％／d PC．18811－50 | 1 | 0.55 |  |
| 135 | Cap．Pap． $0.005 \mathrm{UF} \pm 20 \%$ 250V PC． $19307-4$ | 1 | 0.20 |  |
| 136 | Cap．Elyc．100uF 12V PC．18409－8 | 3 | 0.10 |  |
| 137 |  | 1 | 0.50 |  |
| 138 | Cap．Metd． 0.25 FF $\pm 20 \%$ 250V PC．19813－8 | 1 | 0.25 |  |
| 139 | Cap．Resin Encapsulated 47pF $\pm 2 \mathrm{pF} \frac{1}{2} \mathrm{pF}$ 50V PC．18979－18） | 2 | 0.40 |  |
| 140 | Cap．Resin Encapsulated 390pF $\pm$ 陇 50V PC．18811－25 | 1 | 0.40 |  |
| 141 | Cap．Resin Encapsulated 180pF $\pm$ 生 50V PC．18811－24 Cap．Tantalum 60 F $+20 \%$ 15V PC．18441－11 | 1 | 0.40 |  |
| 142 | Cap．Tantalum 60uF $\pm 20 \%$ 15V PC．18441－11 | 1 | 3.40 |  |
| F | ＋ |  |  | $\begin{aligned} & 6768 \\ & \text { ist } 3 \end{aligned}$ |


| No. | Description and Identity | Oty. | $\begin{aligned} & \text { Price } \\ & \text { Each } \\ & \text { ع. s. d. } \end{aligned}$ | Scale |
| :---: | :---: | :---: | :---: | :---: |
| 143 | Cap. Resin Encapsulated 33pF $\pm 2 \mathrm{pF}$ 50V PC. $18979-16$ | 1 | 0.65 |  |
| 144 | Cap. Resin Encapsulated 82pF $\pm 2 \mathrm{pF}$ 50V PC.18979-20 | 1 | 0.70 |  |
| 145 | Cap. Resin Incapsulated 56pF $\pm 2 \mathrm{pF}$ 50V PC.18979-46 | 1 | 0.50 |  |
| 146 | Cap. Resin Encapsulated 270pF $\pm 50$ 50V PC.18811-11 | 1 | 0.85 |  |
| 147 | Cap. Pap. $400 \mathrm{pF} \pm 20 \%$ 500V PC.19306-1 | 1 | 0.25 |  |
| 148 | Cap. Var. 1.5pF -10pF PC. $20004-2$ | 1 | 0.35 |  |
| 149 | Clip B40-0182-50 | 35 | 10.50 |  |
| 150 | Indr. 2.7mH $\pm$ \% W. $56565-\mathrm{C-S} 47$ | 2 | 2.75 |  |
| 151 |  | 1 | 3.20 |  |
| 152 | Indr. 2.2luH W.62309-B-S117 | 1 | 2.90 |  |
| 153 | Rect. Hughes HG5004 | 19 | 0.20 |  |
| 154 | Rect. Mullard OA10 | 7 | 0.30 |  |
| 155 | Rect. Hughes HG5085 | 13 | 0.20 |  |
| 156 | Rect. Hughes HG1005 | 3 | 0.10 |  |
| 157 | Rect. Hughes HD 5004 | 5 | 1.20 |  |
| 158 | Rect. Mullard OA200 | 2 | 0.10 |  |
| 159 | Res. Metal 0xide 2.7k ohms $\pm 1 \%$ 0.5W PC. 66637-82 | 5 | 0.10 |  |
| 160 | Res. Metal 0xide 1.5k ohms $=1 \%$ 0.5W PC.66637-35 | 9 | 0.10 |  |
| 161 | Res. Metal Oxide 3.3k ohms $\pm 1 \%$ 0.5W PC.66637-83 | 6 | 0.10 |  |
| 162 | Res. Metal Oxide 3.9k ahms $\pm 1 \%$ 0.5W PC.66637-105 | 1 | 0.10 |  |
| 163 | Res. Metal Oxide 270 ohms $\pm 1 \%$ 0.5W PC.66637-143 | 1 | 0.10 |  |
| 164 | Res. Metal Oxide 82 ohms $\pm 1 \%$ 0. 5 F : PC. $66637-79$ | 4 | 0.10 |  |
| 165 | Res. Metal 0xide 390 ohms $\pm 1 \%$ 0.5W PC. 66637-96 | 1 | 0.10 |  |
| 166 | Res. Metal Oxide 18k ohms $\pm 1 \%$ 0.5W PC.66637-94 | 2 | 0.10 |  |
| 167 | Res. Comp. 27 ohms $\pm 2 \% 0.125 \mathrm{~W}$ PC.66623-6 | 1 | 0.20 |  |
| 168 | Res. Metal 0xide 6.8 k ohms $\pm 1 \%$ P. 5W PC. $66637-106$ | 6 | 0.10 |  |
| 169 | Res. Metal 0xide 100k ohms $\pm 1 \%$ 0.5W PC.66637-125 | 4 | 0.10 |  |
| 170 | Res. Metal Oxide 56 k ohms $\pm 1 \%$ 0.5W PC.66637-149 | 2 | 0.10 |  |
| 171 | Res. Metal Oxide 150 k ohms $\pm 1 \%$ 0.5W PC. $66637-24$ | 2 | 0.10 |  |
| 172 | Res. Metal Oxide 22 k ohms $\pm 1 \%$ 0.5W PC.66637-110 | 7 | 0.10 |  |
| 173 | Res. Metal Oxide 47 k ohms $\pm 1 \%$ 0.5W PC.66637-116 | 6 | 0.10 |  |
| 174 | Res. Metal Oxide 12 k abms $\pm 1 \%$ 0.5W PC.66637-107 | 3 | 0.10 |  |
| 175 | Res. Metal Oxide 180k ohms $\pm 1 \% 0.5 \mathrm{~W}$ PC.66637-130 | 1 | 0.10 |  |
| 176 | Res. Metal Oxide 270 k ohms $\pm 7 \% 0.5 \mathrm{~W} \mathrm{PC.66637-135}$ | 2 | 0.10 |  |
| 177 | Res. Metal Oxide 5.6 k ohms $51 \% 0.5 \mathrm{NPC.66637-85}$ | 4 | 0.10 |  |
| 178 | Res. W/W. 1.5 ohms $\pm 10 \% 1.5 \mathrm{~W}$ FC. $67091-3$ | 1 | 0.70 |  |
| 179 | Res. Metal Oxide 100 ohms $\pm 10 \%$ 0.5W PC.66637-89 | 6 | 0.20 |  |
| 180 | Res. Metal Oxide 1.8 k ohms $\pm 1 \%$ 0.5W PC.66637-81 | 4 | 0.10 |  |
| 181 | Res. Comp. 10 ohms $\pm 2 \% 0.255 \mathrm{FPC.66623-1}$ | 2 | 0.10 |  |
| 182 | Res. Metal Oxide 39 k ohms $\pm 1 \%$ 0.5W PC.66637-115 | 1 | 0.10 |  |

182 Res. Metal 0xide 39 k ohms $\pm 1 \%$ 0.5W PC. 66637-115

| Nri． | Description and Identity | Oty． | Price Each －O．B．U．K $\perp$ Sterling | Scale |
| :---: | :---: | :---: | :---: | :---: |
| 183 | Res．Metal Oxide 180k ohms $: 180$ 0．5W PC．66637－142 | 5 | 0.10 |  |
| 184 | Res．Comp． 22 ohms $\pm 2 \% 0.125 \mathrm{~W}$ PC．66623－5 | 2 | 0.20 |  |
| 185 | Res．Metal 0xide 4．7k ohms -180.5 W PC．66637－84 | 7 | 0.10 |  |
| 186 | Res．Metal 0xide 8．2k ohms $£ 780$ 0．5W PC．66637－75 | 1 | 0.10 |  |
| 187 | Res．Metal 0xide 2.2 k ohms $\pm 2 \%$ IW PC．66331－23 | 1 | 0.10 |  |
| 188 | Res．W／W． 10 ohms - 现 1．5W PC．67007－1 | 1 | 0.20 |  |
| 189 | Res．W／W． 18 ohms $=$ 恢 1．5W PC．67007－28 | 1 | 0.20 |  |
| 190 | Res．Metal Oxide 470 ohms $51 \%$ 0．5W PC．66637－93 | 3 | 0.10 |  |
| 191 | Res．Metal 0xide 120 ohms $\pm 1 \% 0.5 \mathrm{~W}$ PC．66637－91 | 1 | 0.10 |  |
| 192 | Res．Metal Oxide 390 ohms $\pm 1 \% 0.5 \mathrm{~W}$ PC．66637－96 | 6 | 0.10 |  |
| 193 | Res．Comp． 56 ohms $\pm 280.125 \mathrm{WPC.66623-10}$ | 1 | 0.10 |  |
| 194 | Res．Metal 0xide 82 ohms $\leq 5000.125 W$ PC．66626－2 | 1 | 0.10 |  |
| 195 | Res．Metal Oxide 270 ohms $\pm$ 號 0.125 W PC．66626－8 | 3 | 0.10 |  |
| 196 | Res．W／W． 22 ohms $\pm 5 \% 1.5 \mathrm{~W}$ PC． $67007-3$ | 1 | 0.10 |  |
| 197 | Res．Metal 0xide 150 ohms $\pm 1 \%$ 0．5W PC．66637－148 | 3 | 0.10 |  |
| 198 | Res．Comp． 68 ohms $\pm 2 \% 0.25 \mathrm{~W}$ PC ．66624－11 | 1 | 0.10 |  |
| 199 | Res．Metal 0xide 330k ohms $\pm 180.5 \mathrm{~W}$ PC．66637－137 | 1 | 0.10 |  |
| 200 | Res．Metal Oxide 15 k ohms $\pm 1 \% 0.5 \mathrm{~W}$ PC．66637－108 | 2 | 0.10 |  |
| 201 | Res．Comp． 47 ohms $\pm 2$ \％ $0.125 \mathrm{WPC.66623-9}$ | 2 | 0.10 |  |
| 202 | Res．Metal 0xide 33k ohms $\pm 18$ 0．5W PC．66637－113 | 3 | 0.10 |  |
| 203 | Res．Comp． 100 ohms $\pm$ \％ 0.125 W PC．66623－13 | 1 | 0.10 |  |
| 204 | Res．Metal Oxide 12 k ohms $\pm$ 倁 0.125 W PC．66626－29 | 1 | 0.10 |  |
| 205 | Res．Metal Oxide 100k ohms $\pm$ \％ 0.125 W PC．66626－40 | 1 | 0.10 |  |
| 206 |  | 1 | 0.10 |  |
| 207 | Res．Metal Oxide 10 k ohms $\pm$ \％ 0.125 W PC．66626－28 | 1 | 0.10 |  |
| 208 | Res．Metal Oxide 560 ohms $\pm$ 栊 0．125W PC．66626－12 | 4 | 0.10 |  |
| 209 | Res．Metal Oxide 220k ohms $\pm 1 \%$ 0．5W PC．66637－90 | 1 | 0.20 |  |
| 210 | Res．Var． 500 ohms $\pm 20 \%$ 0．25W PC．67207－12 | 2 | 1.70 |  |
| 212 | Res．Var． 350 ohms $\pm 20 \%$ 0．25W PC．67207－19 | 1 | 2.05 |  |
| 213 | Res．Var． 250 ohms $\pm 20 \%$ 0．25W PC．67207－18 | 5 | 0.85 |  |
| 214 | Res．Var．10k ohms $\pm 20 \%$ 0．25W PC．67207－4 | 1 | 0.80 |  |
| 215 | Res．Var． 14 ohms $\pm 20 \mathrm{C} 0.25 \mathrm{~W}$ PC．67207－1 | 2 | 0.80 |  |
| 216 | Res．Var． 250 k ohms $\pm 20 \%$ 0．25W PC．67207－8 | 1 | 1.25 |  |
| 217 | Res．Var． 100 ohms $\pm 20 \%$ 0．25W PC．67207－13 | 1 | 0.65 |  |
| 218 | Screen B99－1073－50 | 1 | 0.85 |  |
| 219 | Terminals PH．76801－1 | 134 | ＋0．20 |  |
| 220 | Transf．WIS ．11716－C－S1 | 1 | 30.50 |  |
| 221 | Transistor Mullard $0 \times 140$（ now（ 6140 ） | 11 | 0.90 |  |
| H |  |  | 6768 List |  |




| No. | Description and Identity | Oty. | Price Each F. O. B. U. 1 $\mathcal{\Sigma}$ Sterling |
| :---: | :---: | :---: | :---: |
|  | Appendix 3 <br> Line Scan Rversal Aesy. B-99-1067-01 Kit of Parts |  |  |
| 3001 | Res. Vble. 2.5k ohms 0.5W PC.67401-25 | 1 | 0.65 |
| 3002 | Switch 250V 3A PC.71301-2 | 1 | 0.40 |
| 3003 | Relay PC-65421-1 | 1 | 6.25 |
| 3004 | Screw 4-4 UNC PAN HD. 0.125 in . | 2 | 0.20 |
|  | Appendix 4 Remote Sun Shutter Asay. VB-00-4033-01 Kit of Parts |  |  |
| 1,001 | Switch D.P. 3 Position VIS.9025-C-R4 | 1 | 1.30 |
| 1,002 | Adaptor B-99-0609-50 | 2 | 14.50 |
| 14003 | Adaptor plate B-99-0630-50 | 1 | 20.00 |
| 4,0014 | Bracket B-99-0839-50 | 1 | 45.50 |
| 1,005 | Circlip PH-64702-7 | 1 | 0.10 |
| 4,006 | Collar W-11812-C-1-25HA | 1 | 5.50 |
| 4007 | Cover WIS-9495-C-1 | 1 | 0.90 |
| 14008 | Ledex Assy. B-99-0893-02 | 1 | 93.50 |
| 4009 | Nut 6BA HEX Full PF-12101-306 | 1 | 0.10 |
| 1,010 | Nut 2-56 HEX PF-45101-302 | 2 | 0.10 |
| 4011 | Res. w.w. 100 ohms $\pm 5 \%$ 3W PC-67008-7 | 1 | 0.10 |
| 1,012 | Screw 6BA Csk. Hd. 0.25 in. PF-13611-308 | 3 | 0.10 |
| 4,013 | Screw 2-56 UNC Pan Hd. 0.25 in. PF-47241-308 | 1 | 0.10 |
| 4.014 | Screw 2-56 UNC Pan Hd. 0.4375 in. PF-47241-314 | 2 | 0.10 |
| 4015 | Screw. 4-40 UNC Sjcket 0.1875 in. PF-47471-2 | 1 | 0.10 |
| 4.016 | Shutter B-99-0610-50 | 1 | 1.65 |
| 1588 | $+$ |  | I |
| T6768 |  |  |  |
| List |  |  |  |


| No. | 00scription and Identity | 019. | Price <br> Each <br> F. O. B. U.K <br> $\dot{\Sigma}$ <br> Sterling |
| :---: | :---: | :---: | :---: |
| 4017 | Shutter Shaft B-99-0498-50 | 1 | 30.00 |
| 4018 | Spacer B-99-0948-50 | 1 | 19.50 |
| 4019 | Spring B-99-5160-50 | 1 | 18.00 |
| 4.020 | Spur Gear B-99-0613-51 | 1 | 42.00 |
| 2021 | Switch-micro 5A WIS-6908-C-1 | 1 | 1.30 |
| 4022 | Washer 8BA PF-74011-308 | 2 | 0.10 |
| 4023 | Washer 8BA PF-74121-1 | 1 | 0.10 |
|  | Appendix 5 <br> Lens Filter Asay. VB-00-4034-01 Kit of Parts |  |  |
| 5001 | Switch D.P. 3 Position WIS-9025-C-R/4 | 1 | 1.30 |
| 5002 | Adaptor B-99-0664-50 | 2 | 14.50 |
| 5003 | Adaptor B-99-3642-50 | 1 | 14.50 |
| 5004 | Adaptor Plate B-99-0630-50 | 1 |  |
| 5005 | Bracket Assy. B-99-0923-01 | 1 | 76.00 |
| 5006 | Circlip PH-64702-7 | 1 | 0.10 |
| 5007 | Collar W-11812-C-1-25NA | 1 |  |
| 5008 | Cover UIS-9495-C-1 | 1 | 0.90 |
| 5009 | Filter Frame 3-99-0901-50 | 1 |  |
| 5010 | Filter Neutral Density B-99-2522-50 (Jub Schedule Item) | 1 | 7.85 |
| 0011 | Ledex Assy. B-99-0893-01 | 1 | 93.50 |
| 5012 | Nut 6BA HEX Full PF-12101-306 | 1 | 0.10 |
| 5013 | Nut 2-56 HEX PF-45101-302 | 2 | 0.10 |
| $5014$ $5015$ | Res. w.w. 100 ohms $\pm 5 \%$ 3W PC-67008-7 | 1 | 0.10 |
| 5015 | Screw 6BA Csk. Hd. 0.25 in. PF-13611-308 | 1 | 0.10 |
| 5016 | Screw 6BA Rd. Hd. 0.375 in. PF-13641-312 | 2 | 0.10 |
| $\begin{gathered} 1888 \\ M \end{gathered}$ | $\dagger$ |  | $\begin{aligned} & 6768 \\ & \text { ist } 3 \end{aligned}$ |


| $\mathrm{N}:$. | Description and identity | Diy. | Price <br> Each <br> O. B. U.K. <br> $\Sigma$ <br> Sterling |
| :---: | :---: | :---: | :---: |
| 5017 | Screw 2-56 UNC Pan Hd. 0.25 in. PF-47241-308 | 1 | 0.10 |
| 5018 | Screw 2-56 UNC Pan Hd. 0.5 in. PF-47241-316 | 2 | 0.10 |
| 5019 | Screw 4-40 UNC Socket 0.1875 in. PF-47471-2 | 1 | 0.10 |
| 5020 | Shutter Shaft B-99-0498-51 | 1 | 30.00 |
| 5001 | Spacer B-99-0948-50 | 1 |  |
| 5022 | Spring B-99-5161-50 | 1 | 18.00 |
| 5023 | Spur Gear B-99-0613-51 | 1 | 15.50 |
| 5024 | Switch-micro 5A WIS-6908-C-1 | 1 | 1.30 |
| 5025 | Washer 8BA PF-74011-308 | 2 | 0.10 |
| 5026 | Washer 6BA PF-74001-306 | 2 | 0.10 |
| 5027 | Washer 8BA Crinkle PF-74121-1 | 1 | 0.10 |
|  | ```Appendix 6 Remote Focus Unit VB-00-4012-01 Kit of Parts``` |  |  |
| 6001 | Cover WIS-9495-C-RI | 2 | 0.80 |
| 6002. | Res. w.w. 33 ohms PC-67008-4 | 0 | 0.10 |
| 6003 | Switch 3 Position WIS-9025-C-1-2 | 1 | 1.30 |
| 6001 | WSS-5103-C-R28 | 1 | 0.70 |
| 6005 | Zener Diode Brush $20 \mathrm{Bl2}$ | 0 | 0.65 |
| 6006 | Actuator WIS-6908-C-2-4 | 2 | 0.45 |
| 6007 | Bush WIS-10503-C-1 | 1 |  |
| 6008 | Cam Assy. L. H. B-99-0846-01 |  | 104.00 |
| 6009 | Cam Assy. R.H. B-99-0845-01 | 1 | 103.00 |
| 6010 | Cap. pap. 0.04uF $\pm 20 \%$ 250V PC-19307-10 | $?$ | 0.25 |
| 6011 | Cap. metd. O.1uF $\pm 20 \%$ 250V PC-19801-7 | 1 | 0.10 |
| 6012 | Diode Plessey 1024 | 2 | 0.60 |
| 6013 | Diode Zener $\mathrm{Z3B12}$ | 1 | 1.25 |
| 6014 | Indr. W. 56565-C-48 | 2 | 2.30 |
| 6015 | Indr. W. 56565-C-5l | 2 | 11.50 |
| 6016 | Lock Washer 0.25 in. I/D PF-74014-8 | 1 | 0.10 |
| 1886 |  |  |  |
| $\begin{aligned} & \text { T676 } \\ & \text { List } \end{aligned}$ |  |  |  |




[^0]:    399-0854. SH

[^1]:    $\oint$ Alternative Units see MCL 2A
    $\nrightarrow$ Individual components included in MCL

[^2]:    Page 1 of 3
    Isaue 6
    ( For power supply unit $220 / 110 \mathrm{~V} 50 / 60 \mathrm{c} / \mathrm{s}$ use No. 245 For power supply unit $400 \mathrm{c} / \mathrm{s}$ use No. 249

